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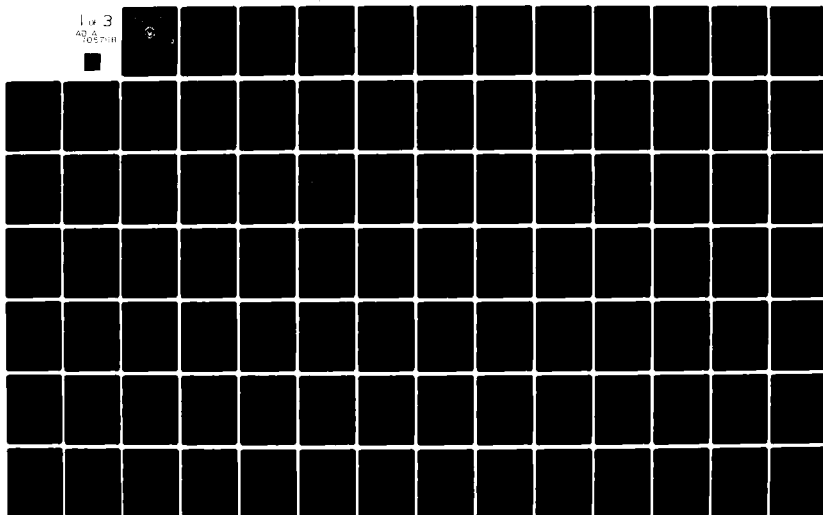
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NAVAL POSTGRADUATE SCHOOL  
Monterey, California



THESIS

COMPUTER PROGRAM APPLICATIONS TO  
TACTICAL MISSILE CONCEPTUAL DESIGN

by

Martin David Sullivan

June 1981

Thesis Advisor: Gerald H. Lindsey

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<p>This thesis is comprised of four independent computer programs and their related operating instructions. Each of these programs focuses on a particular facet of tactical missile design. The topics covered include guidance and trajectory calculations, rocket motor propulsion sizing, warhead design, and aerodynamic coefficient determination. The programs are developed from accepted mathematical procedures and are tailored to optimize operator interaction for educational purposes. This thesis is intended to be utilized</p>		

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as a supplement to the thesis Tactical Missile Conceptual Design by D. R. Redmon, Naval Postgraduate School, September 1980.

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Computer Program Applications to  
Tactical Missile Conceptual Design

by

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Lieutenant, United States Navy  
B.S., Georgia Institute of Technology, 1975

Submitted in partial fulfillment of the  
requirements for the degree of

MASTER OF SCIENCE IN ENGINEERING SCIENCE

from the

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## ABSTRACT

This thesis is comprised of four independent computer programs and their related operating instructions. Each of these programs focuses on a particular facet of tactical missile design. The topics covered include guidance and trajectory calculations, rocket motor propulsion sizing, warhead design, and aerodynamic coefficient determination. The programs are developed from accepted mathematical procedures and are tailored to optimize operator interaction for educational purposes. This thesis is intended to be utilized as a supplement to the thesis Tactical Missile Conceptual Design by D.R.Redmon, Naval Postgraduate School, September 1980.

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Finally, a certain acknowledgement must be provided to the staff of the Naval Postgraduate School Computer Center who, in the process of installing and debugging a whole new computer system, have made this thesis a most exciting and memorable undertaking.

## I. INTRODUCTION

The programs contained in this thesis were assembled expressly to supplement the work of Dan Redmon in his thesis, Tactical Missile Conceptual Design. Two of the programs, LPATH, the trajectory model, and LAERO1, the aerodynamic coefficients program, originated in Redmon's thesis and were expanded/modified for use on the Naval Postgraduate School's new IBM 370 computer system. The other two programs were generated for this thesis and utilize the procedures and principles outlined by Redmon.

The specific intention of these programs is to provide students of tactical missile engineering and design with a method of solving complex mathematical routines rapidly and interactively. Each of the programs request data which are likely to be used as design parameters for the topics concerned. The programs also allow repeated operation with input alteration capability, allowing the user to personally optimize his design. This approach was chosen to allow students to understand the relationships various input parameters have with the final solutions.

## II. TRAJECTORY MODELS

### A. DESCRIPTION AND ORIGIN OF PROGRAM

This program applies the principles of missile guidance laws to the terminal phase (the last 5 to 10 seconds) of a missile trajectory in order to determine the maximum normal acceleration on the missile for a given scenario. Of the three general guidance law categories, pursuit guidance is not included in the program capability. It has been found that pursuit guidance invariably produces a tail-chase situation, greatly reducing an anti-air missile's effectiveness against maneuvering targets of similar speed characteristics. Line-of-sight guidance and proportional navigation guidance are both options of the program.

Figure (II-1) shows a typical encounter geometry as required for this program. The encounter is considered to occur entirely within a two-dimensional plane. No differentiation is required or assumed concerning the orientation of the encounter plane. The plane may be at any angle to the horizontal as desired by the program user. The reference direction is an arbitrary choice by the program user. The angles shown are positive in value, however the program does not require positive angles. If TAL were 150 degrees, it could also be entered as -210 degrees. The IRA term represents the initial range to the target.

Tangential velocities (air speeds) of the missile and the target are considered by the program to be constant throughout the problem. Since the program concerns itself with only the final moments of a trajectory, this is a reasonable consideration. Target normal accelerations, when specified by the user, are also held constant throughout the problem for the same reason. The missile normal

Program Variables  
 $\theta$  = LOS (line of sight angle)  
 $\alpha_t$  = TAL (target alpha)  
 $\alpha_m$  = MAL (missile alpha)  
 $V_t$  = TSP (target speed)  
 $V_m$  = MSP (missile speed)  
 $R_t$  = IRT (initial range to  
 target from missile  
 launch point)  
 $R_m$  = IBM (initial range to  
 missile from  
 launch point)

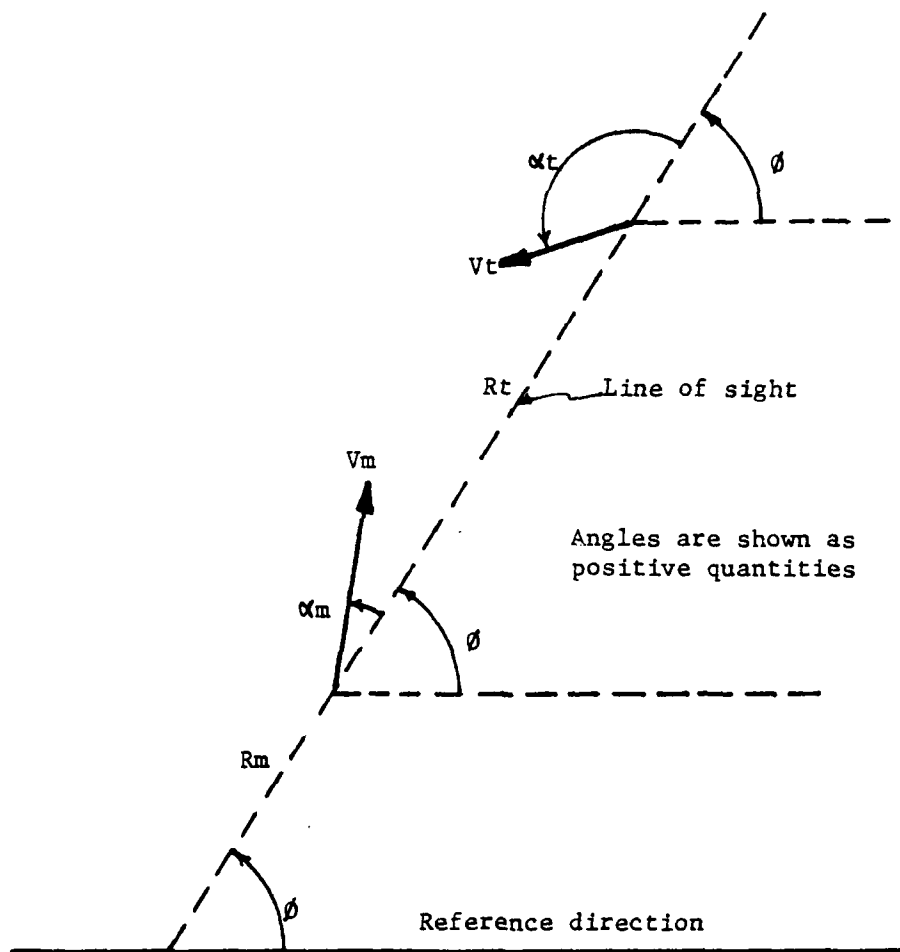


Figure (II-1). Encounter geometry

acceleration, however, is a function of the guidance laws and will vary according to the resulting flight path requirements. A constraint on the encounter is that the missile normal acceleration must be zero at the start of the problem.

The program "flies" both the missile and the target as simple points in space with no consideration given to aerodynamics. The missile will always strike the target dead center when it is given the proper speed advantage for the encounter since there is no provision for statistical miss analysis. The unbounded nature of the missile normal acceleration allows the missile to turn as rapidly as necessary to hit the target.

This program analyzes the given encounter by time increment calculations. As is the case with all integrations conducted by incremental steps, the accuracy of the results is a function of the increment size. The results will become increasingly accurate as the time increment is made smaller. However, as the time increment decreases in size, the length of the output becomes increasingly longer. The user must balance the desire for accuracy against the amount of time he wishes to spend on the computer terminal.

The primary output is a tabular listing of the missile and target coordinates at each time increment. The coordinate frame is established within the encounter plane with the abscissa oriented along the reference direction. The problem stops once the missile has passed its closest point of approach to the target. Output then provides the time to intercept from time of problem initiation and the maximum acceleration the missile was required to endure. A Versatec plot of overlaying successive encounters is an optional output.

This program originated as two separate BASIC programs written by Redmon [Ref. 1] for use on the HP 9830 desktop calculator. It was subsequently translated into FORTRAN IV for use on the IBM 370 computer system.

#### B. USER INSTRUCTIONS

If it is desired to abort the operation of this program prematurely, two methods are available. When the program is waiting for data entry, press **ENTER**. When the program is not waiting for data entry but is processing, type "HX" and press **ENTER**. Both actions will return the terminal to CMS mode.

When the screen becomes full, or "MORE...." appears in the status area, clear the screen by pressing **ALT** and **CLEAR** simultaneously. At several points in the program, the user will be directed to "CLEAR SCREEN AND INPUT 0". This is to provide proper positioning of the output on the screen for ease of reading. If any other symbol than "**4**<sup>A</sup>**///**" should appear in the lower left of the screen, press **RESET** and continue.

1. Turn the terminal on with the red **1**<sub>0</sub> switch.
2. When the large "NPS" appears after about 30 seconds, press **RESET**, then press **ENTER**.
3. When "CP READ" appears in the status area on the lower right of the screen, type "L nnnnP", where nnnn is your 4-digit user number, then press **ENTER**.
4. You will now be asked for your password. Type it in (the characters will not appear on the screen), then press **ENTER**.
5. Your personal file must contain a PROFILE EXEC routine with the appropriate Fortran GLOBAL statement. If it does not, type "GLOBAL TITLIB PORTMOD2 MOD2EEH", then press **ENTER**.

6. Type "LINK TO xxxXP 191 AS 192 RR", where xxxx is the 4-digit user number for the project file, then press **ENTER**.

7. You will now be asked for the project file password. Type it in (the characters will not appear on the screen), then press **ENTER**.

8. Type "ACCESS 192 B" and press **ENTER**.

9. Press **ALT** and **CLEAR** simultaneously to clear screen.

10. Type "LPATH" and press **ENTER**.

11. Input the following data as it is requested on the screen by typing the data and then pressing **ENTER**. Ensure that the data is input as either decimal or integer as specified. The terms in parenthesis below are the program variable names.


<u>Parameter</u>	<u>Units</u>	<u>Value range</u>
Trajectory option (TITLE)	none	0=Line-of-sight 1=Proportional navigation 2=Both
Time increment (DEL)	seconds	Larger than .0001 times the problem time
Navigation constant (NAV)	none	2.5 to 6.5
LOS Angle (LOS)	degrees	0.0 to 360.0
Initial target range from the launch site (IRT)	meters	Larger than the missile range
Target speed (TSP)	m/sec	Larger than 0.0
Target normal acceleration (TAC)	m/sec/sec	Positive is to target's left
Initial target angle to line of sight (TAL)	degrees	0.0 to 360.0 the
Missile speed (MSP)	m/sec	Larger than 0.0
Initial missile range from launch site (IRM)	meters	Such that impact occurs in less than 10 seconds

12. If you desire to rerun the problem, or want to run a new problem, answer the questions appropriately when asked by the terminal after the execution of the current problem.



13. To receive the printout and plot of your encounters, answer "no" to rerunning or restarting the problem when asked by the terminal and follow the directions presented on the screen.

14. Upon completion of the program, type "LOGOFF" and press **ENTER**.

15. Turn the terminal off with the red  switch.

### C. EXAMPLE PROBLEMS

#### 1. Example II-A. Line-of-sight Non-maneuvering Crossing Target

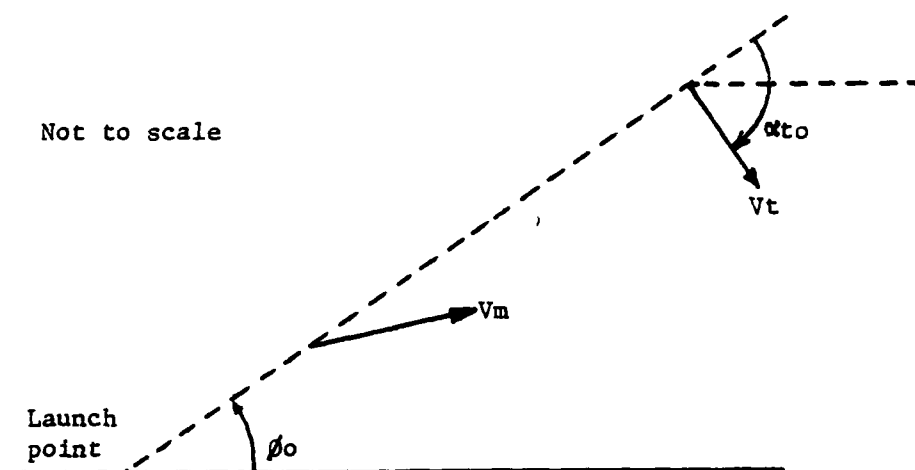


Figure (II-2). Non-maneuvering crossing target

$R_t=10000$  meters

$R_m=9000$  meters

$\phi_0=30.0$  degrees

$\alpha_{to}=-90.0$  degrees

$a_t=0$

$V_t=200$  meters/second

$V_m=800$  meters/second

TABLE (II-1). OUTPUT OF EXAMPLE II-A

\$\$\$ RUN NUMBER	1	PROBLEM PARAMETERS			
01)	TIME INCREMENT	0.0050	SECONDS		
02)	NAVIGATION CONSTANT	0.0	DEGREES		
03)	LINE-OF-SIGHT ANGLE	30.000	METERS/SEC		
04)	INITIAL SEPARATION	1000.000	M/SEC/SEC		
05)	TARGET SPEED	200.000	M/SEC/SEC		
06)	TARGET ACCELERATION	0.0	DEGREES		
07)	TARGET SPEED	-90.000	DEGREES		
08)	MISSILE INITIAL ALPHA	800.000	METERS/SEC		
09)	MISSILE INITIAL ALPHA	-13.003	DEGREES		
PROBLEM TIME(S)					
0.0					
0.125					
0.250					
0.375					
0.500					
0.625					
0.750					
0.875					
1.000					
1.125					
1.250					
1.290					
LINE OF SIGHT GUIDANCE INTERCEPT TRAJECTORY					
--POSITION COORDINATES (METERS)--					
	XM	YM	XT	YT	RANGE (METERS)
0.0	0.0	0.0	866.0	500.0	0.0
0.125	95.7	29.0	878.5	478.3	902.6
0.250	191.6	57.5	891.0	456.7	805.4
0.375	287.5	85.5	903.0	435.0	708.2
0.500	383.7	113.1	916.0	413.4	611.4
0.625	479.9	140.7	928.0	391.7	517.3
0.750	576.9	166.8	941.0	370.1	420.9
0.875	672.5	192.4	953.0	348.8	324.3
1.000	769.5	218.6	966.0	305.1	227.9
1.125	866.3	243.6	978.5	283.4	131.7
1.250	964.3	276.0	995.0	276.5	31.9
1.290	994.3	276.0	995.0	276.5	31.9
MAXIMUM LATERAL ACCELERATION ON THE MISSILE					
IS -32.000 M/SEC/SEC; OR					
THE TIME TO INTERCEPT IS 1.295 SECONDS.					
ACCEL. (M/S/S)					
					0.0
					-31.982
					-31.942
					-31.921
					-31.899
					-31.876
					-31.852
					-31.828
					-31.803
					-31.777
					-31.768

Figure (11-3). Versatec plot of example 11-A

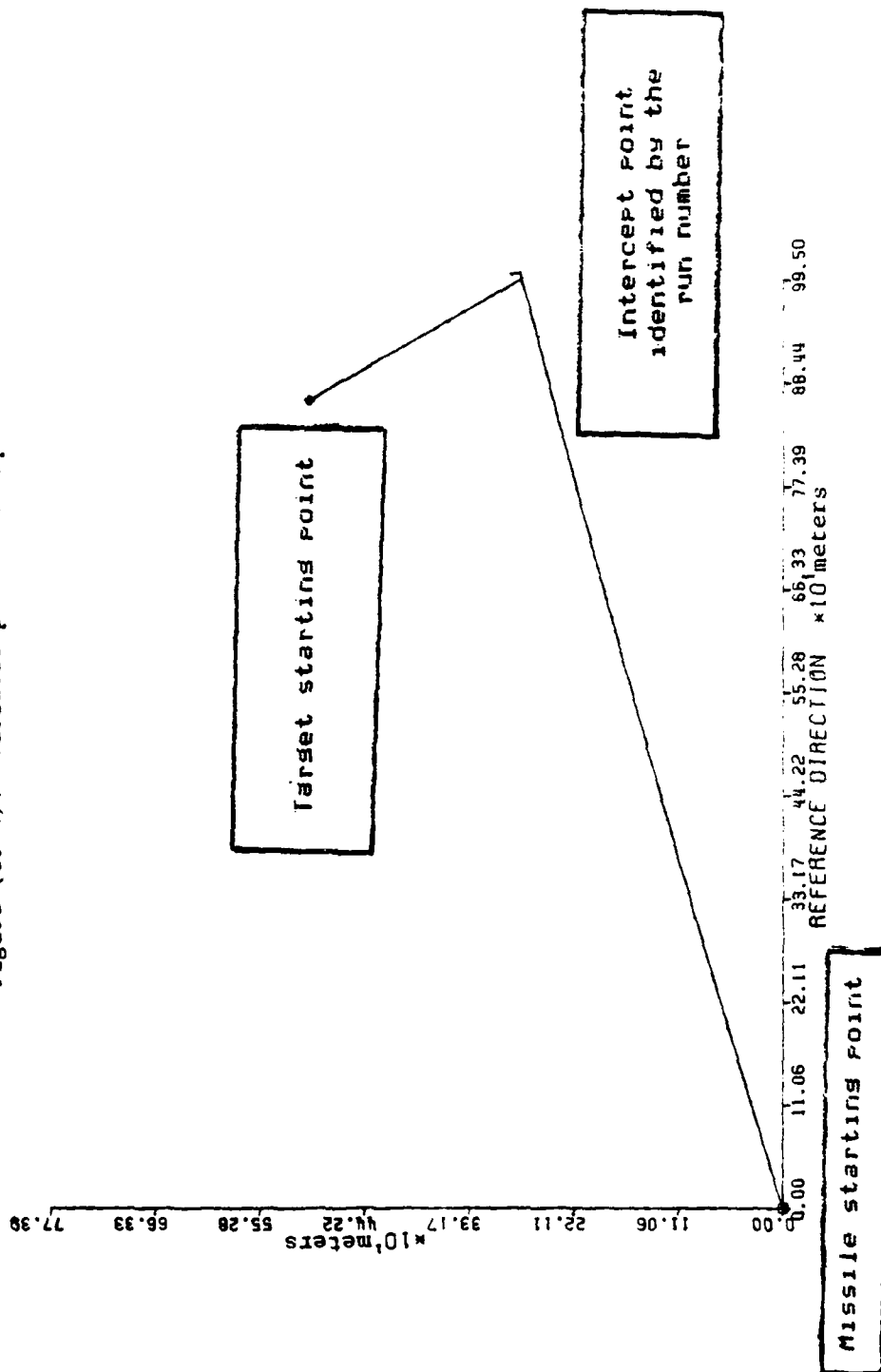


Table (II-1) is the corresponding computer output for this encounter. As indicated, the missile maximum normal acceleration is

$$a_m = -32.00 \text{ m/sec/sec or } -3.26 \text{ g's.}$$

Figure (II-3) is the Versatec plot of the engagement.

2. Example II-B. Proportional Navigation Maneuvering Crossing Target

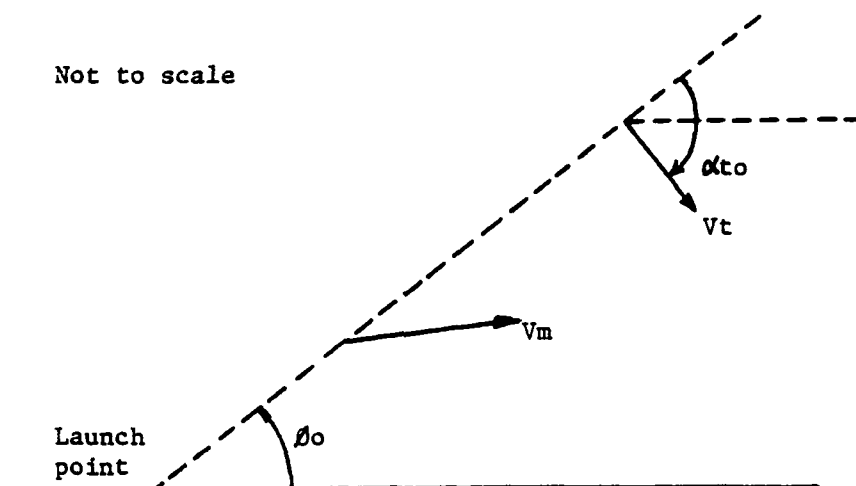


Figure (II-4). Maneuvering crossing target

$R_t = 10000$  meters  
 $R_m = 9000$  meters  
 $\theta_0 = 30.0$  degrees  
 $\alpha_{to} = -90.0$  degrees  
 $a_t = 156.8$  m/sec/sec (16 g's)  
 $V_t = 200$  meters/second  
 $V_m = 800$  meters/second  
 Navigation constant = 3.06

TABLE (II-2). OUTPUT OF EXAMPLE II-B

PROBLEM TIME(S)	PROBLEM NUMBER	1	PROBLEM PARAMETERS	0.0050 SECONDS	DEGREES	METERS/SEC	DEGREES	DEGREES	ACCEL. (M/S/S)
0.0	01)	TIME INCREMENT	3.060						0.0326
0.125	02)	NAVIGATION CONSTANT	30.000						2.7333
0.250	03)	LINE-OF-SIGHT ANGLE	1000.000						22.483
0.375	04)	INITIAL SEPARATION	200.000						40.670
0.500	05)	TARGET SPEED	156.800						64.170
0.625	06)	TARGET ACCELERATION	-90.000						92.587
0.750	07)	TARGET ALPHA	800.000						125.188
0.875	08)	MISSILE SPEED	-14.478						160.838
1.000	09)	MISSILE INITIAL ALPHA							197.903
1.125									234.093
1.250									266.065
1.375									283.935
1.470									
PROPORTIONAL NAVIGATION GUIDANCE INTERCEPT TRAJECTORY									
--POSITION COORDINATES (METERS)--									
XT									
0.0		XT	866.0	500.0	1000.0				
0.125		YT	879.5	479.0	904.3				
0.250			895.0	459.4	811.1				
0.375			912.3	441.4	720.1				
0.500			931.4	425.1	631.7				
0.625			951.9	410.9	545.2				
0.750			973.7	398.6	460.8				
0.875			996.6	388.9	377.5				
1.000			1020.3	380.9	296.4				
1.125			1044.7	375.5	216.4				
1.250			1069.5	372.1	137.4				
1.375			1094.5	373.3	59.4				
1.470			1113.5	373.3	0.5				
MAXIMUM LATERAL ACCELERATION ON THE MISSILE									
IS 283.935 M/SEC/SEC OR 28.95 G'S.									
THE TIME TO INTERCEPT IS 1.475 SECONDS.									

Figure (II-5). Versatec plot of example II-B

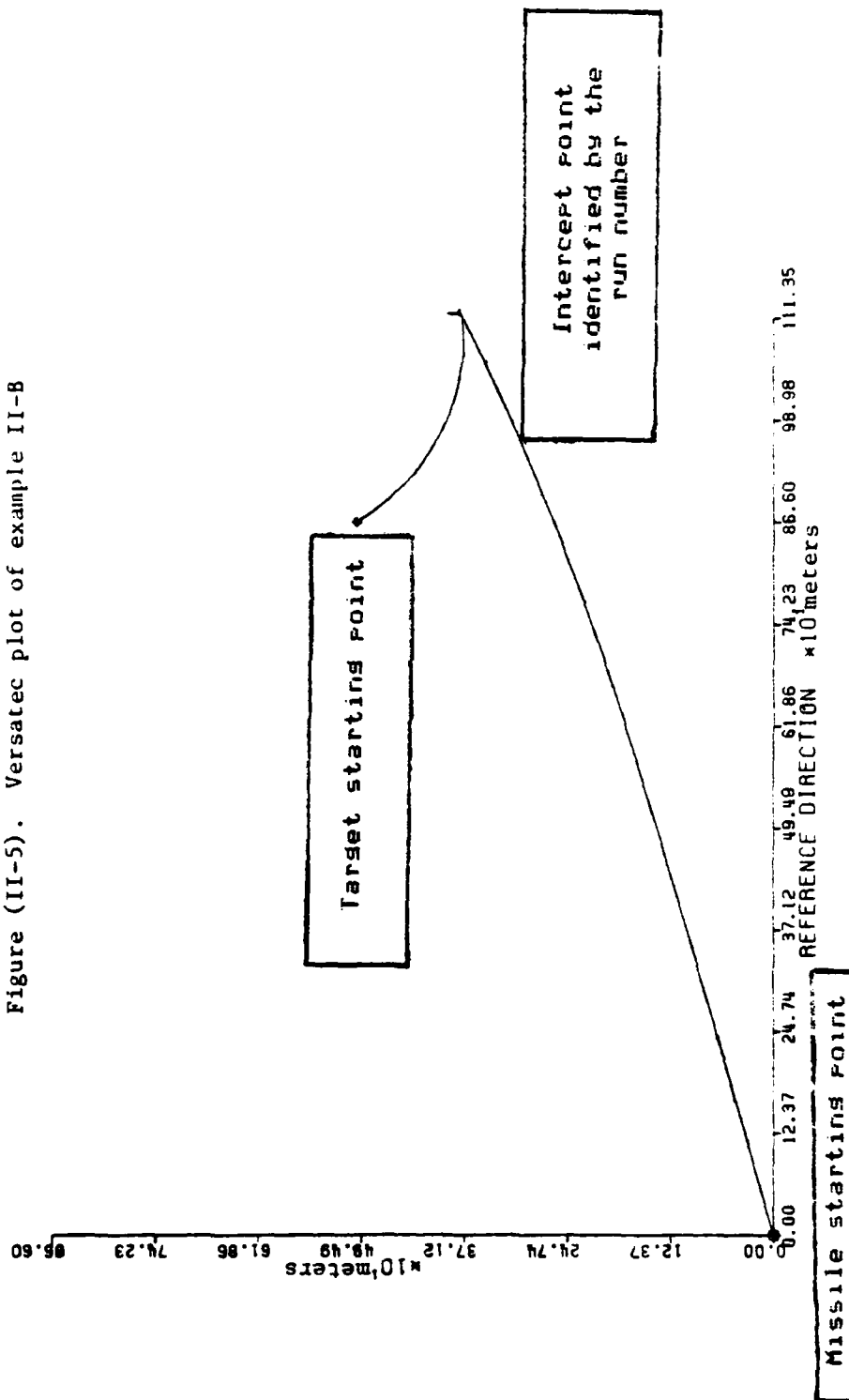
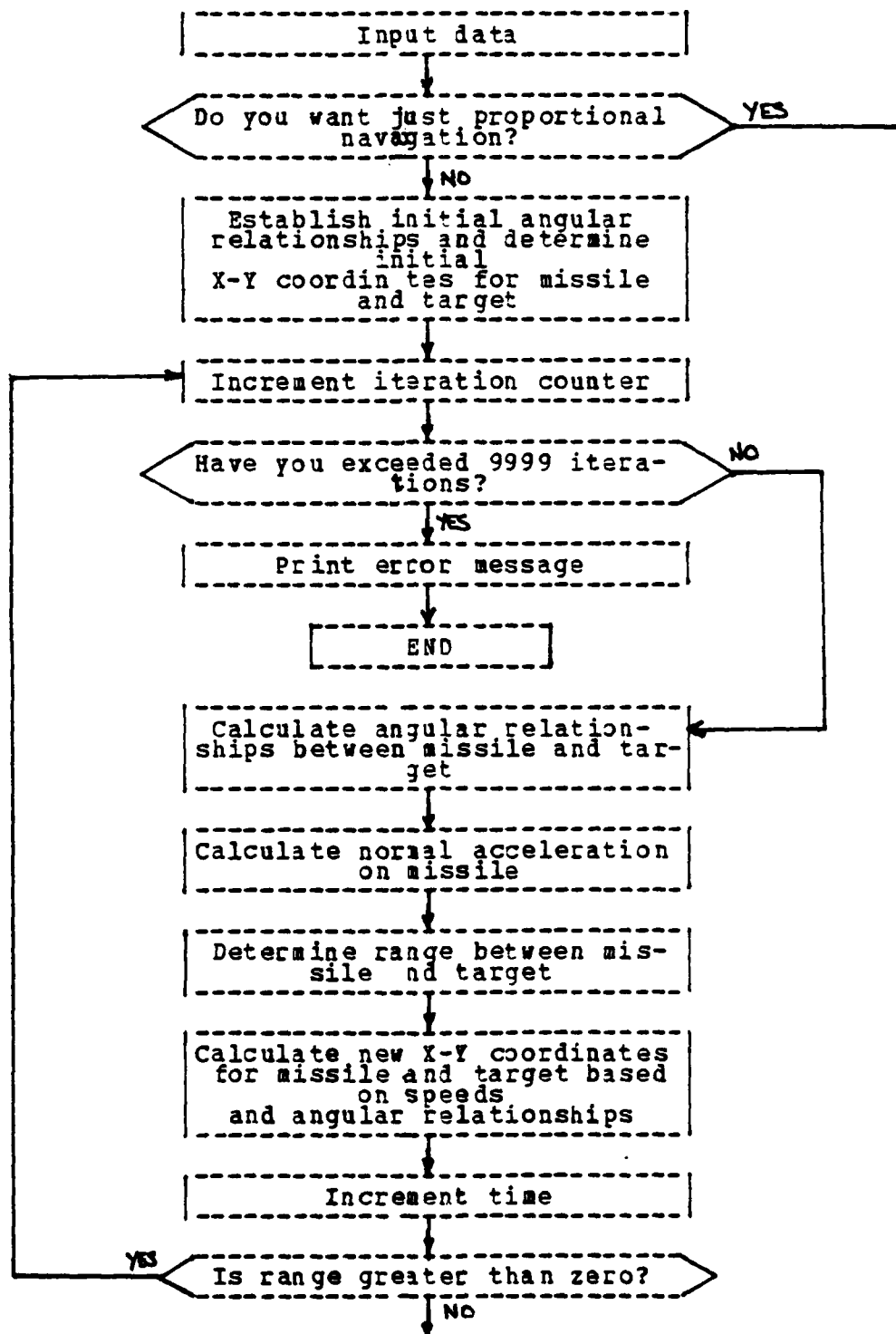


Table (II-2) is the computer output for this encounter.  
The missile maximum normal acceleration is

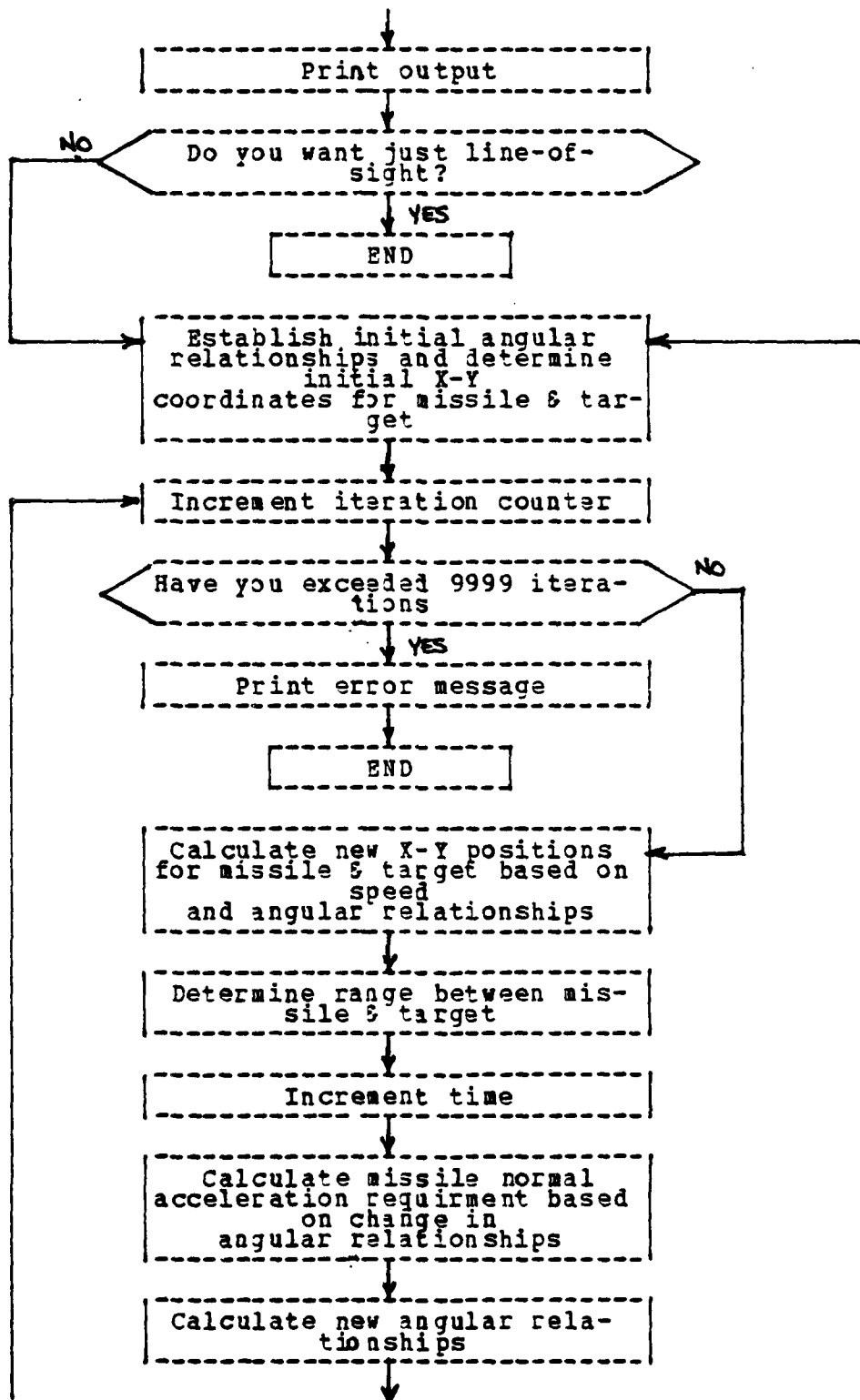
$$a_m = 283.94 \text{ m/sec/sec or } 28.95 \text{ g's.}$$

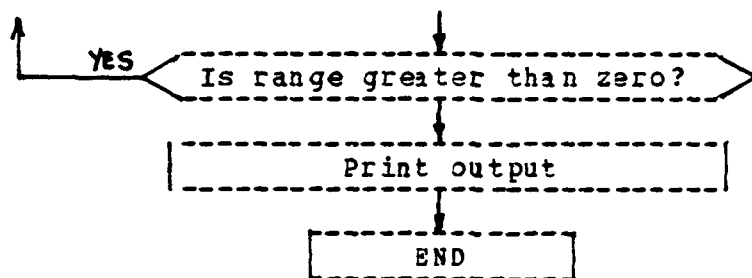
Figure (II-5) is the Versatec plot of the engagement.

# D. PROCEDURAL FLOWCHART









#### E. PROGRAM CHANGES

##### 1. Language Translation.

The two BASIC programs contained in Reference 1 were translated into standard FORTRAN IV.

##### 2. Program Condensation.

The two individual programs were combined to form a single integrated routine which allows the user to choose either of the two guidance laws or both for a given encounter. The two original programs were meshed such that only the actual guidance law algorithms are separate routines, all input and output routines are now common.

##### 3. Input and Output Facility.

The data input instructions were modified to maximize user facility on the IBM 370 System 3278 terminals. Completion of data input is now followed by data feedback for user verification prior to actual program execution.

Data output has been expanded to provide data delivery to three destinations; to the user's terminal for observation, to a printer file for hardcopy duplication of the terminal display, and to a plot data file for subsequent use by the plot program. The destinations are options chosen by the user for each execution of the program. Up to nine different problems can be printed and plotted each time the program is entered.

The program can now be rerun multiple times without exiting and re-entering each time. The user has a choice of either rerunning the same problem or initiating a new problem completely.

4. Plot Program.

PATHPLOT FORTRAN was developed to produce a Versatec plot picture of the encounter. It will produce a single plot each time the program is entered and will plot up to 9 engagements in an overlaying manner. This format was adopted to allow comparisons of successive input data modifications.

5. Data Overcapacity Check.

If the user initiates a problem requiring more than 9999 iterations, the program will stop. The user will be notified of the error and given the opportunity to rerun the problem.

6. Initial Missile Acceleration.

Initial missile acceleration was removed as a user input variable and established as zero. Due to the mathematical nature (i.e., no physical constraints) of the program, any "wrong" accelerations of the missile in the initial state were immediately "corrected" by the algorithm. The model is better served by providing no initial accelerations.

7. Theta Angles.

Both the target and the missile theta angles (the angles between the velocity vectors and the reference direction) were removed as user input variables. The program now calculates the theta angles from other input data, reducing redundancy and possible contradiction of input data.

8. Initial Conditions Perspective.

Originally, the missile guidance calculations started at  $t=0$ . Specifically, the anchor point for the line

of sight solution was the point where the missile commenced the problem, whether or not that was on the launch site. This produced a situation removed from reality where the LOS anchor point should be at the fire control location, usually at or near the launch site. A similar, though less pronounced, condition existed for the proportional navigation solution. The program was modified to provide proper positioning of the external guidance reference. As a result of the modification, an additional output is the correct lead angle for the missile at the start of the problem. This angle is based on the assumption that neither the target nor the missile have maneuvered prior to time  $t=0$ .

### III. WARHEAD DESIGN

#### A. DESCRIPTION AND ORIGIN

This program develops a warhead using the same methods as presented by D Redmon [Ref. 1]. However, its capability is somewhat greater and it applies the relationships in a slightly different manner. This program was written for this thesis in FORTRAN IV for use on the IBM 370 computer system 3278 terminals. It is configured expressly for operator-computer interaction.

It starts with an initial input of data from which a table of fragment initial velocities is generated and presented to the user. From this, the user selects values for fragment mass and impact velocity and another table is generated and displayed. From this one, the desired probability of hit given a detonation is selected and the final solution is produced. At various points during the operation of the program, the user will have opportunities to alter or revise selected parameters.

The program is limited to a cylindrical warhead with either a solid or hollow core. The fragments are required to be square in shape and are sized by the program. Figure (III-1) illustrates the shape of the warhead and the location of various input and output quantities.

Initially, the target altitude is used to determine the atmospheric density, temperature and speed of sound. These values are, in turn, used to calculate required initial velocities for the fragments. The program is preloaded with various values for the fragment mass and impact velocity, which are used to generate the table of initial velocities. These velocities come from the following relationship:

$$V(\text{hit}) = V_i [\exp(-ks)]$$

$$k = \frac{1}{2m} \rho_a A C_d$$

where  $V(\text{hit})$  is the impact velocity,  $V_i$  is the initial velocity,  $s$  is the kill radius,  $m$  is the fragment mass,  $\rho_a$  is the atmospheric density,  $A$  is the plan area of the fragment, and  $C_d$  is the drag coefficient of the fragment.

The ballistic limit velocity is calculated for the various presized fragments and is provided as a reference when choosing an appropriate impact velocity. The ballistic limit velocity is that velocity at which one half of the fragments will penetrate the target's skin and the other half will not. The empirical relationship, developed by A. E. Fuhs [Ref. 6], presents the ballistic limit velocity as a function of the fragment size to skin thickness ratio. His function dealt with steel fragments impacting an aluminum plate. His results were modified to qualitatively account for different skin materials and fragment densities.

Next computed is the fragment spray angle and the critical miss distance. The spray angle is a function of the initial velocity, the detonation velocity and the warhead length. The critical miss distance is defined as the range where the fragment spray exactly covers the entire target. The critical miss distance is used by the program to separate the two functions which determine the average number of hits received by the target. The program assumes the target is always centered within the fragment spray and aligned perpendicular to the central ray of the spray.

A selection of warheads is then produced, one for each of a preloaded set of  $P_d$ 's (probability of a hit given a detonation) to provide the user with a  $P_d$  versus warhead weight/size trade off comparison. This sizing process is based entirely on the following relationship:

$$P_d = 1 - \exp(-a)$$

where  $a$  is the average number of hits. The variable  $a$ , as shown by Redmon [Ref. 1], is a function of the cube of the warhead radius. The user then chooses a desired  $P_d$  which, in turn, produces the final warhead sizing.

Values that are shown in tabular form for user selection and input into the program are not limited to those displayed. Any value in between the displayed values or completely outside of the value range may be used. The one exception is that  $P_d$  can never be selected to be larger than .999 and may even, if forced by the program limitations, be required to be lower. Since ultimately in this algorithm,  $P_d$  is a function of the warhead radius, the maximum value for  $P_d$  may be reduced in order to keep the radius within the original input parameters. The user is notified if this condition occurs.

Useful reference information for some common explosives and case materials is contained in the following tables.

Table (III-1). Characteristics of common explosives

<u>Explosive</u>	<u>Density (lb/cu.in)</u>	<u>2E(ft/sec)</u>	<u>Vd (ft/sec)</u>
TNT	.0574	7600.	21785.
RDX	.0596	9300.	26837.
HMX	.0665	10230.	29934.
FETN	.0625	9300.	27231.
TETRYL	.0585	8200.	25755.
COMP B	.0607	8800.	25722.
OCTOL	.0650	9500.	28356.

Table (III-2). Densities of common case materials

<u>Case material</u>	<u>Density (lb/cu.in)</u>
Steel	.283
Aluminum	.100
Uranium	.688
Titanium	.163
Lead	.410

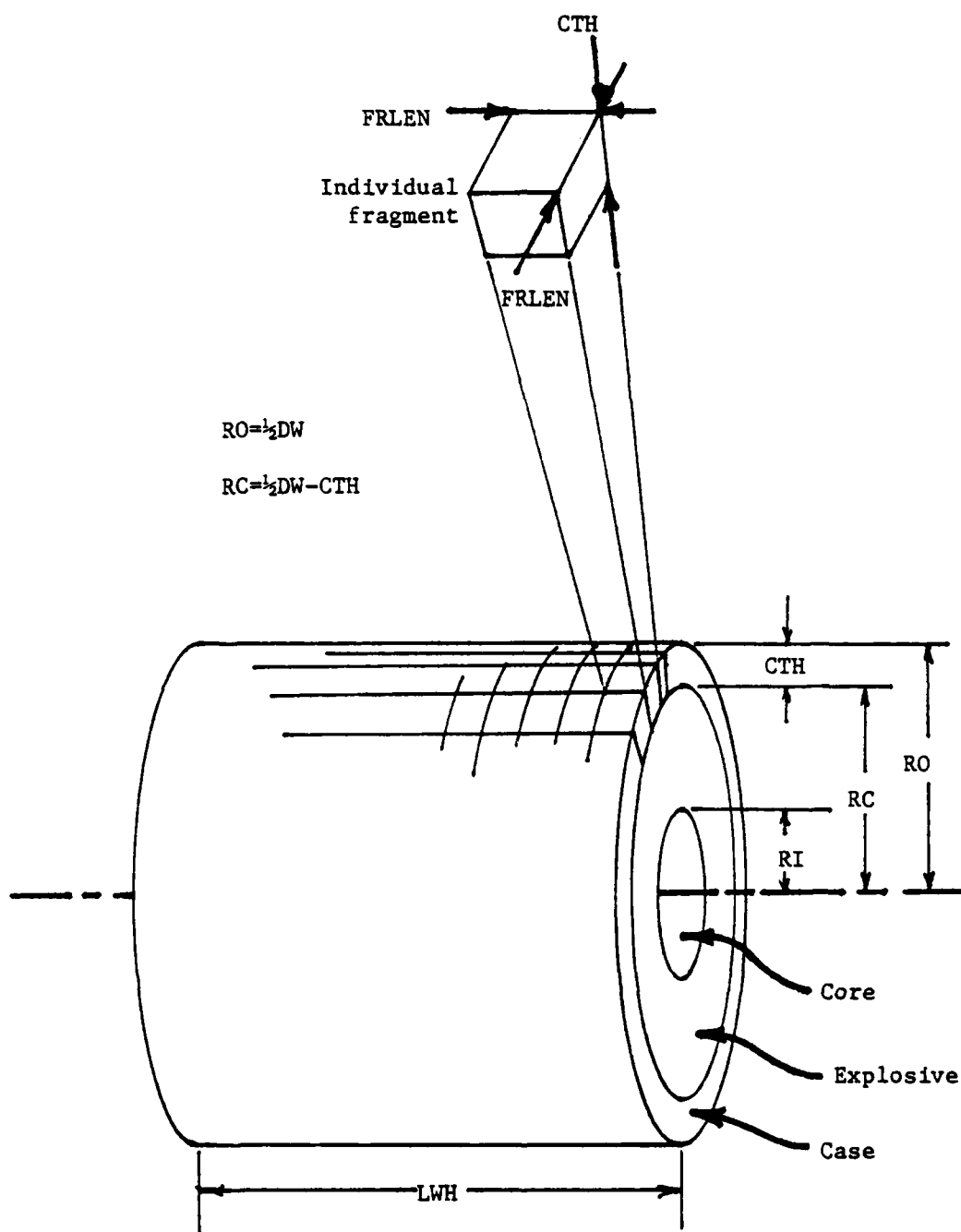


Figure (III-1). Form of warhead as used by the program



## B. USER INSTRUCTIONS

If it is desired to abort the operation of this program prematurely, two methods are available. When the program is waiting for data entry, press **ENTER**. When the program is not waiting for data entry but is processing, type "HX" and press **ENTER**. Both actions will return the terminal to CMS mode.

When the screen becomes full, or "MORE...." appears in the status area, clear the screen by pressing **ALT** and **CLEAR** simultaneously. At several points in the program, the user will be directed to "CLEAR SCREEN AND INPUT 0". This is to provide proper positioning of the output on the screen for ease of reading. If any other symbol than "4<sup>A</sup>/" should appear in the lower left of the screen, press **RESET** and continue.

1. Turn the terminal on with the red **1/0** switch.
2. When the large "NPS" appears after about 30 seconds, press **RESET**, then press **ENTER**.
3. When "CP READ" appears in the status area on the lower right of the screen, type "L nnnnP", where nnnn is your 4-digit user number, then press **ENTER**.
4. You will now be asked for your password. Type it in (the characters will not appear on the screen), then press **ENTER**.
5. Your personal file must contain a PROFILE EXEC routine with the appropriate Fortran GLOBAL statement. If it does not, type "GLOBAL TXTLIB PORTMOD2 MOD2EEH", then press **ENTER**.
6. Type "LINK TO xxxxP 191 AS 192 RR", where xxxx is the 4-digit user number for the project file, then press **ENTER**.
7. You will now be asked for the project file password. Type it in (the characters will not appear on the screen), then press **ENTER**.

8. Type "ACCESS 192 B" and press **ENTER**.
9. Press **ALT** and **CLEAR** simultaneously to clear screen.
10. Type "LBOMB" and press **ENTER**.
11. Input the following data as it is requested on the screen by typing the data and then pressing **ENTER**. Ensure that the data is input as either decimal or integer as specified. The terms in parenthesis are the program variable names. Input the following variables as decimal values:

Explosive density (XDEN)	lb/cu.in
Explosive Gurney constant (GC)	ft/sec
Explosive detonation velocity (VD)	ft/sec
Case material density (CDEN)	lb/cu.ft
Desired kill radius (RKILL)	feet
Warhead diameter (DW)	inches
Warhead length-to-diameter ratio (LTD)	
Target length (LT)	feet
Target mean width (WT)	feet
Target vulnerability, P(k/h) (PKH)	
Target altitude (ALT)	feet
Target skin thickness (TTH)	inches
Target skin material (MAT)	1.0=Aluminum
	2.0=Fiberglass/Kevlar
	3.0=Steel

12. After entering the above data, you will be presented with an initial velocity table built around your desired kill radius. The initial velocities will be listed as a function of fragment mass and impact velocity. Also provided will be the ballistic limit velocities for each of the fragment masses. Input the following parameters as decimal values:

Fragment mass (IFMLB(1))	grains
Impact velocity (VHIT(1))	ft/sec

13. You will now be presented with a shopping list of warheads developed for a range of Pd's. The warheads are described by the following quantities:

Warhead weight in pounds (total weight)  
Case thickness in inches  
Core diameter in inches  
Number of fragments from the warhead  
Number of fragments hitting the target  
Edge length of the fragments in inches


Input the following parameter as a decimal value:

Desired probability of a hit given a detonation (PDF)

14. If you desire to rerun the problem, or want to run a new problem, answer the questions appropriately when asked by the terminal after the execution of the current problem.

15. To receive the printout of your encounters, answer "nc" to rerunning or restarting the problem when asked by the terminal and follow the directions presented on the screen.

16. Upon completion of the program, type "LOGOFF" and press **ENTER**.

17. Turn the terminal off with the red  switch.

#### C. EXAMPLE PROBLEMS

##### 1. Example III-A

It was desired to build a warhead which would kill a typical cruise missile flying at 100 feet altitude. The warhead was required to have a lethal radius of 50 feet with a Pd of 0.98. TNT was selected for the explosive and steel was chosen for the case material. The diameter of the missile was 13.5 inches.

Table (III-3) outlines the input parameters. Table (III-4) shows the program output. After the initial velocity table was displayed at the terminal, the fragment mass was chosen to be 130 grains and the impact velocity was selected to be 2500 feet per second. After the Pd table was displayed, 0.98 was entered as the kill probability.

## 2. Example III-B

A warhead was required which would kill a typical manned aircraft at 30000 feet. A lethal radius of 75 feet was specified. The warhead was limited in weight to 50 pounds and needed to have a core diameter of at least 5 inches. The diameter of the missile was 10.0 inches. HMX was chosen as the explosive and depleted uranium as the case material.

Table (III-5) outlines the input parameters. Table (III-6) shows the program output. After the initial velocity table was displayed at the terminal, the fragment mass was chosen to be 210 grains and the impact velocity was selected to be 5000 feet per second. After the Pd table was displayed, it was determined that the fragments were too large and the fragment mass was then reduced to 100 grains. The impact velocity was also reduced to 3000 feet per second. When the Pd table was redisplayed, 0.995 was chosen as the desired kill probability.

TABLE (III-3). INPUT DATA FOR EXAMPLE III-A

THE FOLLOWING IS A SUMMARY OF THE INPUT DATA:

01)	EXPLOSIVE DENSITY	0.05740	LB/CU.IN
02)	EXPLCSIVE GURNEY CONSTANT	7600.00	FT/SEC
03)	EXPLOSIVE DETONATION VELOCITY	21785.00	FT/SEC
04)	CASE MATERIAL DENSITY	0.2830	LB/CU.IN
05)	DESIRED KILL RADIUS	50.0	FEET
06)	WARHEAD DIAMETE	13.50	INCHES
07)	WARHEAD LENGTH-TJ-DIAMETER RATIO	2.50	
08)	TARGET LENGTH	36.00	FEET
09)	TARGET WIDTH	3.50	FEET
10)	TARGET VULNERABILITY, P(K/H)	0.150	
11)	TARGET ALTITUDE	100.	FEET
12)	TARGET SKIN THICKNESS	0.060	INCHES
13)	TARGET SKIN MATERIAL	STEEL	

TABLE (III-4). OUTPUT DATA FOR EXAMPLE III-A

INITIAL VELOCITY TABLE FOR 50.0 FT KILL RADIUS									
IMPACT VELOCITY		50 GR.	100 GR.	150 GR.	RADIUS				
		2513.	2078.	1895.	200 GR.	250 GR.	300 GR.		
1000.		5027.	4156.	3789.	1787.	1714.	1661.		
2000.		7540.	6235.	5684.	3574.	3429.	3321.		
3000.		10054.	8313.	7579.	5361.	5143.	4982.		
4000.		12567.	10391.	9473.	7148.	6857.	6643.		
5000.		15081.	12469.	11368.	8936.	8571.	8303.		
6000.					10723.	10286.	9964.		
BALLISTIC LIMIT		641.	533.	476.	439.	412.	391.		
FRAGMENT MASS..... 130.0 GRAINS									
IMPACT VELOCITY..... 2500. FT/SEC									
WARHEAD WEIGHT		CASE THICKNESS	CORE DIAMETER	FRAGMENTS					
				NUMBER	ON TARGET	LENGTH			
0.999	183.17	0.55	10.51	3587.64	71.94	0.35			
0.990	139.85	0.48	11.14	2392.40	47.98	0.37			
0.980	125.45	0.45	11.35	2032.49	40.76	0.38			
0.950	105.03	0.41	11.65	1556.62	31.22	0.40			
0.900	88.15	0.38	11.89	1196.59	24.00	0.42			

KILL PROBABILITY..... 0.980

WARHEAD DESCRIPTION-----

WARHEAD WEIGHT 125.45 POUNDS  
 EXPLOSIVE WEIGHT 45.39 POUNDS  
 CASE WEIGHT 80.07 POUNDS  
 CASE THICKNESS 0.4513 INCHES  
 CORE DIAMETER 11.35 INCHES  
 FRAGMENT WEIGHT 130.00 GRAINS  
 FRAGMENT DIMENSIONS 0.381 X 0.451 INCHES  
 NUMBER OF FRAGMENTS 2032.  
 NUMBER OF HITS ON TARGET 41.  
 PROBABILITY OF KILL (PD) 0.980  
 INITIAL FRAGMENT VELOCITY 4886.8 FT/SEC  
 CRITICAL MISS DISTANCE 1912.1 FEET

TABLE (III-5). INPUT DATA FOR EXAMPLE III-B

THE FOLLOWING IS A SUMMARY OF THE INPUT DATA:

01)	EXPLOSIVE DENSITY	0.06650	LB/CU.IN
02)	EXPLOSIVE GURNEY CONSTANT	10230.00	FT/SEC
03)	EXPLOSIVE DETONATION VELOCITY	29934.00	FT/SEC
04)	CASE MATERIAL DENSITY	0.6880	LB/CU.IN
05)	DESIRED KILL RADIUS	75.0	FEET
06)	WARHEAD DIAMETER	10.00	INCHES
07)	WARHEAD LENGTH-TO-DIAMETER RATIO	2.00	
08)	TARGET LENGTH	60.00	FEET
09)	TARGET WIDTH	20.00	FEET
10)	TARGET VULNERABILITY, P(K/H)	0.100	
11)	TARGET ALTITUDE	30000.	FEET
12)	TARGET SKIN THICKNESS	0.180	INCHES
13)	TARGET SKIN MATERIAL	ALUMINUM	

TABLE (III-6). OUTPUT DATA FOR EXAMPLE III-B

INITIAL VELOCITY TABLE FOR 75.0 FT KILL RADIUS				
VELOCITY	50 GR.	100 GR.	150 GR.	200 GR.
1000.	1329.	1253.	1218.	1196.
2000.	2658.	2507.	2436.	2393.
3000.	3988.	3760.	3654.	3589.
4000.	5317.	5014.	4873.	4785.
5000.	6646.	6267.	6091.	5982.
6000.	7975.	7521.	7309.	7178.
BALLISTIC LIMIT	329.	277.	249.	231.

FRAGMENT MASS..... 210.0 GRAINS  
 IMPACT VELOCITY..... 5000. FT/SEC

PD	WARHEAD		CASE THICKNESS	CORE DIAMETER	FRAGMENTS		
	WEIGHT	HEIGHT			NUMBER	ON TARGET	LENGTH
0.999	90.17	0.27	0.27	7.95	1480.22	75.39	0.40
0.990	68.82	0.23	0.23	8.41	986.93	50.26	0.43
0.980	61.73	0.22	0.22	8.56	838.42	42.70	0.44
0.950	51.67	0.20	0.20	8.77	642.08	32.70	0.46
0.900	43.3	0.19	0.19	8.95	493.54	25.14	0.48

INITIAL VELOCITY TABLE FOR 75.0 FT KILL RADIUS				
VELOCITY	50 GR.	100 GR.	150 GR.	200 GR.
1000.	1329.	1253.	1218.	1196.
2000.	2658.	2507.	2436.	2393.
3000.	3988.	3760.	3654.	3589.
4000.	5317.	5014.	4873.	4785.
5000.	6646.	6267.	6091.	5982.
6000.	7975.	7521.	7309.	7178.
BALLISTIC LIMIT	329.	277.	249.	231.

FRAGMENT MASS..... 100.0 GRAINS  
 IMPACT VELOCITY..... 3000. FT/SEC



TABLE (III-6). CONTINUED

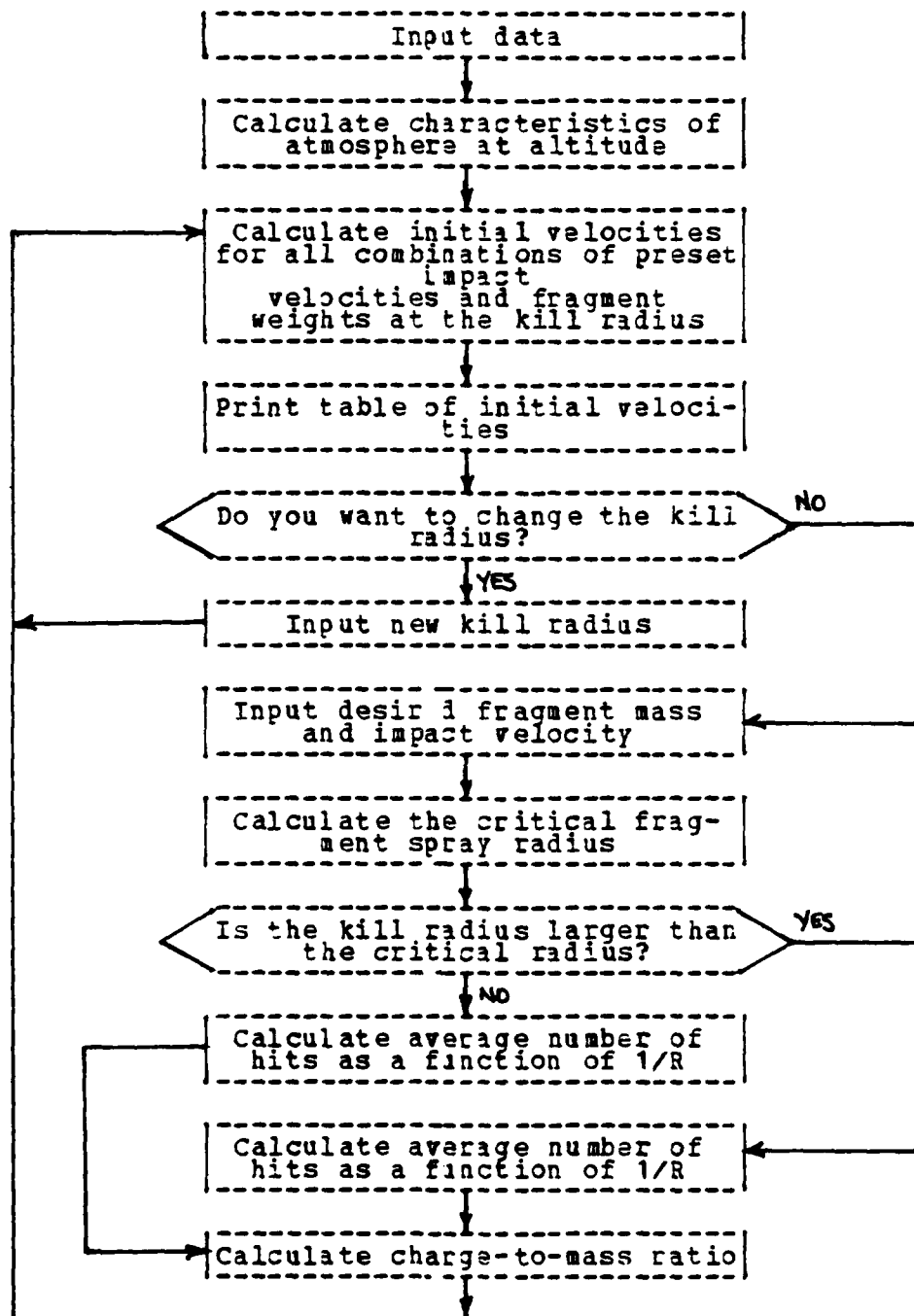
PD	WARHEAD WEIGHT	CASE THICKNESS	CORE DIAMETER	NUMBER	FRAGMENTS ON TARGET	LENGTH
0.999	52.41	0.36	8.92	1306.57	66.54	0.24
0.990	40.00	0.32	9.10	871.07	44.36	0.26
0.980	35.87	0.30	9.16	739.97	37.69	0.26
0.950	30.03	0.27	9.25	566.66	28.86	0.27
0.900	25.20	0.25	9.33	435.55	22.18	0.29

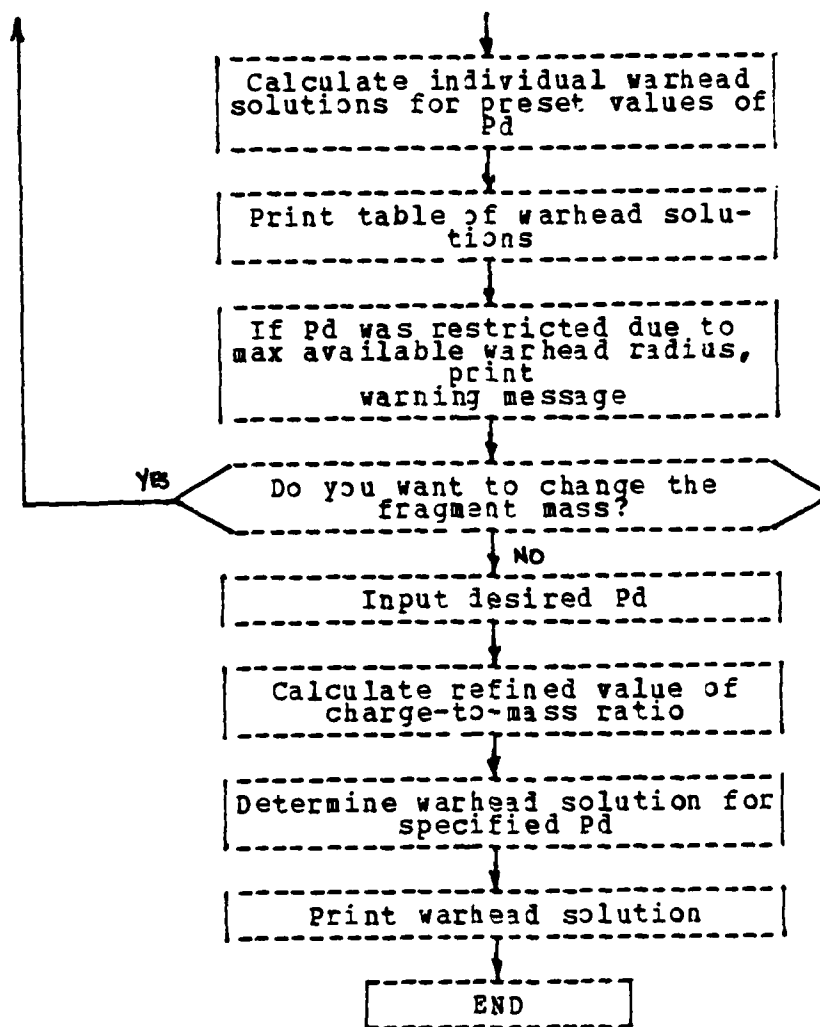
KILL PROBABILITY..... 0.995

WARHEAD DESCRIPTION-----

WARHEAD WEIGHT	43.91 POUNDS
EXPLOSIVE WEIGHT	5.67 POUNDS
CASE WEIGHT	38.24 POUNDS
CASE THICKNESS	0.3322 INCHES
CORE DIAMETER	9.04 INCHES
FRAGMENT WEIGHT	100.00 GRAINS
FRAGMENT DIAMETER	0.250 X 0.332 INCHES
NUMBER OF FRAGMENTS	1002.
NUMBER OF HITS ON TARGET	51.
PROBABILITY OF KILL (PD)	0.995
INITIAL FRAGMENT VELOCITY	3760.3 FT/SEC
CRITICAL MISS DISTANCE	6230.0 FEET

D. PROCEDURAL FLOWCHART





#### IV. PROPULSION MOTOR SIZING

##### A. DESCRIPTION AND ORIGIN OF PROGRAM

This program provides a method for the preliminary sizing of a solid propellant rocket motor for a boost-sustain trajectory of a tactical missile. The analytical method was developed by Redmon [Ref. 1] and was expanded with the addition of material from Platzek [Ref. 2] and Hill [Ref. 3]. The program was written for this thesis in FORTRAN IV for use on the IBM 370 computer system. Essentially, the analysis consists of sizing the booster motor from differential velocity and acceleration requirements with limitations imposed by the physical dimensions of the missile. The booster is at all times considered to be a core-burning motor. The sustainer motor calculations are controlled by the maximum range specified by the user and by the solution of the booster motor. The sustainer can be either a core-burning or an end-burning motor.

The rocket motor configuration is assumed to be either an integral booster-sustainer motor as shown in Figure (IV-1) or a staged motor as in Figure (IV-2). The booster and the sustainer always burn exclusively, or, in other words, one is not burning while the other one is. The nozzle half angle is specified by the user consistent with space available in the missile. If a staged motor is utilized, both nozzles will have the same half angle.

The booster calculations start by determining the amount of thrust needed to boost the total weight of the missile to its cruise velocity at the prescribed acceleration. From this, the necessary amount of propellant is estimated and the process is iterated to account for the decreasing mass situation. The chamber pressure is initially estimated by

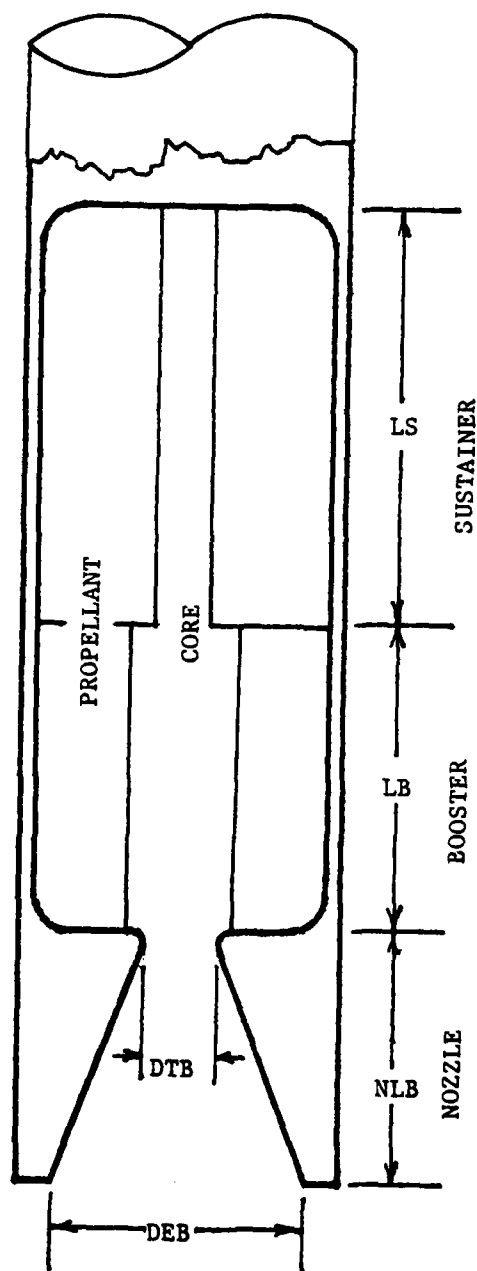


Figure (IV-1). Integral booster-sustainer motor

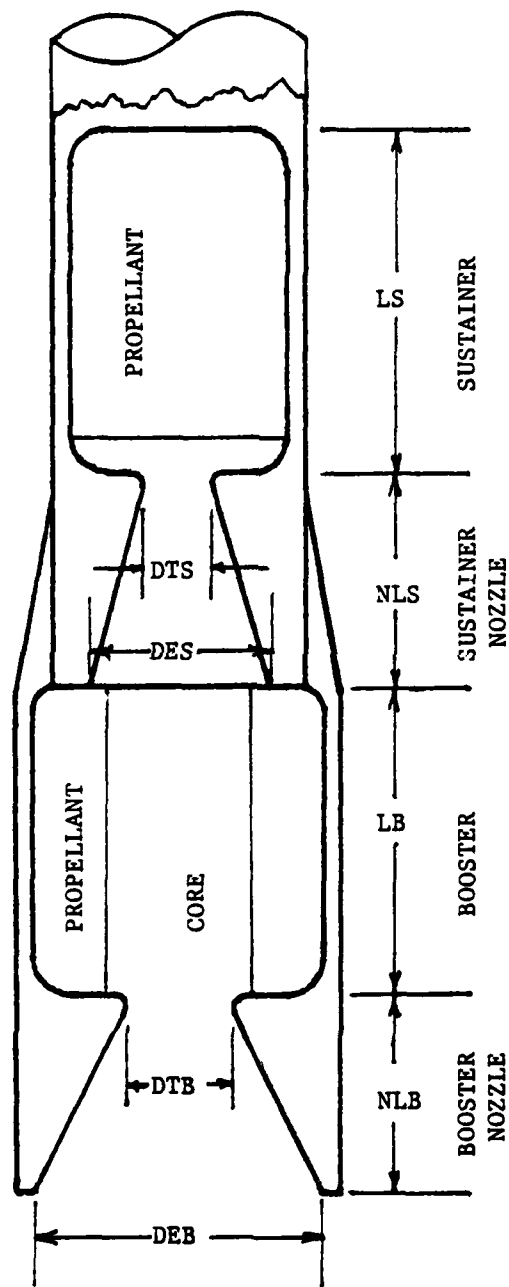


Figure (IV-2). Staged motor

minimizing the motor weight to propellant specific impulse ratio, as presented by Redmon [Ref. 1]. The next step of the program is to size the nozzle using the now known initial pressure ratio. Once the ideal nozzle is developed, the chamber pressure is raised or lowered as necessary in an attempt to cause the nozzle exit diameter to exactly match the booster diameter. However, if the integral motor option is used, the program will drive the nozzle as small as it can without violating one of the following limits in order to increase the probability that the sustainer will operate properly. The iterative process has two limits: an absolute maximum of 2000 PSI chamber pressure [Ref. 2] and a minimum of 1000 PSI if the pressure had previously been higher. The solution can be less than 1000 PSI if the pressure remained below that level throughout the problem. Also limited is the exit pressure to ambient pressure ratio. At the low end, it is limited to 0.4 to prevent flow separation in the nozzle. At the high end, it is limited to 2.5 to prevent excessive underexpansion and loss of physical reality in the program results [Ref. 4]. The burn rate is initialized at a potential maximum of 1.25 inches/second [Ref. 2] and is allowed to decrease to arrive at a compatible burn area and web thickness combination.

The sustainer motor, in the integral motor case, is virtually a continuation of the booster solution. The initial thrust requirement is determined by increasing the cruise speed drag to account for speed loss through maneuvers. It is also then refined for weight change if any climbing or diving is required to reach the target altitude. The nozzle is the same one as developed for the booster except that the throat area will be expanded as a result of the erosion effect. From the new area ratio, a pressure ratio is determined. The chamber pressure and thrust coefficient are then

iterated until a steady chamber pressure evolves to provide the required thrust. If at any time it drops below 125 PSI, the program will stop since this is considered a minimum chamber pressure for proper propellant combustion. The exit pressure to ambient pressure ratio remains subject to the same restrictions. The burn rate starts at 0.45 inches/second [Ref. 2] and is decreased to provide an acceptable web thickness and burn area. The solution can be either an end burner or a core burner, depending on the burn area required.

The sustainer for the staged motor is solved in essentially the same manner as the booster. The two major exceptions are that it can produce an end burner if the burn area is small enough and the thrust required is based on the cruise drag and not the velocity to be gained. The chamber pressure is limited to an absolute maximum of 800 PSI and a minimum of 250 PSI if the pressure had previously been higher [Ref. 2]. The same pressure ratio restrictions apply and the burn rate starts at 0.45 inches/second.

Other motor-nozzle combinations can be created from the results of this program on a first-order approximation basis. Figures (IV-3) and (IV-4) illustrate two possible methods for separating the motor nozzles without resorting to staging. Although these two methods will probably have the same weight disadvantage that staging does, they can be packaged in to a smaller volume of space. A hint for "creative construction" is to rerun the problem after sizing the motors using a smaller missile diameter to force the nozzles to a smaller size.



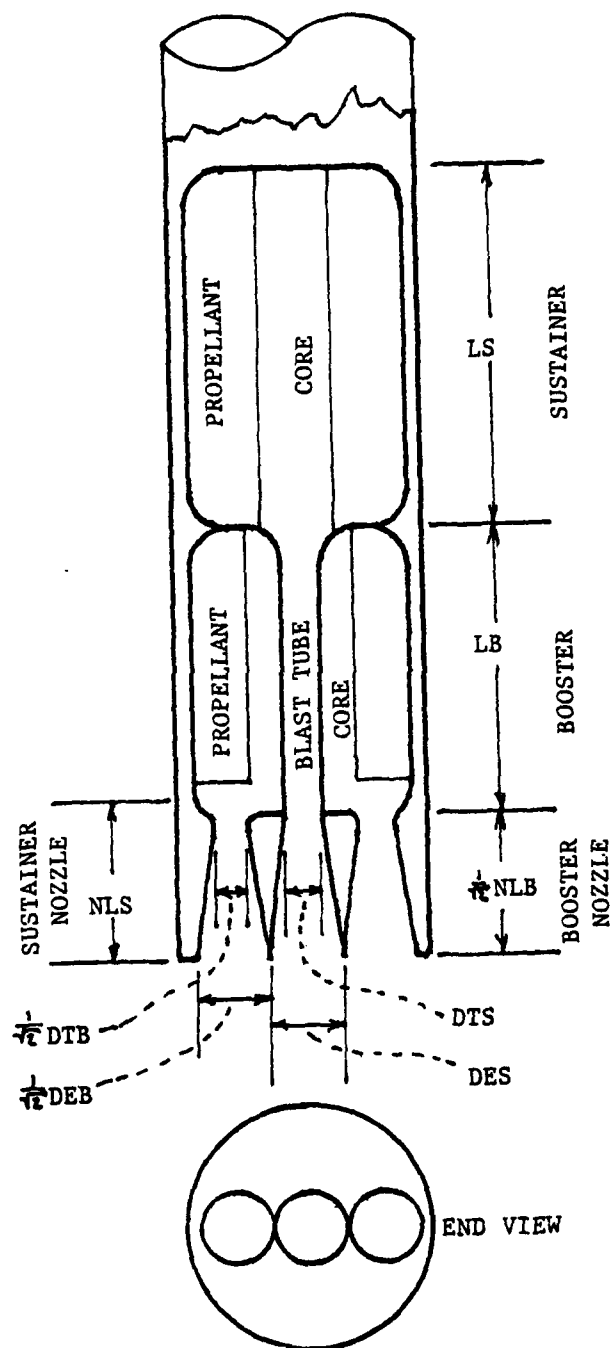


Figure (IV-3). Separate nozzles (nonstaged motors)  
The values are obtained from the staged motor option.

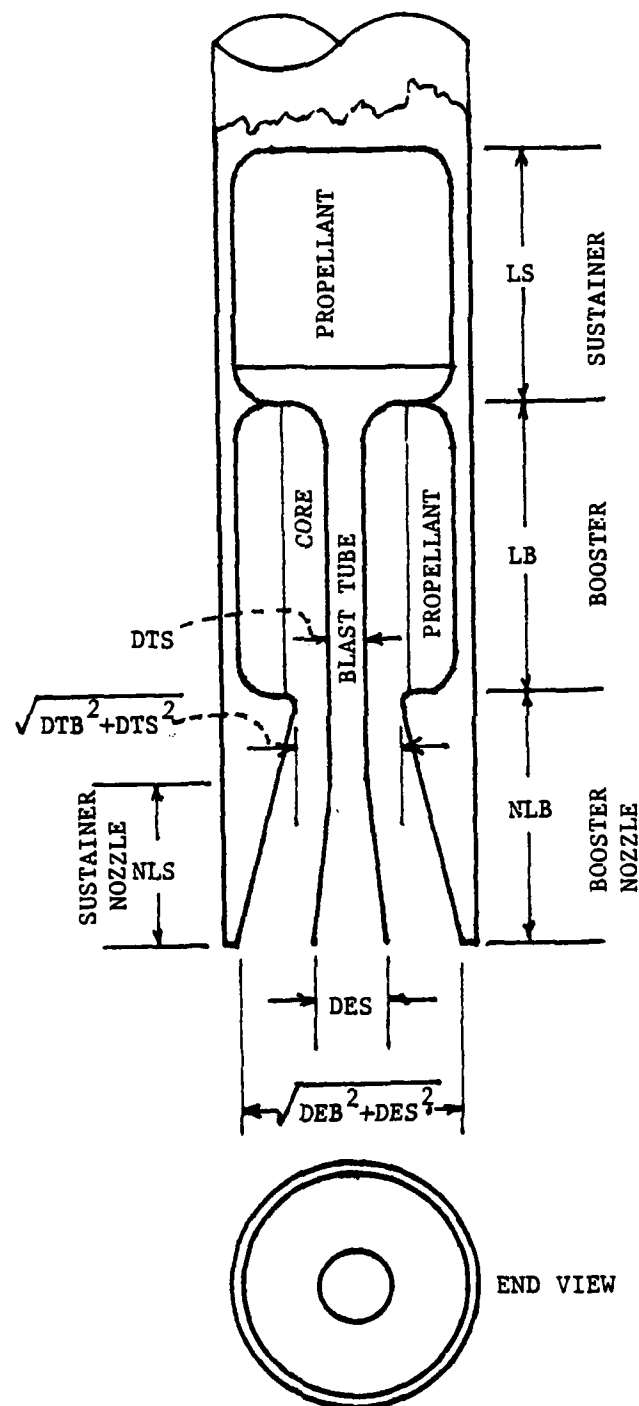


Figure (IV-4). Concentric nozzles (nonstaged motors)  
The values are obtained from the staged motor option.

## B. USER INSTRUCTIONS

If it is desired to abort the operation of this program prematurely, two methods are available. When the program is waiting for data entry, press **ENTER**. When the program is not waiting for data entry but is processing, type "HX" and press **ENTER**. Both actions will return the terminal to CMS mode.

When the screen becomes full, or "MORE...." appears in the status area, clear the screen by pressing **ALT** and **CLEAR** simultaneously. At several points in the program, the user will be directed to "CLEAR SCREEN AND INPUT 0". This is to provide proper positioning of the output on the screen for ease of reading. If any other symbol than "4<sup>A</sup>" should appear in the lower left of the screen, press **RESET** and continue.

1. Turn the terminal on with the red **1**/**0** switch.
2. When the large "NPS" appears after about 30 seconds, press **RESET**, then press **ENTER**.
3. When "CP READ" appears in the status area on the lower right of the screen, type "L nnnnP", where nnnn is your 4-digit user number, then press **ENTER**.
4. You will now be asked for your password. Type it in (the characters will not appear on the screen), then press **ENTER**.
5. Your personal file must contain a PROFILE EXEC routine with the appropriate Fortran GLOBAL statement. If it does not, type "GLOBAL TXTLIB FORTMOD2 MOD2EEH", then press **ENTER**.
6. Type "LINK TO xxxxP 191 AS 192 RR", where xxxx is the 4-digit user number for the project file, then press **ENTER**.
7. You will now be asked for the project file password. Type it in (the characters will not appear on the screen), then press **ENTER**.

8. Type "ACCESS 192 B" and press **ENTER**.
9. Press **ALT** and **CLEAR** simultaneously to clear screen.
10. Type "LPROP" and press **ENTER**.
11. Input the following data as it is requested on the screen by typing the data and then pressing **ENTER**. Ensure that the data is input as either decimal or integer as specified. The terms in parenthesis are the program variable names.

The following variables are required inputs for both motor option problems.

Motor option	(IMOTOR)	0=integral motors 1=staged motors
Launch altitude	(LALT)	feet
Launch weight	(WL)	pounds
Launch velocity	(VBI)	feet/second
Launch elevation angle	(ELB)	degrees
Boost acceleration	(A)	gravities
Cruise velocity	(VBF)	feet/second
Cruise velocity drag	(DRAGS)	pounds
Maximum range to target	(R)	nautical miles
Maximum target altitude	(TALT)	feet
Booster propellant specific impulse	(ISPB)	seconds
Booster propellant density	(DENSB)	pounds/cu. inch
Booster exhaust specific heat ratio	(GB)	
Sustainer propellant specific impulse	(ISPS)	seconds
Sustainer propellant density	(DENSS)	pounds/cu. inch
Sustainer exhaust specific heat ratio	(GS)	
Nozzle half angle	(ALN)	degrees

The following variables are required inputs for the integral motors option only.

Nozzle design altitude	(ALTCN)	feet
Nozzle erosion rate	(ER)	inches/second
Missile diameter	(DB)	inches
Case yield strength	(YIELD)	PSI
Case density	(DENSE)	pounds/cu. inch

The following variables are required inputs for the staged motors option only.

Booster design altitude	(ALTCN)	feet
Booster diameter	(DB)	inches
Booster case yield strength	(YIELD)	PSI
Booster case density	(DENSE)	pounds/cu. inch
Sustainer design altitude	(ALTSN)	feet
Sustainer diameter	(D)	inches
Sustainer case yield strength	(YIELD)	PSI
Sustainer case density	(DENSE)	pounds/cu. inch

12. This program will cue the user when the input parameters have dictated a scenario which either cannot be achieved within reality or produce less than optimum requirements on the propulsion system of the missile. They are not definitive and are only intended to make the user aware of a situation which may need correction. The following is a list of available cue messages with short definitions.

"SUSTAINER NOT CALCULATED SINCE THE BOOSTER BURNOUT RANGE EXCEEDS THE DESIGN RANGE." This can result from entering an extremely short range for the missile, or it can be caused by a very low acceleration requirement.

"SUSTAINER NOT CALCULATED: THE BOOSTER NOZZLE DESIGN PREVENTS SUSTAINER OPERATION. RECOMMEND STAGING OR INDEPENDENT NOZZLES." This occurs only when using the integral motors option. The scenario described to the program can cause the booster nozzle to be too large to

maintain the proper chamber pressures when the motor has shifted to sustainer operation. This usually occurs when a large acceleration is demanded but the thrust required for the cruise trajectory is small.

"BOOSTER BURN RATE WAS ADJUSTED TO CORRESPOND WITH THE WEB THICKNESS." This occurs quite often and simply indicates that the burn rate was decreased from its potential physical maximum of 1.25 inches/second.

"THE BOOSTER NOZZLE DESIGN WAS RESTRICTED DUE TO THE MISSILE DIAMETER," and "THE SUSTAINER NOZZLE DESIGN WAS RESTRICTED DUE TO THE MISSILE DIAMETER." The nozzle was not able to be designed for optimum pressure ratios at the mid point of the boost trajectory. Usually, the exit diameter is solved larger than the missile diameter and is subsequently reduced to fit.

"BOOSTER NOZZLE DESIGN IS NOT OPTIMUM DUE TO EXCESSIVE BOOSTER CHAMBER PRESSURES," and "SUSTAINER NOZZLE DESIGN IS NOT OPTIMUM DUE TO EXCESSIVE SUSTAINER CHAMBER PRESSURES." If the nozzle cannot be downsized without exceeding pressure thresholds (2000 PSI for the booster and 800 PSI for the sustainer), the chamber pressure is held just below the pressure threshold and the nozzle area ratio will be adjusted to allow the nozzle to fit in the missile.

"THE SUSTAINER MOTOR HAS A CORE-BURNING GRAIN." The required burn area for the sustainer was too large to permit an end burning grain with a properly realistic burn rate.

"SUSTAINER BURN RATE WAS ADJUSTED TO CORRESPOND WITH THE WEB THICKNESS." This indicates the sustainer burn rate was lowered from a potential maximum of 0.45 inches/second to provide a proper web thickness.

"THE SUSTAINER MOTOR HAS AN END BURNING GRAIN." The required burn area for the sustainer was small enough to permit an end burning grain. The burn rate is then adjusted to correspond with the nonreduceable burn area.

"REESTIMATION OF LAUNCH WEIGHT IS REQUIRED FOR THESE MISSILE PERFORMANCE PARAMETERS." The scenario described to the program produced a motor whose weight is either larger than 75% of the total or less than 25% of the total.


"ENLARGEMENT OF DIAMETER IS RECOMMENDED DUE TO A VERY HIGH LENGTH-TO-DIAMETER RATIO FOR THE MOTOR." This cue indicates the length-to-diameter ratio is greater than 15. Other components of the missile will make the missile's overall length-to-diameter ratio even larger.

13. Immediately after completion of the solution, the program will ask if you want to receive a hardcopy printout of that particular solution. A "yes" answer stores that solution in a file for retrieval by the user when he finishes with the program.

14. If you desire to rerun the problem, or want to run a new problem, answer the questions appropriately when asked by the terminal after the execution of the current problem.

15. To receive the printout of your encounters, answer "no" to rerunning or restarting the problem when asked by the terminal and follow the directions presented on the screen.

16. Upon completion of the program, type "LOGOFF" and press **ENTER**.

17. Turn the terminal off with the red  switch.

### C. EXAMPLE PROBLEMS

#### 1. Example IV-A. Integral motors, common nozzle

The following parameters are input for the integral motor example:

Launch altitude	35.0 feet
Launch weight	1000.0 pounds
Launch velocity	0.0 feet/second
Launch angle	60.0 degrees
Average acceleration	30.0 g's
Cruise velocity	4000.0 feet/second
Drag at cruise velocity	1500.0 pounds
Maximum range	20.0 miles
Final (target) altitude	50000 feet
Booster propellant specific impulse	260.0 seconds
Booster propellant density	0.075 lbs/cu.inch
Booster exhaust specific heat ratio	1.244
Sustainer propellant specific impulse	210.0 seconds
Sustainer propellant density	0.065 lbs/cu.inch
Sustainer exhaust specific heat ratio	1.270
Nozzle half angle	20.0 degrees
Nozzle design altitude	0.0 feet

TABLE (IV-1). OUTPUT OF EXAMPLE IV-A

INTEGRAL MOTORS (COMMON NOZZLE)		=====	
SUMMARY OF INPUT PARAMETERS		=====	
1) LAUNCH ALTITUDE	35.0	FEET	
2) LAUNCH WEIGHT	1000.00	POUNDS	
3) LAUNCH VELOCITY	0.0	FT/SEC	
4) LAUNCH ANGLE	60.0	DEGREES	
5) AVERAGE ACCELERATION	30.00	G'S	
6) CRUISE VELOCITY	4000.0	FT/SEC	
7) DRAG AT CRUISE VELOCITY	1500.0	POUNDS	
8) MAXIMUM RANGE	20.0	MILES	
9) FINAL (TARGET) ALTITUDE	50000.0	FEET	
10) BOOSTER PROPELLANT SPECIFIC IMPULSE	260.0	SEC	
11) BOOSTER PROPELLANT DENSITY	0.0750	LBS/CU. IN	
12) BOOSTER EXHAUST SPECIFIC HEAT RATIO	1.24400		
13) SUSTAINER PROPELLANT SPECIFIC IMPULSE	0.210.0	SEC	
14) SUSTAINER PROPELLANT DENSITY	0.0650	LBS/CU. IN	
15) SUSTAINER EXHAUST SPECIFIC HEAT RATIO	1.27000		
16) NOZZLE HALF ANGLE	20.00	DEGREES	
17) NOZZLE DESIGN ALTITUDE	0.00100	FEET	
18) NOZZLE EROSION RATE	10.0	IN/SEC	
19) MISSILE DIAMETER	18000.0	INCHES	
20) YIELD STRENGTH OF CASE MATERIAL	0.2662	PSI	
21) DENSITY OF CASE MATERIAL	0.2662	LBS/CU. IN	
=====			
PROPELLANT WEIGHT	800.21	LBS	
CASING WEIGHT	393.21	LBS	
TOTAL WEIGHT	36.95	LBS	
THRUST COEFFICIENT	430.16		
THRUST CHARACTERISTIC VELOCITY	1.6032	FT/SEC	
BURN TIME	5217.7	LBS	
HORIZONTAL BURNOUT RANGE	24669.5	FEET	
CHAMBER BURN PRESSURE	4144.0	PSI	
GRAIN WEB THICKNESS	1999.66	IN	
GRAIN PORT AREA	1590.873	SQ. IN	
REQUIRED BURN RATE	3.296	IN/SEC	
MOTOR CASE LENGTH	9.053	IN	
MOTOR CASE VOLUME	0.7955	CU. IN	
NOZZLE EXIT AREA	6046.29	SQ. IN	
NOZZLE LENGTH	7.695	IN	
NOZZLE THROAT AREA	58.510	SQ. IN	
NOZZLE EXIT AREA	7.557	IN	
NOZZLE LENGTH	38.88	LBS	
NOZZLE THICKNESS	0.05555	IN	
CASE WEIGHT	61.87	LBS	
TOTAL PROPELLANT WEIGHT	646.88	LBS	



TABLE (IV-1). (CONTINUED)

TOTAL ROCKET MOTOR WEIGHT	747.62 LBS
TOTAL ROCKET MOTOR LENGTH	140.74 IN
BOOSTER BURN RATE WAS ADJUSTED TO CORRESPOND WITH THE WEB THICKNESS.	
THE BOOSTER NOZZLE DESIGN WAS RESTRICTED DUE TO THE MISSILE DIAMETER.	
BOOSTER NOZZLE DESIGN IS NOT OPTIMUM DUE TO EXCESSIVE BOOSTER CHAMBER PRESSURES.	
THE SUSTAINER MOTOR HAS A CORE-BURNING GRAIN.	
SUSTAINER BURN RATE WAS ADJUSTED TO CORRESPOND WITH THE WEB THICKNESS.	

Nozzle erosion rate	0.001 inches/second
Missile diameter	10.0 inches
Yield strength of case material	180000.0 PSI
Density of case material	0.2662 lbs/cu.inch

The solution for this problem is presented in Table

(IV-1).

2. Example IV-B. Staged motors, separate nozzles

The following are input for the staged motor problem:

Launch altitude	35.0 feet
Launch weight	2200.0 pounds
Launch velocity	0.0 feet/second
Launch angle	30.0 degrees
Average acceleration	25.0 g's
Cruise velocity	2200.0 feet/second
Drag at cruise velocity	1000.0 pounds
Maximum range	50.0 miles
Final (target) altitude	75000 feet
Booster propellant specific impulse	250.0 seconds
Booster propellant density	.0647 lbs/cu.inch
Booster exhaust specific heat ratio	1.225
Sustainer propellant specific impulse	205.0 seconds
Sustainer propellant density	.0625 lbs/cu.inch
Sustainer exhaust specific heat ratio	1.257
Nozzle half angle	15.0 degrees
Booster design altitude	0.0 feet
Booster diameter	14.5 inches
Yield strength of booster case	180000.0 PSI
Density of booster case material	0.2662 lbs/cu.inch
Sustainer design altitude	0.0 feet

TABLE (IV-2). OUTPUT OF EXAMPLE IV-8

## STAGED MOTORS (INDEPENDENT NOZZLES)

SUMMARY OF INPUT PARAMETERS		=====	
1) LAUNCH ALTITUDE	35.0	FEET	
2) LAUNCH WEIGHT	2200.00	POUNDS	
3) LAUNCH VELOCITY	0.0	FT/SEC	
4) LAUNCH ANGLE	30.00	DEGREES	
5) AVERAGE ACCELERATION	2250.0	G'S	
6) CRUISE VELOCITY	1000.0	FT/SEC	
7) DRAG AT CRUISE VELOCITY	50.	POUNDS	
8) MAXIMUM RANGE	75000.0	MILES	
9) FINAL (TA GET) ALTITUDE	250.0	FEET	
10) BOOSTER PROPELLANT SPECIFIC IMPULSE	0.0647	SEC	
11) BOOSTER PROPELLANT DENSITY	1.22500	LBS/CU.IN	
12) BOOSTER EXHAUST SPECIFIC HEAT RATIO	0.2050	SEC	
13) SUSTAINER PROPELLANT SPECIFIC IMPULSE	0.0625	LBS/CU.IN	
14) SUSTAINER PROPELLANT DENSITY	1.25700	SEC	
15) SUSTAINER EXHAUST SPECIFIC HEAT RATIO	15.00	DEGREES	
16) NOZZLE HALF ANGLE	0.0	FEET	
17) BOOSTER DESIGN ALTITUDE	14.50	INCHES	
18) BOOSTER DIAMETER	180000.0	PSI	
19) YIELD STRENGTH OF BOOSTER CASE	0.2662	LBS/CU.IN	
20) DENSITY OF BOOSTER CASE MATERIAL	0.0	FEET	
21) YIELD STRENGTH OF BOOSTER ALTITUDE	14.50	INCHES	
22) SUSTAINER DIAMETER	180000.0	PSI	
23) YIELD STRENGTH OF SUSTAINER CASE	0.2662	LBS/CU.IN	
24) DENSITY OF SUSTAINER CASE MATERIAL			

PROPELLANT WEIGHT		=====	
CASING WEIGHT	916.16	LBS	
TOTAL WEIGHT	11.82	LBS	
THRUST COEFFICIENT	927.98	LBS	
CHARACTERISTIC VELOCITY	1.2900	FT/SEC	
THRUST	5113.1	LBS	
BURN TIME	1370.9	SEC	
HORIZONTAL PRESSURE	136.997	PSI	
CHAMBER BURN AREA	249.17	SQ.IN	
GRAIN BURN AREA	2472.758	SQ.IN	
GRAIN WEB THICKNESS	5.928	IN	
GRAIN PORT AREA	5.018	SQ.IN	
REQUIRED BURN RATE	0.043	IN/SEC	
MOTOR CASE LENGTH	97.15	IN	
MOTOR CASE VOLUME	15804.59	CU.IN	
NOZZLE THROAT AREA	4.2894	SQ.IN	
NOZZLE EXIT AREA	12.894	SQ.IN	
NOZZLE LENGTH	13.212	IN	

SUSTAINER		=====	
BOOSTER	537.95	LBS	
	59.42	LBS	
	597.37	LBS	
	1.6035	FT/SEC	
	5016.1	LBS	
	49171.0	SEC	
	2.735	FEET	
	2606.7	PSI	
	1998.07	SQ.IN	
	2431.947	IN	
	3.419	SQ.IN	
	18.055	SQ.IN	
	1.250	IN/SEC	
	63.30	IN	
	9641.00	CU.IN	
	15.347	SQ.IN	
	165.068	SQ.IN	
	18.804	IN	

TABLE (IV-2). (CONTINUED)

NOZZLE WEIGHT	33.62 LBS	46.95 LBS
CASE THICKNESS	0.08048 IN	0.01004 IN
TOTAL CASE WEIGHT	71.24 LBS	
TOTAL PROPELLANT WEIGHT	1454.11 LBS	
TOTAL ROCKET MOTOR WEIGHT	1605.93 LBS	
TOTAL ROCKET MOTOR LENGTH	182.47 IN	

THE BOOSTER NOZZLE DESIGN WAS RESTRICTED DUE TO THE MISSILE DIAMETER.  
BOOSTER NOZZLE DESIGN IS NOT OPTIMUM DUE TO EXCESSIVE BOOSTER CHAMBER PRESSURES.

THE SUSTAINER MOTOR HAS A CORE-BURNING GRAIN.

SUSTAINER BURN RATE WAS ADJUSTED TO CORRESPOND WITH THE WEB THICKNESS.

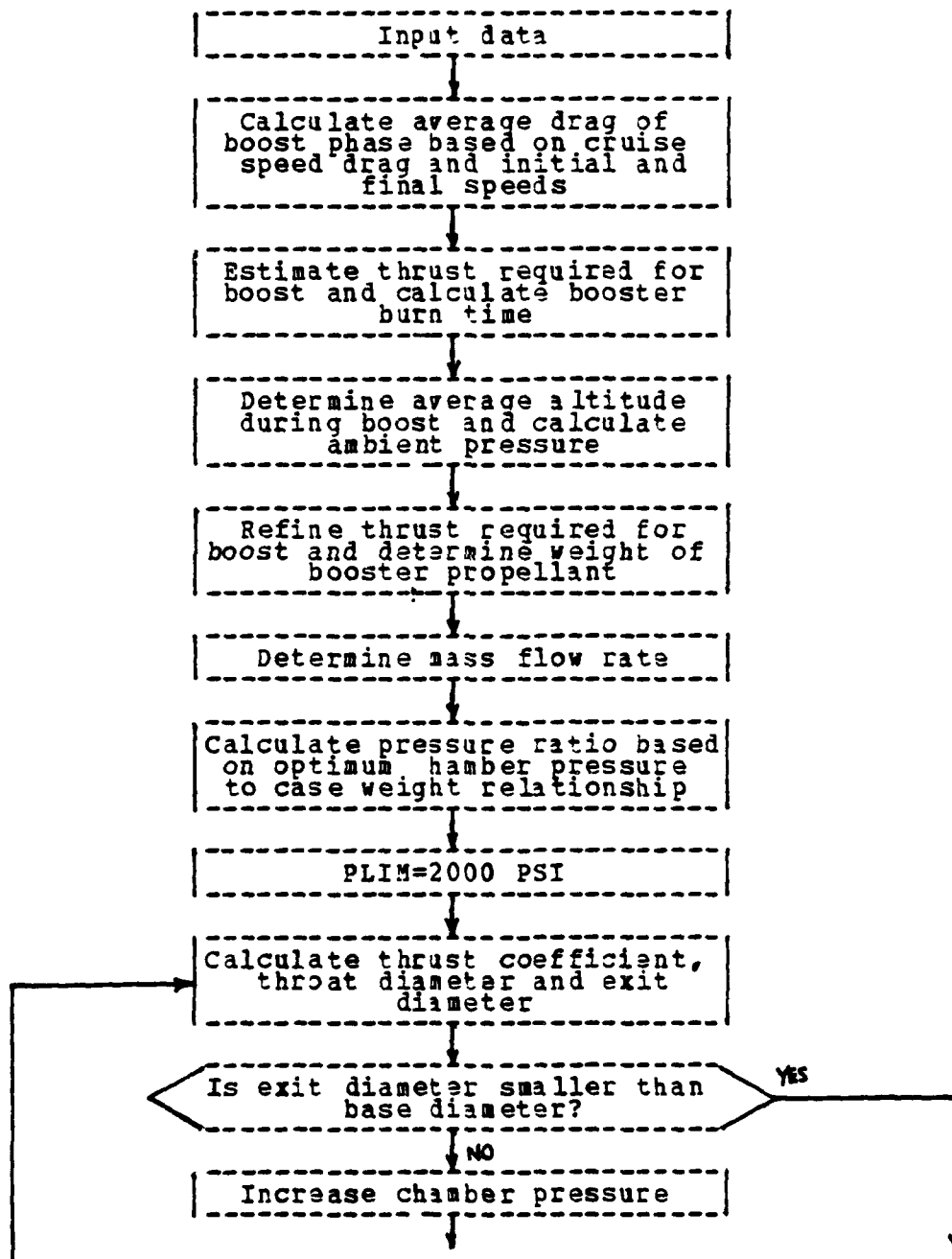
Sustainer diameter 14.5 inches

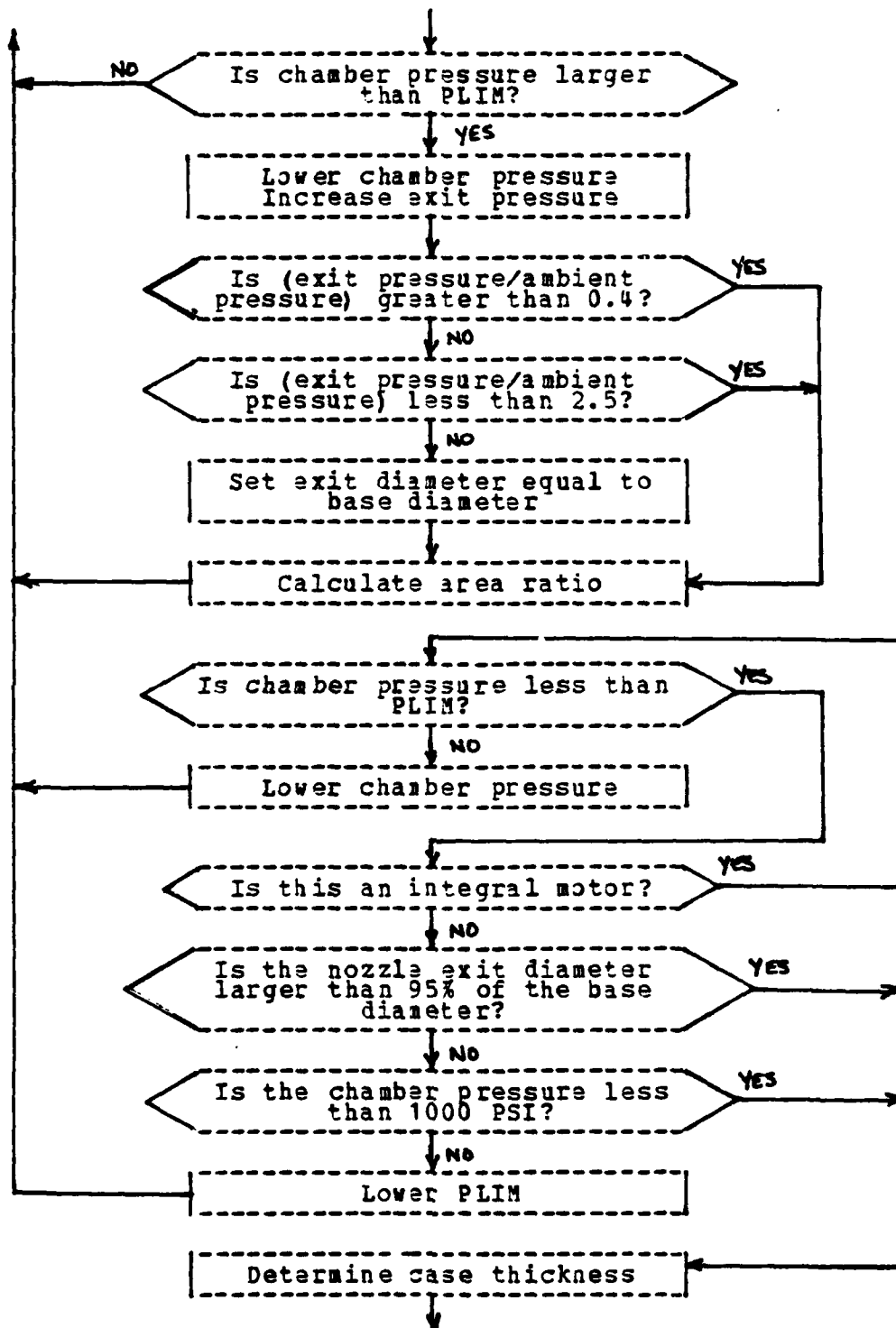
Yield strength of  
sustainer case 180000.0 PSI

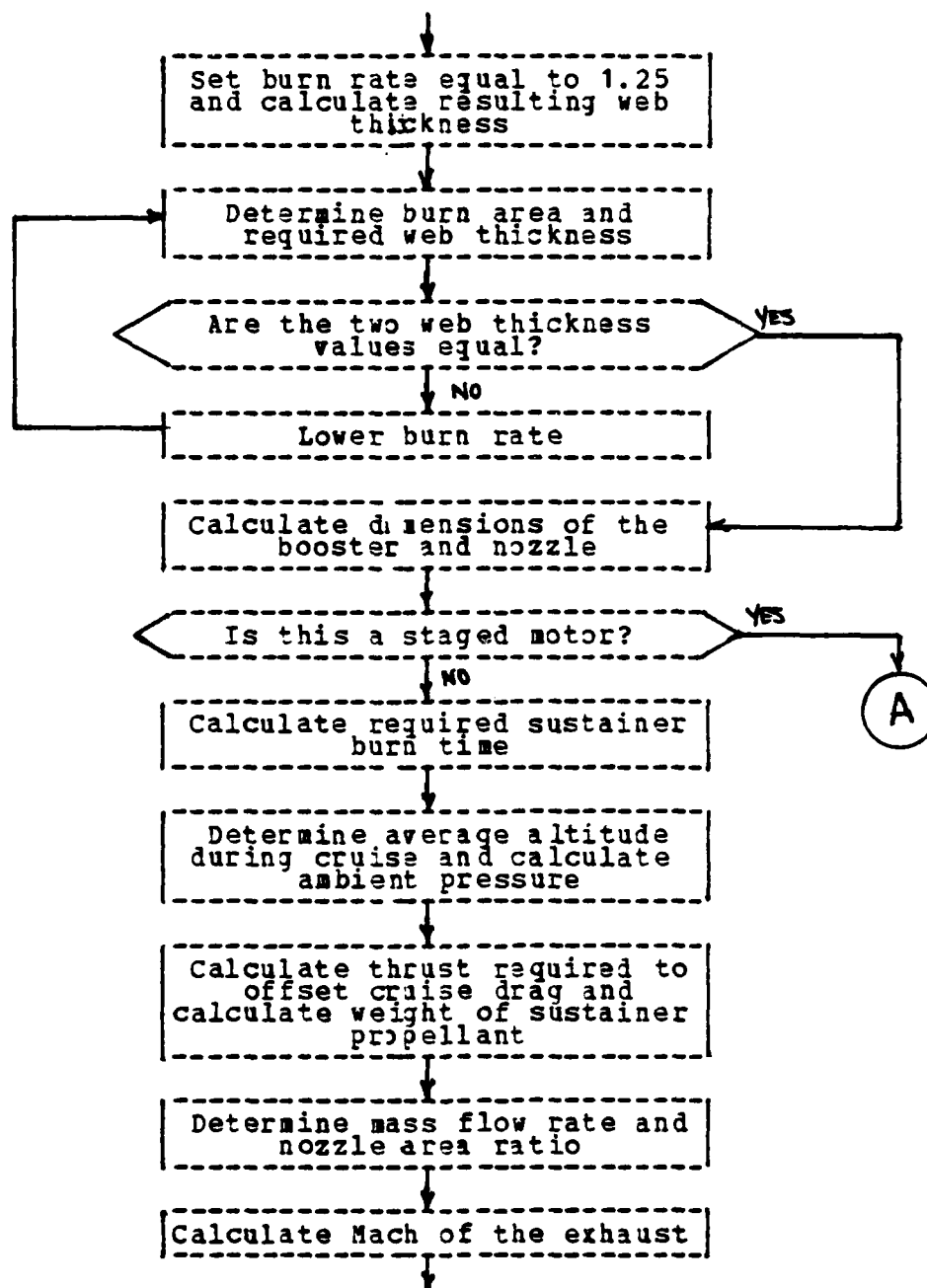
Density of sustainer  
case material 0.2662 lbs/cu.inch

The output for this example is provided in Table  
(IV-2).

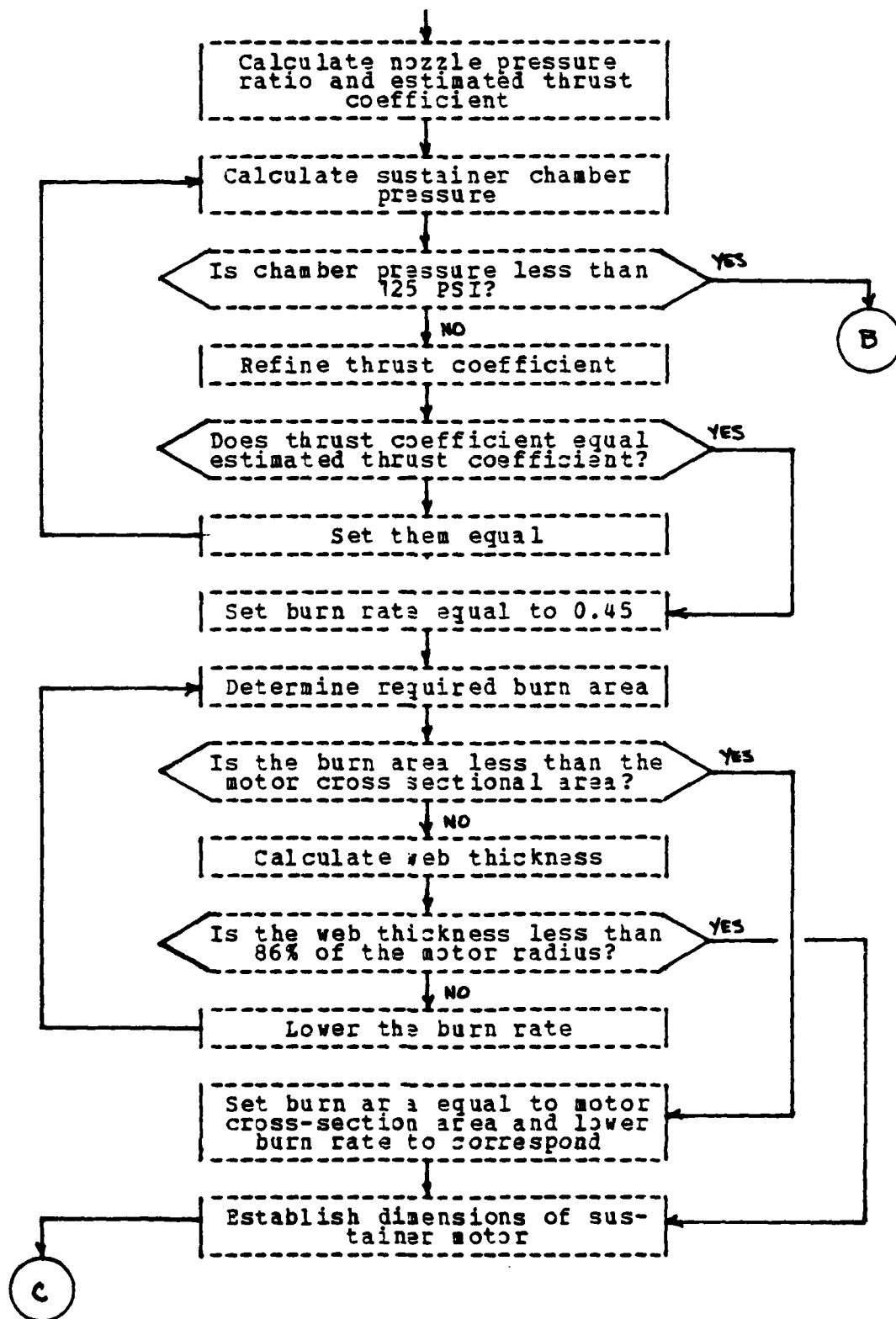
D. PROCEDURAL FLOWCHART

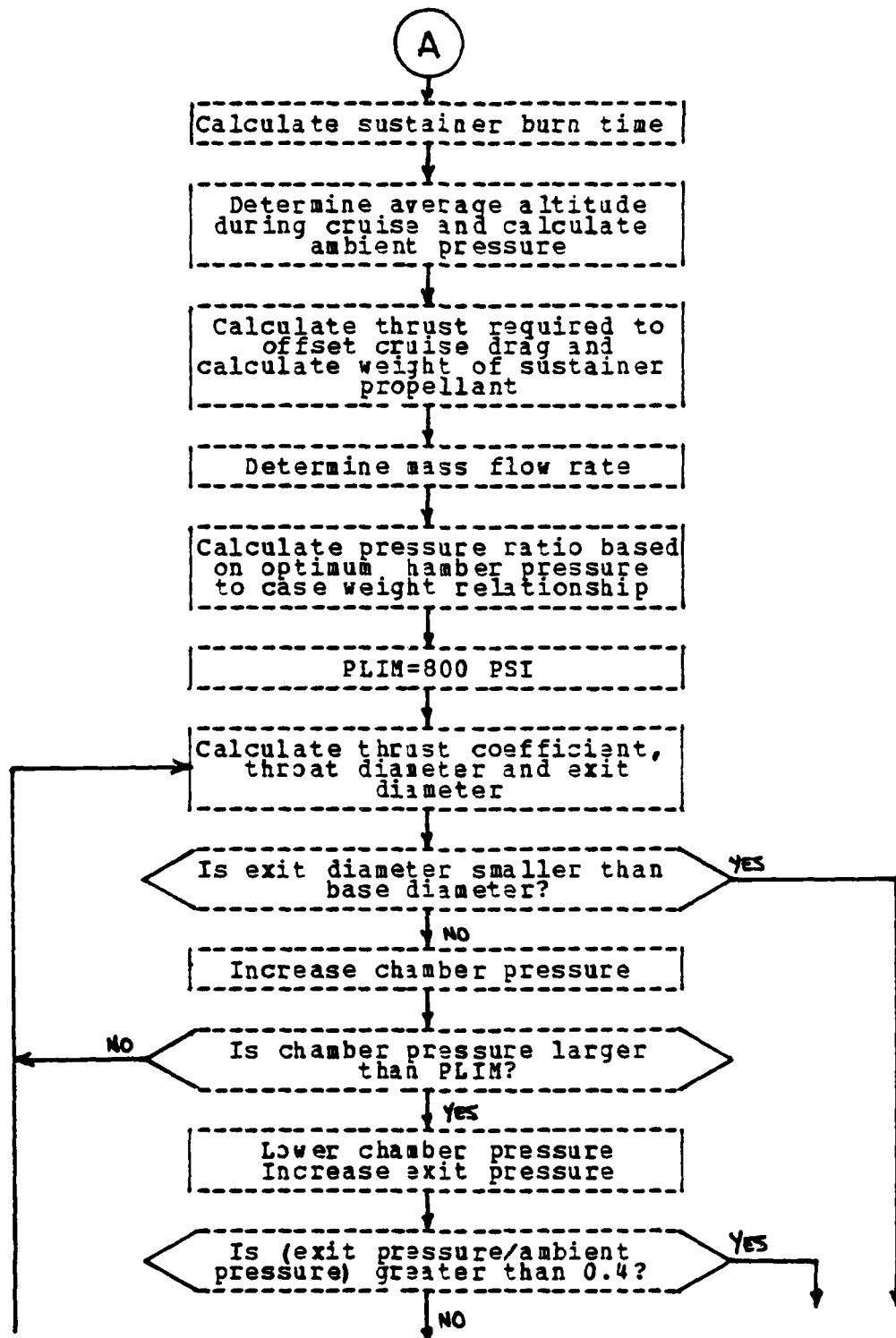


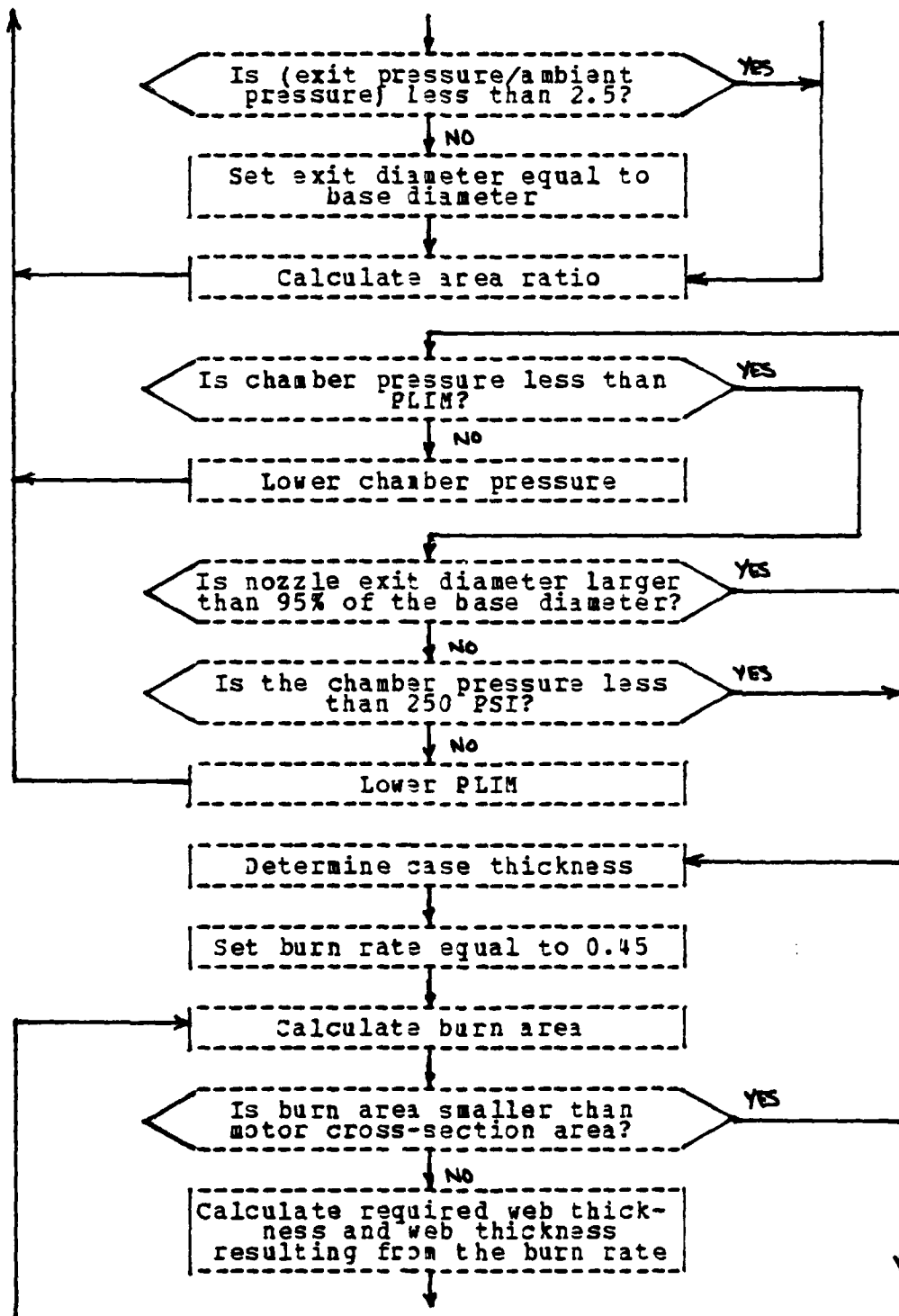


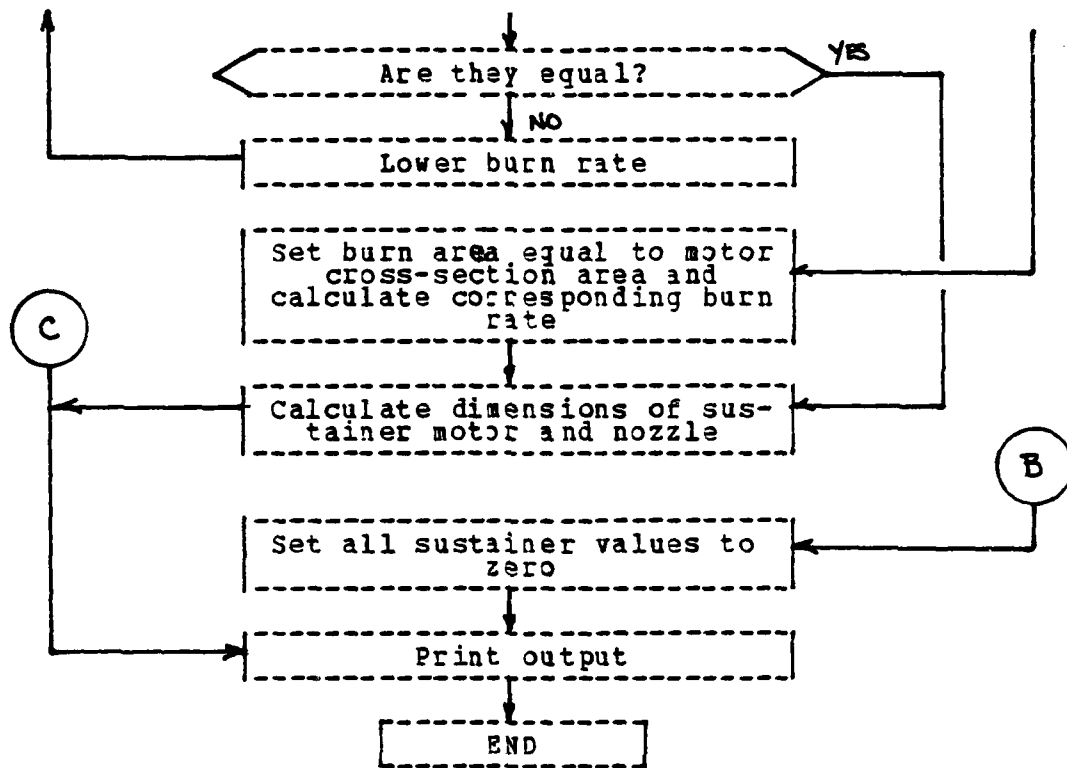












## V. AERODYNAMIC COEFFICIENTS

### A. DESCRIPTION AND ORIGIN

This program is the current edition of a program which originated at the Naval Ship Research and Development Center in 1971 [Ref. 5]. The program was written in FORTRAN II for use on the IBM 7090 digital computer. It was developed as a method for predicting the static, longitudinal aerodynamic characteristics of typical missile configurations with the control surfaces in a "plus" attitude. The original program computed the aerodynamic characteristics for missiles operating at angles of attack up to 180 degrees. The effects of control surface deflections for all modes of aerodynamic control are taken into account. The method was based on the then well known linear, nonlinear crossflow and slender body theories with empirical modifications to provide the high angle of attack capability.

The program was modified and, presumably, updated in 1974 by F. A. Kuster, Jr., of the Naval Air Development Center. In 1980, the program was modified for use on the Naval Postgraduate School IBM 360 computer system by D. Redmon [Ref. 1]. The current version of the program was modified for use on the new Naval Postgraduate School IBM 370 computer system. It has been expanded to provide graphical presentation of the output data.

It must be emphasized at this point that the current program edition is not in a completely finished state. Somewhere in the history of the program after its initial establishment on the IBM 360, errors were introduced during the modifications. At present, these errors do not prevent the use of the program and the output data is considered to be correct for trend-observance purposes.

Specifically, the program does not produce any drag-rise phenomena for either the wings or the tails when  $C_d$  is observed as a function of Mach number. Additionally, the decline of the drag coefficient above Mach 1.0 is not smooth or as prolonged as is found experimentally. It is very probable that these two failings of the program are linked to a common error inserted accidentally in the process of tailoring the program for use on the IBM 370. In order to temporarily smooth over the graphical discontinuities, exponential decay functions were inserted. They are clearly marked in the the program listing for removal when the program is corrected.

The input to the program is composed of a detailed listing of the dimensions of the missile to be analyzed. The current version of the program will consider a missile which has four symmetrical wings and four symmetrical tails. The missile may be either canard or tail equipped and either wing or canard or tail controlled. The program assumes the control surface is the tail, however, the input data is "mislabeled" to produce the proper configuration. For instance, if the missile is a wing control missile, the wing data is input as the tail and the tail data as the wing. For a canard controlled missile, the canard data is input as the tail. Figures (V-1) and (V-3) show two typical missile configurations and where the input parameters for the program are obtained.

#### B. USER INSTRUCTIONS

If it is desired to abort the operation of this program prematurely, two methods are available. When the program is waiting for data entry, press **ENTER**. When the program is not waiting for data entry but is processing, type "HX" and press **ENTER**. Both actions will return the terminal to CMS mode.

When the screen becomes full, or "MORE...." appears in the status area, clear the screen by pressing **ALT** and **CLEAR** simultaneously. At several points in the program, the user will be directed to "CLEAR SCREEN AND INPUT 0". This is to provide proper positioning of the output on the screen for ease of reading. If any other symbol than "**4**<sup>A</sup>**■**" should appear in the lower left of the screen, press **RESET** and continue.

1. Turn the terminal on with the red **!** switch.
2. When the large "NPS" appears after about 30 seconds, press **RESET**, then press **ENTER**.
3. When "CP READ" appears in the status area on the lower right of the screen, type "L nnnnP", where nnnn is your 4-digit user number, then press **ENTER**.
4. You will now be asked for your password. Type it in (the characters will not appear on the screen), then press **ENTER**.
5. Your personal file must contain a PROFILE EXEC routine with the appropriate Fortran GLOBAL statement. If it does not, type "GLOBAL TXTLIB FORTMOD2 MOD2EEH", then press **ENTER**.
6. Type "LINK TO xxxxP 191 AS 192 RE", where xxxx is the 4-digit user number for the project file, then press **ENTER**.
7. You will now be asked for the project file password. Type it in (the characters will not appear on the screen), then press **ENTER**.
8. Type "ACCESS 192 B" and press **ENTER**.
9. Press **ALT** and **CLEAR** simultaneously to clear screen.
10. Type "LAERO1" and press **ENTER**.
11. Input the following data as it is requested on the screen by typing the data and then pressing **ENTER**. Ensure

that the data is input as either decimal or integer as specified. The terms in parenthesis below are the program variable names.

Input the following as integer values unless otherwise noted. The integers must be two digit integers (three=03).

Control constant (ICSC)	01-Tail control 02-Wing control 03-Canard control
Nose shape (INOSE)	01-Ellipsoid 02-Ogive 03-Cone
Number of control deflections (IDT)	Less than 11 You will now be asked for the control deflections in degrees, decimal values.
Number of Mach numbers (IM)	Less than 25 You will now be asked for the Mach numbers, decimal values. Each Mach number will produce a separate table and plot of output data.
Number of angles of attack (IAL)	Less than 25 You will now be asked for the angles of attack in degrees, decimal values.
Number of configurations (NBODY)	No restrictions Each configuration will restart the program. Only the last configuration will produce the written output.
Wing planform (ISWPW)	01-Not delta 02-Delta
Wing position (IAFBW)	00-Body after wing 01-No body after wing
Wing sweep constant (ISWEPW)	00-Delta planform or Unswep leading edge 01-Swept leading edge
Number of wings (NWIN)	04
Tail planform (ISWPT)	01-Not delta 02-Delta
Tail position (IAFBT)	00-No body after tail 01-Body after tail
Tail sweep constant (ISWEPT)	00-Delta planform or Unswep leading edge 01-Swept leading edge
Number of tails (NTAIL)	04

Input the following values as decimal numbers:

Wing tip-to-chord ratio (XLAMW)	
Wing leading edge sweep (CLAMW)	Degrees




Wing span including body (BW)	Feet
Wing root chord (CROOTW)	Feet
Exposed wing area, 2 panels (SW)	Square feet
Wing mean geometric chord (XMACW)	Feet
Distance from nose to wing leading edge (XWING)	Feet
Wing thickness-to-chord ratio (TOVCW)	
Tail tip-to-chord ratio (XLANT)	
Tail leading edge sweep (CLANT)	Degrees
Tail span including body (BT)	Feet
Tail root chord (CROOTT)	Feet
Exposed tail area, 2 panels (ST)	Square feet
Tail mean geometric chord (XMACT)	Feet
Distance from nose to tail leading edge (XTAIL)	Feet
Tail thickness-to-chord ratio (TOVCT)	
Altitude (HT)	Feet
Body diameter (D)	Feet
Missile length (XL)	Feet
Nose length (XLNOSE)	Feet
Distance from nose to CG (XCG)	Feet
Reference area (AREA)	Square feet
Reference length (XREF)	Feet
Engine code (ENGINE)	0.0-Turbofan 1.0-Rocket
Inlet code (ENLET)	0.0-Flush 1.0-Extended
Boat tail angle (BETA)	Degrees
Base diameter (DBASE)	Feet
Nozzle exit diameter (DJET)	Feet
Boat tail length (XLABOD)	Feet
Protuberance drag (CDPROT)	(Coefficient value)
If comparing with experimental values, Reynolds number (REFT)	(Dimensionless)

12. If you desire to rerun the problem, or want to run a new problem, answer the questions appropriately when asked by the terminal after the execution of the current problem.

13. To receive the printout and plot of your encounters, answer "no" to rerunning or restarting the problem when asked by the terminal and follow the directions presented on the screen.

14. Upon completion of the program, type "LOGOFF" and press **ENTER**.

15. Turn the terminal off with the red  switch.

### C. EXAMPLE PROBLEMS

Table (V-5) identifies the output variables as they appear in the output tables.

#### 1. Example V-A. Tail control missile

Figure (V-1) illustrates the missile used in this example. The dimensions for this missile and other input parameters are contained in Table (V-1). The output is shown in Table (V-2) and Figure (V-2).

#### 2. Example V-II. Canard control missile

Figure (V-3) illustrates the canard configuration missile used in this example. The input data is contained in Table (V-3). The output is displayed in Table (V-4) and Figure (V-4).

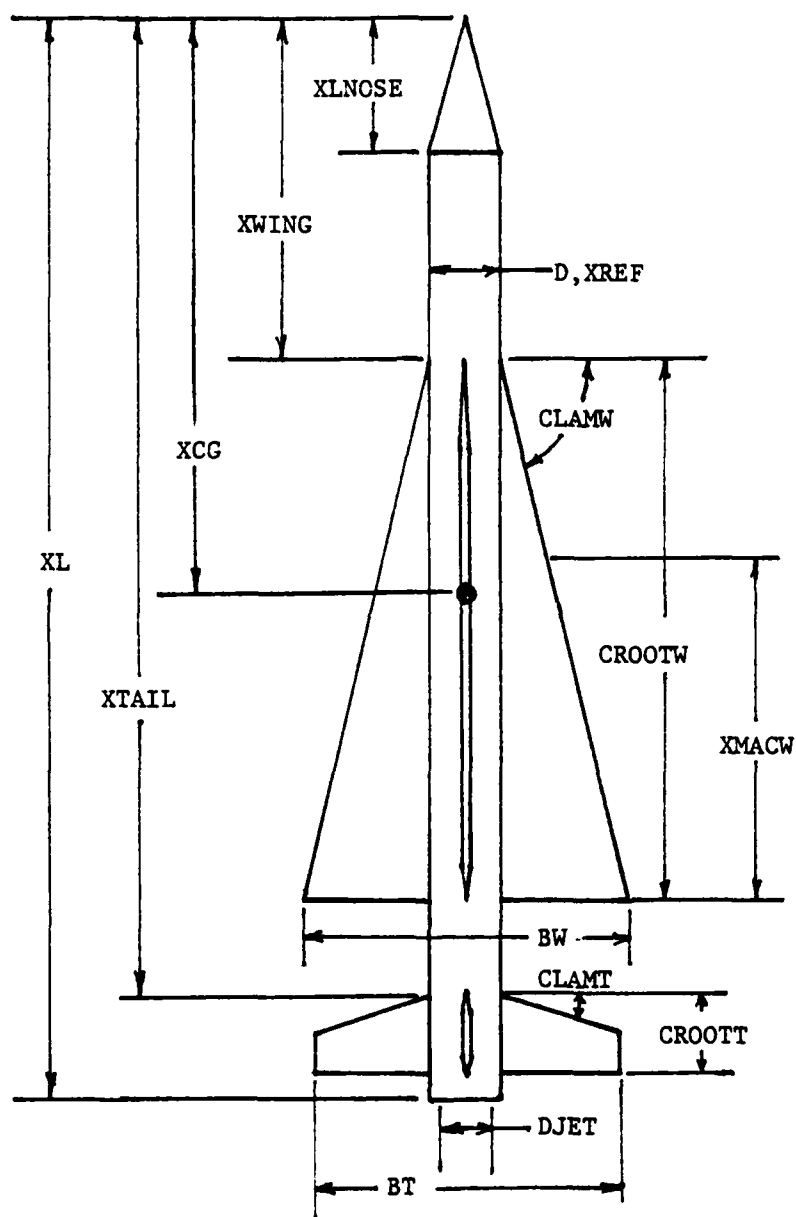


Figure (V-1). Tail control missile as used in Example V-A

THE FOLLOWING TABLE CONTAINS THE INPUT DATA FOR  
EXAMPLE V-A. TAIL CONTROL MISSILE

1)	(ICSC) CONTRL CONSTANT; 1=TAIL, 2=WING, 3=CANARD:	1
2)	(INCSE) NCSE SHAPE; 1=ELLIPSE, 2=OGIVE, 3=CONC:	3
3)	(IDT) NUMBER OF CONTRL DEFLECTIONS:	5
4)	(IM) NUMBER OF 1ACH NUMBERS:	1
5)	(IAL) NUMBER OF ANGLES OF ATTACK:	11
6)	(NBDY) NUMBER OF CONFIGURATIONS:	1
7)	(ISWPW) 1=NON-DELTA WING, 2=DELTA WING:	2
8)	(IAFBW) 0=NO BODY AFTER WING, 1=BODY AFTER WING:	1
9)	(ISWEPW) WING SWEEP CONSTANT (IF DELTA=0) 0=UNSWEPT LEADING EDGE, 1=SWEEP LEADING EDGE:	0
10)	(NWIN) NUMBER OF WINGS:	4
11)	(ISWPT) 1=NON-DELTA TAIL, 2=DELTA TAIL:	1
12)	(IAFBT) 0=NO BODY AFTER TAIL, 1=BODY AFTER TAIL:	1
13)	(ISWPT) TAIL SWEEP CONSTANT (IF DELTA=0) 0=UNSWEPT LEADING EDGE, 1=SWEEP LEADING EDGE:	1
14)	(NTAIL) NUMBER OF TAILS:	4
15)	(XLAMW) TIP-TO-CHORD RATIO OF WING:	0.7
16)	(CLAMW) WING LEADING EDGE SWEEP (DEGREES):	77.000
17)	(BW) WING SPAN, INCLUDING BODY:	1.800
18)	(CRQUTW) WING ROOT CHORD (AT BODY JUNCTION):	2.960
19)	(SW) EXPOSED WING AREA (TWO PANELS):	2.072
20)	(XMACW) WING MEAN GEOMETRIC CHORD:	1.973
21)	(XWING) DISTANCE FROM NOSE TO WING LE:	1.902
22)	(TCVCH) WING THICKNESS TO CHORD RATIO:	0.030
23)	(XLAMT) TIP-TO-CHORD RATIO OF TAIL:	0.609
24)	(CLAMT) TAIL LEADING EDGE SWEEP (DEGREES):	15.000
25)	(BT) TAIL SPAN, INCLUDING BODY:	1.700
26)	(CRQOTT) TAIL ROOT CHORD:	0.400
27)	(ST) EXPOSED TAIL AREA (TWO PANELS):	0.418
28)	(XMACT) TAIL MEAN GEOMETRIC CHORD:	0.328
29)	(XTAIL) DISTANCE FROM NOSE TO TAIL LE:	5.420
30)	(TOVCT) TAIL THICKNESS TO CHORD RATIO:	0.076
31)	(HT) ALTITUDE:	30300.000
32)	(D) BODY DIAMETER:	0.400
33)	(XL) MISSILE LENGTH:	6.000
34)	(XLNOSE) NOSE LENGTH:	0.750
35)	(XCG) DISTANCE TO CG LOCATION FROM NOSE:	3.200
36)	(AREA) REFERENCE AREA:	0.127
37)	(XREF) REFERENCE LENGTH:	0.400
38)	(ENGINE) ENGINE; 0.0=TURBOFAN, 1.0=POCKET:	1.0
39)	(ENLET) INLET; 0.0=FLUSH, 1.0=EXTENDED:	0.0
40)	(BETA) BOAT-TAIL ANGLE (DEGREES):	0.0
41)	(DBASE) BASE DIAMETER:	0.400
42)	(DJET) NOZZLE EXIT DIAMETER:	0.250
43)	(XLABCD) BOAT-TAIL LENGTH:	0.0
44)	(CDPRCT) PROTUBERANCE DRAG:	0.0

MACH	2.000	0.0	0.0	0.0	3.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
DELTA	0.0	4.00	8.00	12.00	16.00	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
ALPHA	0.0	1.00	2.00	3.00	4.00	5.00	6.00	7.00	8.00	9.00	10.00
	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0

Table (V-1). Input data for Example V-A





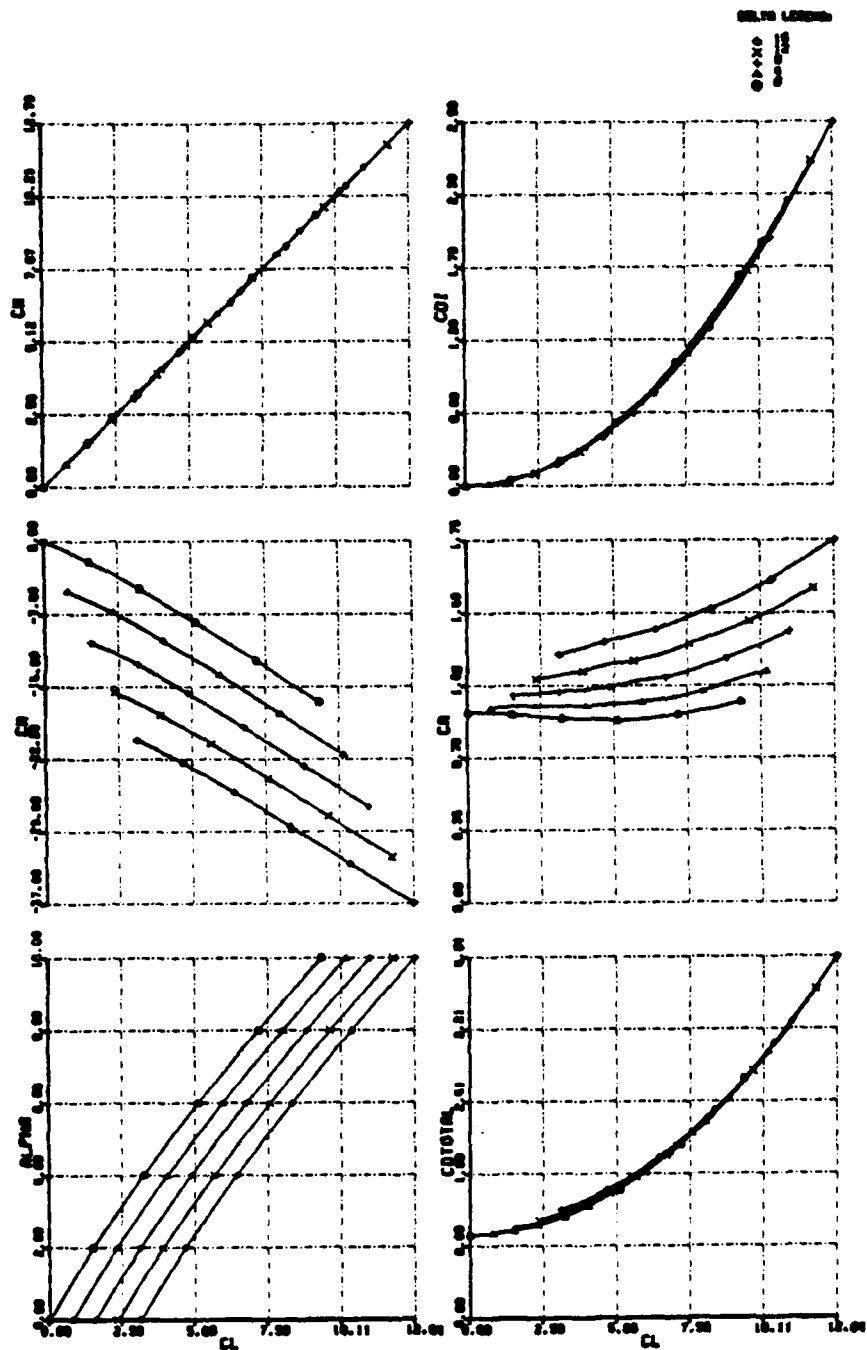


Figure (V-2). Output data plot for Example V-A

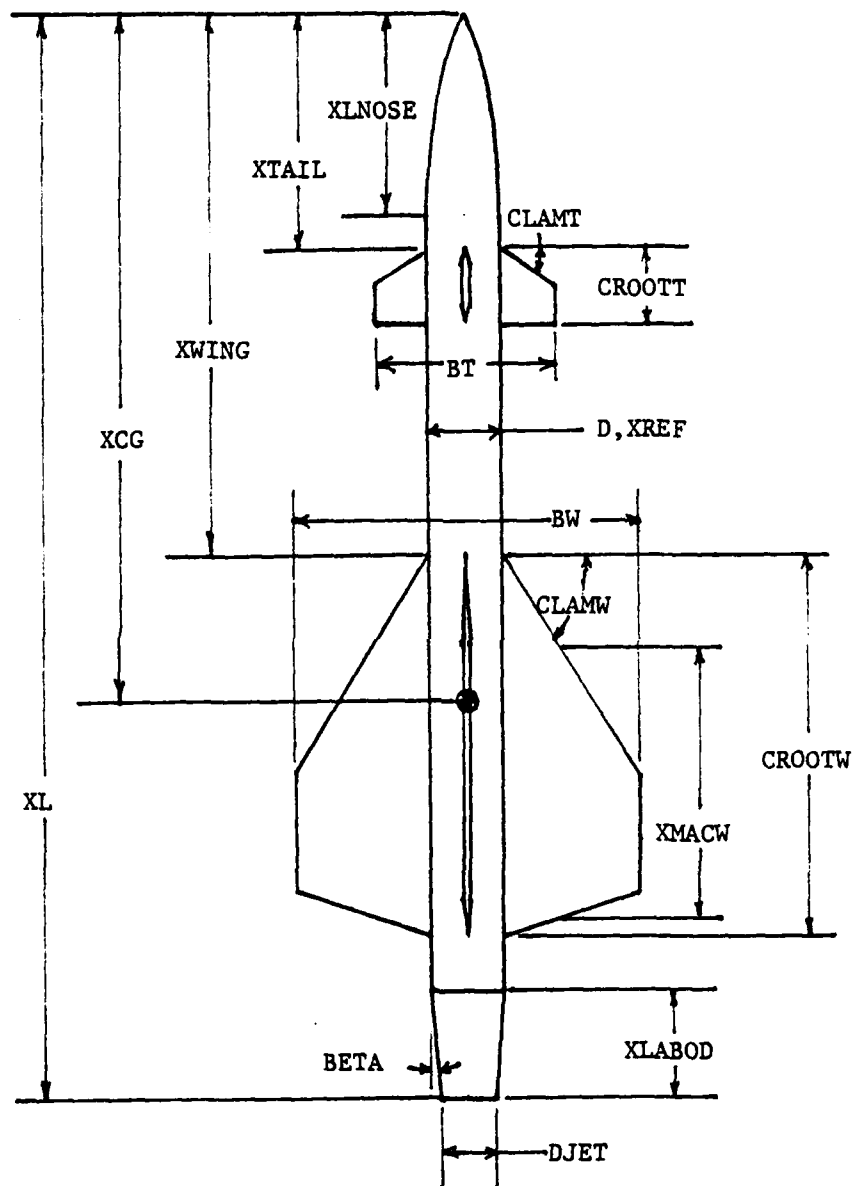


Figure (V-3). Canard control missile for Example V-B



THE FOLLOWING TABLE CONTAINS THE INPUT DATA FOR  
EXAMPLE V-B. CANARD CONTROL MISSILE

1) (ICSC) CONTROL CONSTANT; 1=TAIL, 2=WING, 3=CANARD:	3
2) (INOSE) NOSE SHAPE; 1=ELLIPSE, 2=OGIVE, 3=CONE;	2
3) (IDT) NUMBER OF CONTROL DEFLECTIONS:	5
4) (IM) NUMBER OF MACH NUMBERS:	1
5) (IAL) NUMBER OF ANGLES OF ATTACK:	11
6) (NBDY) NUMBER OF CONFIGURATIONS:	1
7) (ISWPW) 1=NON-DELTA WING, 2=DELTA WING:	1
8) (IAFBW) 0=NO BODY AFTER WING, 1=BODY AFTER WING:	1
9) (ISWEPW) WING SWEEP CONSTANT (IF DELTA=0) 0=UNSWEPT LEADING EDGE, 1=SWEEP LEADING EDGE:	1
10) (INWING) NUMBER OF WINGS:	4
11) (ISWPT) 1=NON-DELTA TAIL, 2=DELTA TAIL:	1
12) (IAFBT) 0=NO BODY AFTER TAIL, 1=BODY AFTER TAIL:	1
13) (ISWPT) TAIL SWEEP CONSTANT (IF DELTA=0) 0=UNSWEPT LEADING EDGE, 1=SWEEP LEADING EDGE:	1
14) (NTAIL) NUMBER OF TAILS:	4
15) (XLAMW) TIP-TO-CHORD RATIO OF WING:	0.314
16) (CLAMW) WING LEADING EDGE SWEEP (DEGREES):	57.500
17) (BW) WING SPAN, INCLUDING BODY:	3.600
18) (CROCTW) WING ROOT CHORD (AT BODY JUNCTION):	4.140
19) (SW) EXPOSED WING AREA (TWO PANELS):	8.070
20) (XMACW) WING MEAN GEOMETRIC CHORD:	2.522
21) (XWING) DISTANCE FROM NOSE TO WING LE:	6.060
22) (TOVCH) WING THICKNESS TO CHORD RATIO:	0.150
23) (XLAMT) TIP-TO-CHORD RATIO OF TAIL:	0.541
24) (CLAMT) TAIL LEADING EDGE SWEEP (DEGREES):	32.000
25) (BT) TAIL SPAN, INCLUDING BODY:	2.000
26) (CROCTT) TAIL ROOT CHORD:	0.614
27) (ST) EXPOSED TAIL AREA (TWO PANELS):	0.566
28) (XMACT) TAIL MEAN GEOMETRIC CHORD:	0.473
29) (XTAIL) DISTANCE FROM NOSE TO TAIL LE:	2.700
30) (TOVCT) TAIL THICKNESS TO CHORD RATIO:	0.085
31) (HT) ALTITUDE:	7000.000
32) (DI) BODY DIAMETER:	0.800
33) (XL) MISSILE LENGTH:	12.000
34) (XLNCS) NOSE LENGTH:	2.200
35) (XCG) DISTANCE TO CG LOCATION FROM NOSE:	7.600
36) (AREA) REFERENCE AREA:	0.503
37) (XREF) REFERENCE LENGTH:	0.900
38) (ENGINE) ENGINE; 0.0=TURBOFAN, 1.0=ROCKET:	1.0
39) (ENLET) INLET; 0.0=FLUSH, 1.0=EXTENDED:	0.0
40) (BETA) BOAT-TAIL ANGLE (DEGREES):	5.000
41) (CBASE) BASE DIAMETER:	0.500
42) (CJET) NOZZLE EXIT DIAMETER:	0.600
43) (XLBCD) BOAT-TAIL LENGTH:	1.200
44) (CDPRCT) PROTUBERANCE DRAG:	0.0

MACH	3.500	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
DELTA	0.0	4.00	8.00	12.00	16.00	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
ALPHA	0.0	1.00	2.00	3.00	4.00	5.00	6.00	7.00	8.00	9.00	10.00
	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0

Table (V-3). Input data for Example V-B





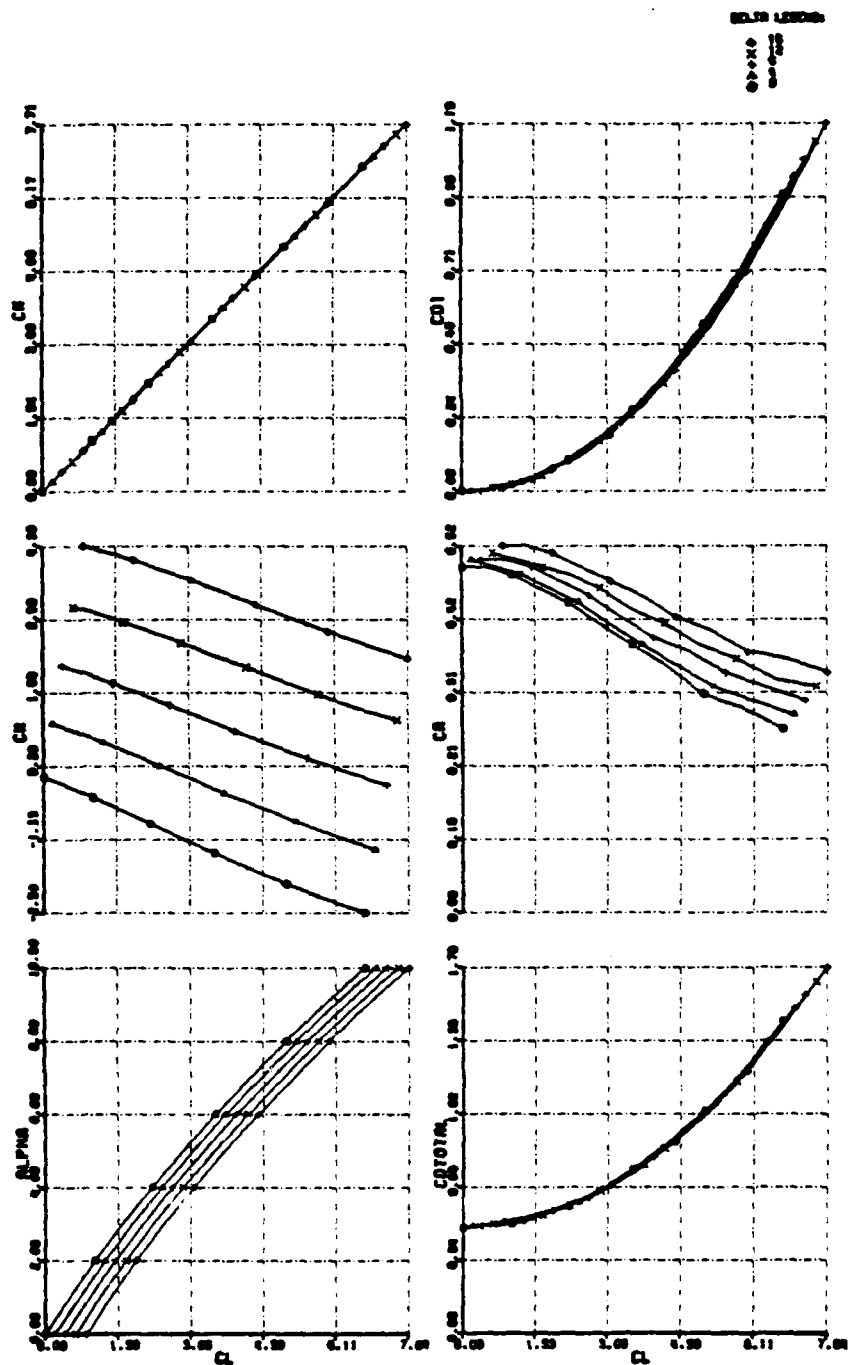


Figure (V-4). Output data plot for Example V-B

Table (V-5). Output variables of LAERO1

AL	Angle of attack
CLTOT	Total coefficient of lift
CDTOT	Total coefficient of drag
CLWP	Wing panel coefficient of lift
CLBW	Additional lift on body due to wing
CLTP	Tail panel coefficient of lift
CLBT	Additional lift on body due to tail
CLB	Body alone lift coefficient
CDI	Induced drag coefficient
CNWP	Wing panel normal force coefficient
CNTP	Tail panel normal force coefficient
CLTD	Lift coefficient due to tail deflection
CDTD	Drag coefficient due to tail deflection
CN	Total normal force coefficient
CA	Total axial force coefficient
XCPW	Wing center of pressure
XCPT	Tail center of pressure
XCP	Total missile center of pressure
CM	Total pitching moment about C.G.
CDOWBT	Zero lift drag coefficient of wing-body-tail combination
CDMISC	Miscellaneous zero lift drag coefficient
CDOT	Zero lift drag coefficient of tail
CDOW	Zero lift drag coefficient of wing
CDOB	Zero lift drag coefficient of body alone
CDPROT	Drag coefficient of body protrusions
CDINL	Drag coefficient of engine inlet
CDAFT	Drag coefficient of boattail region

## VI. CONCLUSIONS AND RECOMMENDATIONS

There are many topics which may be the subjects of follow on work contained within this thesis. Although the four programs have been installed on the IBM 370 computer system, these four alone do not fully satisfy the original goal of this work: Provide a computer supplement to the Tactical Missile Conceptual Design handbook. Numerous additional focal algorithms are utilized in the design handbook which deserve the attention of a programmer. Of immediate interest are the areas concerning radar or infrared guidance systems, baseline configuration modelling and weight distribution, and initial control and lifting surface design. Each of these topics can be programmed to provide missile design students interactive learning tools when coupled with the design handbook.

The most urgent follow on work to this thesis is the restoration of the program LAERO1 to a reliable, useful program. The program was modified and set up on the IBM 370 computer system during the period immediately following the system's installation at the Naval Postgraduate School. As could be expected, the computer suffered many and varied growing pains in its early life. As a result of this, or of the human manipulation expanding the capability of the program, the effectiveness of LAERO1 was substantially reduced.

Work involving the other three programs would involve simply expanding their capabilities. The trajectory models program, LPATH, presently considers only two guidance laws: line-of-sight guidance and proportional navigation guidance. Other guidance laws which can easily be included in the program include pursuit, beam rider, and combinations of different laws. It might also prove useful to be able to

simulate the entire missile trajectory but still only output the terminal phase of the encounter. Another option would be to provide the target with a controlled trajectory instead of the constant acceleration condition now imposed.

The propulsion sizing program, LPROP, should have the various nozzle options incorporated into the program so that it isn't necessary to manually juggle the program output. Other booster-sustainer grain configurations could be explored, such as the booster grain being cast within the core of the sustainer, or even a motor with only a single grain. Another suggestion for the convenience of the program users is to institute a shopping list of available propellants and their characteristics into the program.

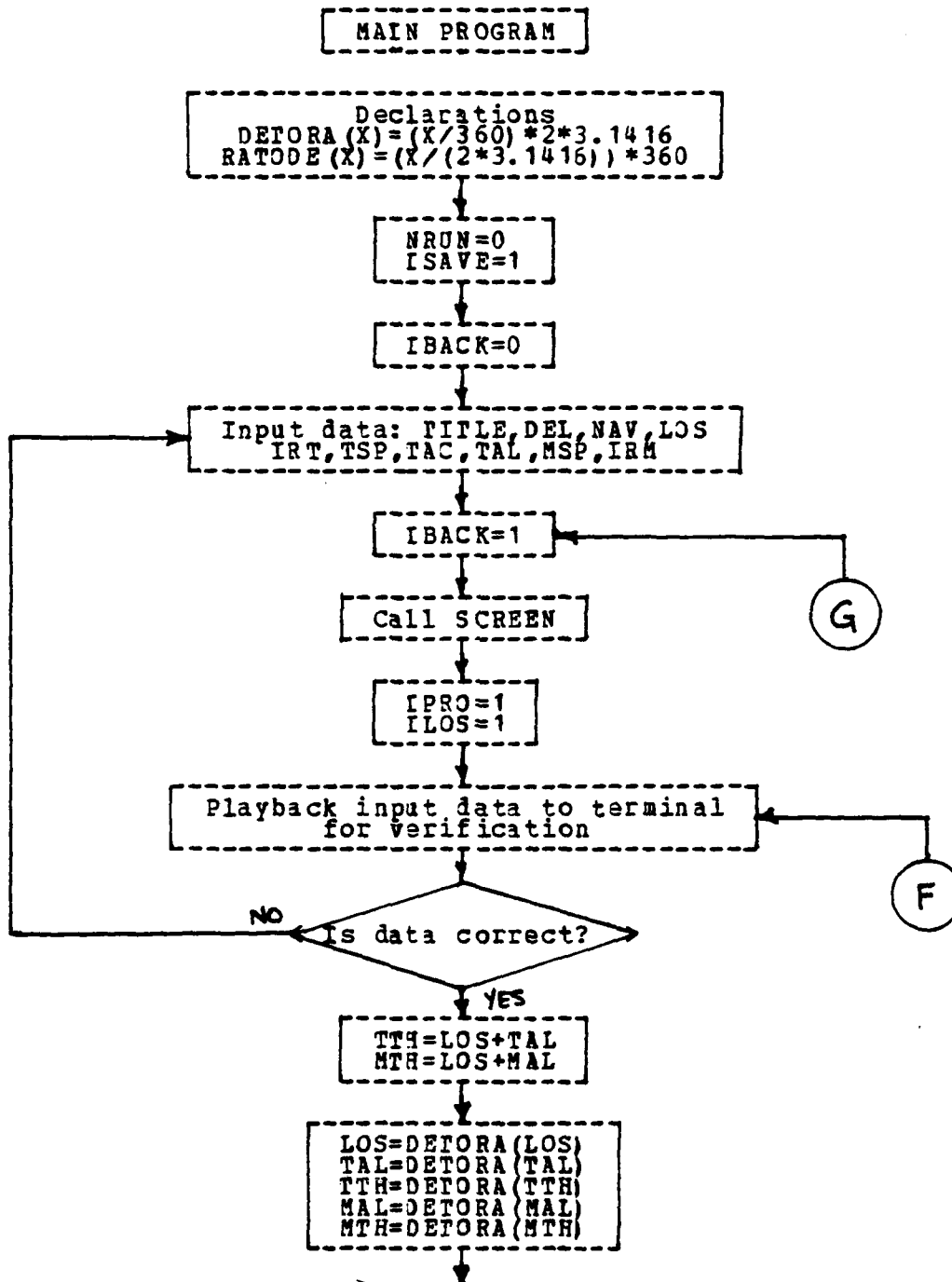
A similar list of available explosives and case materials could be put into the warhead sizing program, LBOMB. These shopping lists would provide ready access to reference information and, at the same time, decrease the number of data values to be manually input into the computer. Since the current program is limited to cylindrical warheads, an area of expansion would be the flexibility of warhead styles, such as curved, shaped charge, continuous rod, etc.

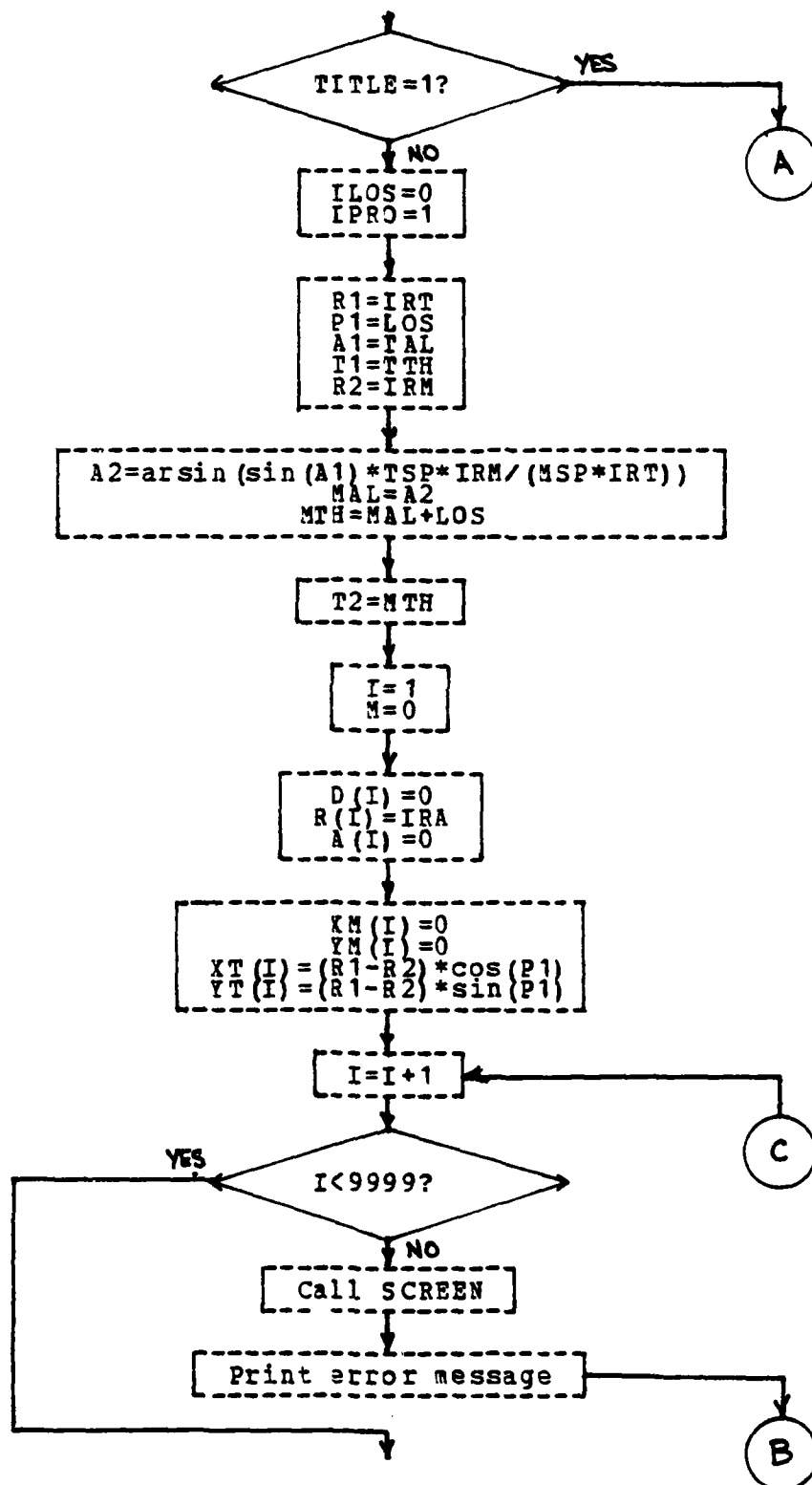
At present, the programs are somewhat hindered by the mechanics involved in producing the printouts and the plots. Due to the results of tailoring a program to be interactive, often it is required to completely exit a program before output can be received. Subsequent design iterations require re-entry into the program, which produces a certain justifiable annoyance to the user. Additionally, the computer center has instituted a new policy of cancelling any jobs with duplicate job names, which can be severely irritating and cumbersome to the persons running the plot routines contained within this thesis. However, the computer center has developed procedures which have the potential to

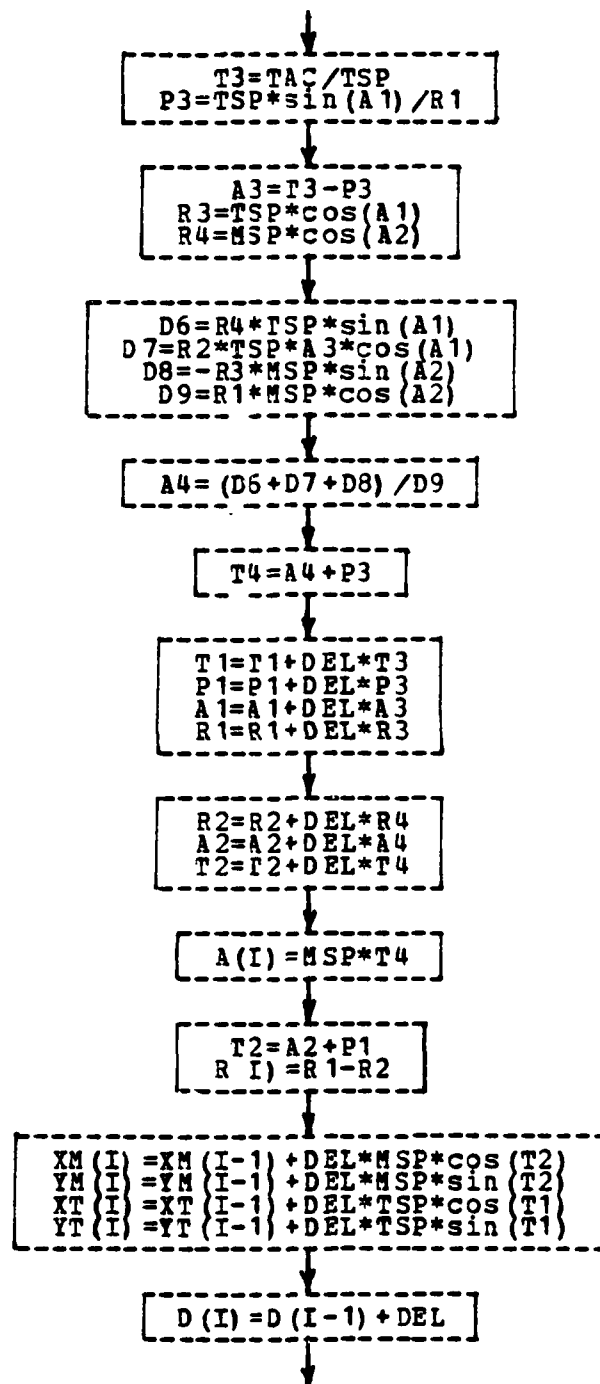
alleviate both of these problems. According to Volume 13, Number 4 of the Computer Center Newsletter, CMS commands can now be invoked from within a FORTRAN program. The print and plot operations presently contained within executive routines can now be placed directly within the source programs. This will remove all current restrictions placed on the numbers of printouts received per session and will label each plot with the user's job name and not the project's job name.

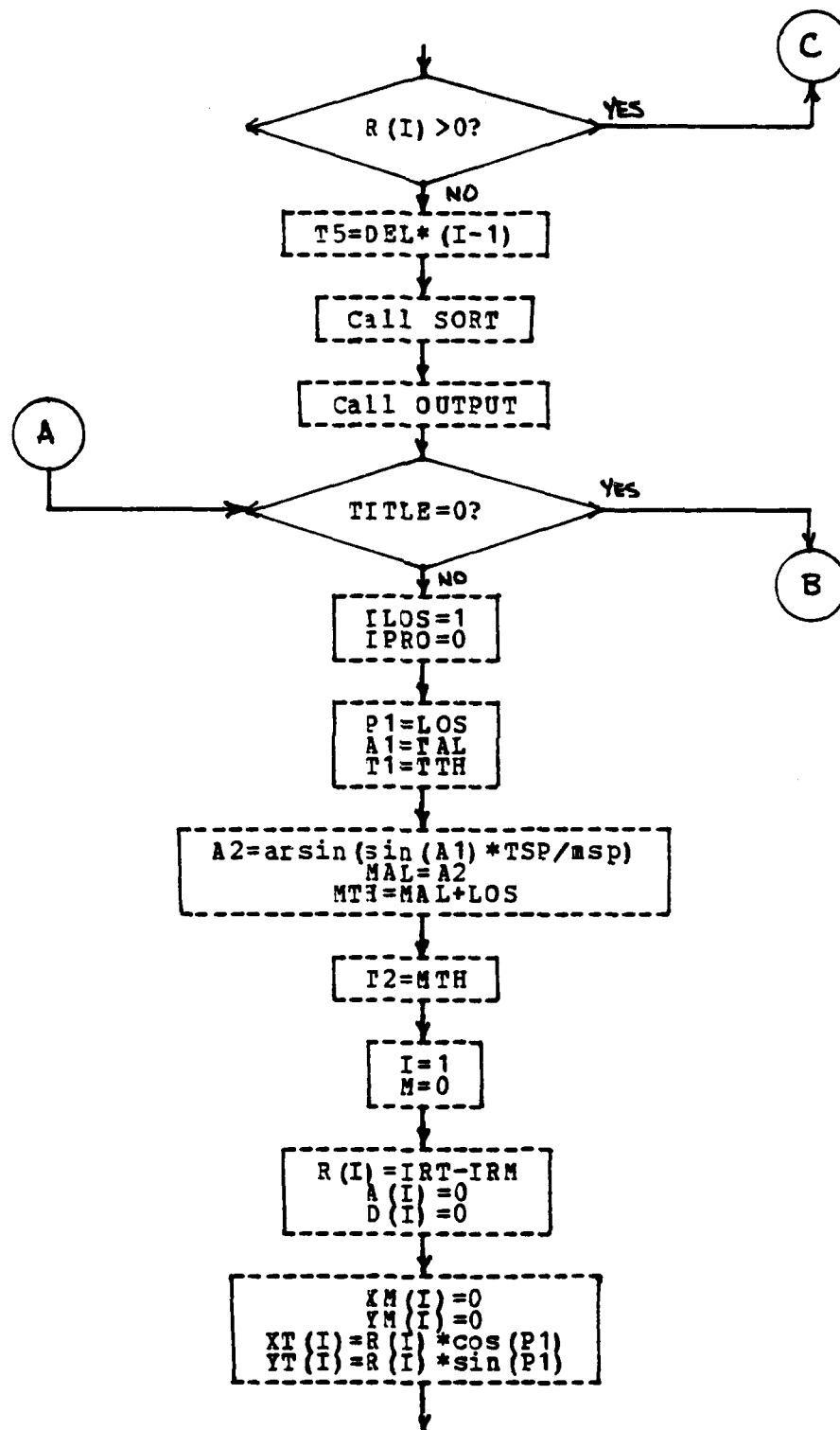


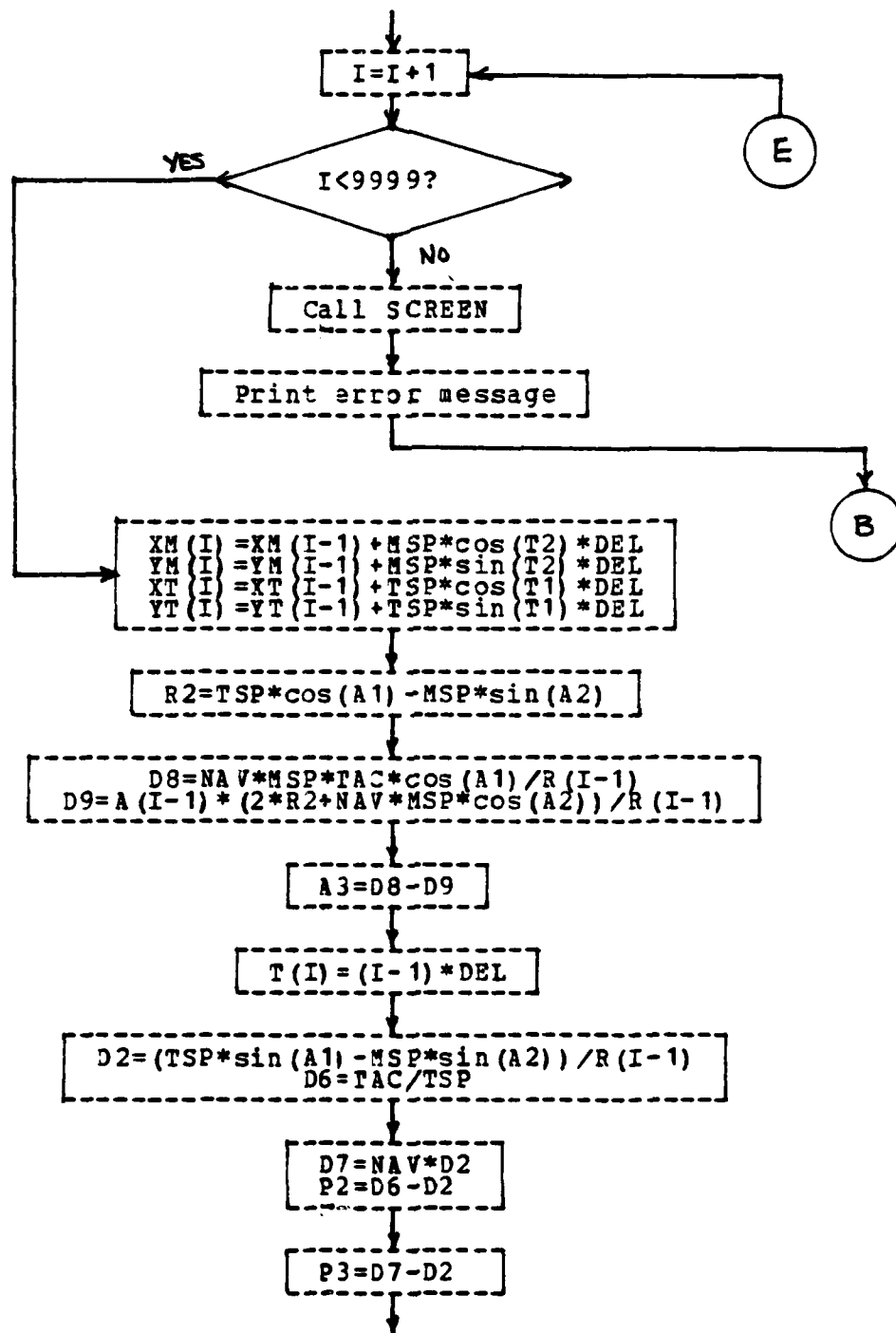
# APPENDIX A. TRAJECTORY MODELS PROGRAM FLOWCHART

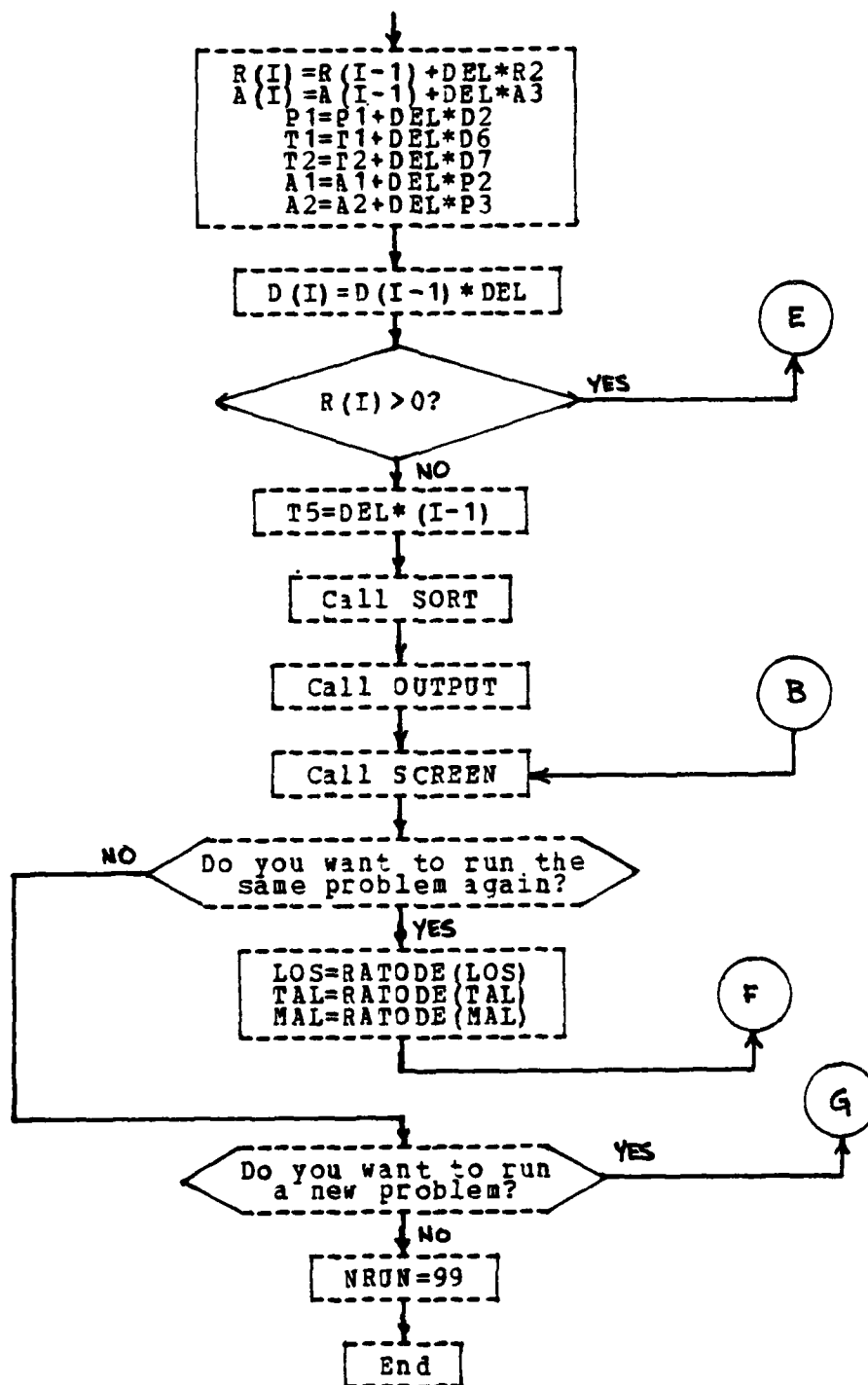












## APPENDIX B. TRAJECTORY MODELS PROGRAM LISTING

Following the next page is the program listing for the Trajectory Models program. It consists of three main divisions; the executive routines, the FORTRAN IV computational program, and the FORTRAN IV plotting program. The executive routines are used to establish required file definitions, initiate operation of the computational program, supervise the transfer of data to the plotting program, and provide operational information to the program user at appropriate times.

The computational program, LPATH FORTRAN, consists of four subprogram divisions. The MAIN program accepts the input data and performs the calculations for the line of sight and the proportional navigation problems. Subroutine SCREEN is used to prompt the user to clear the terminal screen for proper positioning of the output. Subroutine SORT determines the largest missile acceleration value and the value ranges of the X and Y position coordinates for plotting reference. Finally, subroutine OUTPUT formats the calculated data and provides it to the user, the printer file, and the plot program data file.

The plot program, PATHPLOT FORTRAN, is structured for direct submission to the MVS batch reader from the 3278 terminal. No cards need to be punched or read. Attention must be given to the correct JCL accounting data in the first line of the program; those shown in the listing are for illustrative purposes only. This program receives the data from the computational program and produces a single geographic chart of the encounter in the encounter plane. Multiple problems, up to nine, will overlay on the single chart.

FILE: LPATH EXEC A NAVAL POSTGRADUATE SCHOOL

FILEDEF 08 DISK LPATH OUTPUT AO  
FILEDEF 07 DISK PATHPLOT DATA AO  
&BEGTYPE

YOU WILL HAVE THE OPTION TO OBTAIN BOTH A HARDCOPY PRINTOUT  
AND A VERSATEC PLOT OF UP TO NINE ENCOUNTER GEOMETRIES.  
THE PLOT IS A SINGLE FRAME WITH ALL NINE GEOMETRIES  
SUPERIMPOSED ON ONE ANOTHER. THE HARDCOPY PRINTOUT IS  
IDENTICAL IN FORMAT TO THE TERMINAL OUTPUT.

&END  
LOAD LPATH  
START  
&BEGTYPE

TO OBTAIN A HARDCOPY PRINTOUT OF THE RESULTS, TYPE AND  
ENTER:

lpathpr

THE OUTPUT WILL BE PRINTED ON THE VM PRINTER IN ROOM 140  
AND WILL BE IDENTIFIED BY YOUR USER NUMBER. IT USUALLY  
REQUIRES SEVERAL MINUTES TO OBTAIN THE PRINTOUT.

TO OBTAIN THE PLOT OF YOUR ENCOUNTERS, TYPE AND ENTER:

lpathpl

THE PLOT WILL BE PRINTED IN THE COMPUTER ROOM AND WILL BE  
PLACED ON TOP OF THE ALPHABETIZED OUTPUT FILE IN ROOM 140.  
IT WILL BE IDENTIFIED BY THE JCL JOB NAME "PATHPLOT" AND  
USUALLY REQUIRES MANY MINUTES (EVEN HOURS!) TO BE  
OBTAINED. NOTE....IF MANY USERS ARE REQUESTING PLOTS  
SIMULTANEOUSLY, THE COMPUTER CENTER PERSONNEL WILL CANCEL  
"EXCESS" JOBS USING THE SAME IDENTIFIER.

&END

FILE: LPATHPL EXEC A NAVAL POSTGRADUATE SCHOOL

COPY LPATH PLOT A PATHPLOT DATA A PLOT FORTRAN A  
EXEC SUBMIT PLOT FORTRAN A  
ERASE PLOT FORTRAN A

FILE: LPATHPR EXEC A NAVAL POSTGRADUATE SCHOOL

PRINT LPATH OUTPUT (LINECOUN 70



```

C C C C C C C
27 APRIL 1981
THIS PROGRAM COMPARES THE TRAJECTORIES OF TWO GUIDANCE SYSTEM
INTERCEPT GEOMETRIES: LINE OF SIGHT AND PROPORTIONAL
NAVIGATION. THE OUTPUT IS A TABLE OF GEOGRAPHIC POSITIONS, THE
MAXIMUM LATERAL ACCELERATION THE INTERCEPTING MISSILE MUST
ENDURE, AND THE TIME REQUIRED TO MAKE THE INTERCEPT.

DECLARATIONS
REAL DEL, IRT, IRM, LOS, TSP, TAC, TAL, TTH, MSP, MAC, MAL, MTH, NAV
REAL A1, A2, A3, A4, D2, D6, D7, D8, D9, M, M1, P1, P2, P3, R1, R2, R3
REAL R4, T1, T2, T3, T4, T5, T2LAST
INTEGER I, W, TITLE, AGAIN, IBACK, IDO, ISAVE, NRUN, ILOS, IPRO
DIMENSION XM(9999), YM(9999), XT(9999), YT(9999), A(9999), R(9999)
DIMENSION T(9999), RP(9999), D(9999), APN(9999), DT2(9999)
COMMON/BLOCK1/A, X, M, Y, M, XT, YT, M, XPOS, YNEG, I
COMMON/BLOCK2/DEL, NAV, LOS, IRT, IRM, TSP, TAC, TAL, MSP, MAC, MAL, D, R, T5,
* ISAVE, NRUN, ILOS, IPRO
DETORA(X)={X/360}*2*3.1415926535
RATODE(X)={X/(2*3.1415926535)}*360
NRUN=0
ISAVE=1
IBACK=0

1 I BACK=0

C INPUT PROBLEM PARAMETERS
WRITE (6,12)
12 FORMAT (/IX, T13, ' INPUT PROBLEM PARAMETERS')
14 WRITE (6,14)
14 FORMAT (IX, T2, 'FOR LINE OF SIGHT GUIDANCE INTERCEPT TRAJECTORY, INLPA00310
+PUT "0": /, T2, 'FOR PROPORTIONAL NAVIGATION GUIDANCE INTERCEPT TRAJLPA00320
+PECTORY, INPUT "1": /, T2, 'FOR BOTH INTERCEPT TRAJECTORIES, INPUT "2LPA00330
+ (INTEGER).)
READ (6,16) TITLE
16 FORMAT (111)
10001 WRITE (6,15)
15 FORMAT (IX, T2, ' INPUT INTEGRATION TIME INCREMENT (SECONDS, DECIMAL)
*::)
READ (6,117) DEL
117 FORMAT (F10.5)
17 IF (IBACK.EQ.1) GO TO 204
10002 WRITE (6,18)
18 FORMAT (IX, T2, ' INPUT NAVIGATION CONSTANT FOR PROPORTIONAL NAVIGATION
*ON (DECIMAL):)
READ (6,17) NAV
IF (IBACK.EQ.1) GO TO 204
10003 WRITE (6,19)
19 FORMAT (IX, T2, ' INPUT LINE-OF-SIGHT ANGLE (DEGREES, DECIMAL):')
READ (6,17) LOS

```

LPA00040  
 LPA00050  
 LPA00060  
 LPA00070  
 LPA00080  
 LPA00090  
 LPA00100  
 LPA00110  
 LPA00120  
 LPA00130  
 LPA00140  
 LPA00150  
 LPA00160  
 LPA00170  
 LPA00180  
 LPA00190  
 LPA00200  
 LPA00210  
 LPA00220  
 LPA00230  
 LPA00240  
 LPA00250  
 LPA00260  
 LPA00270  
 LPA00280  
 LPA00290  
 LPA00300  
 LPA00310  
 LPA00320  
 LPA00330  
 LPA00340  
 LPA00350  
 LPA00360  
 LPA00370  
 LPA00380  
 LPA00390  
 LPA00400  
 LPA00410  
 LPA00420  
 LPA00430  
 LPA00440  
 LPA00450  
 LPA00460  
 LPA00470  
 LPA00480  
 LPA00490  
 LPA00500  
 LPA00510

AD-A105 788

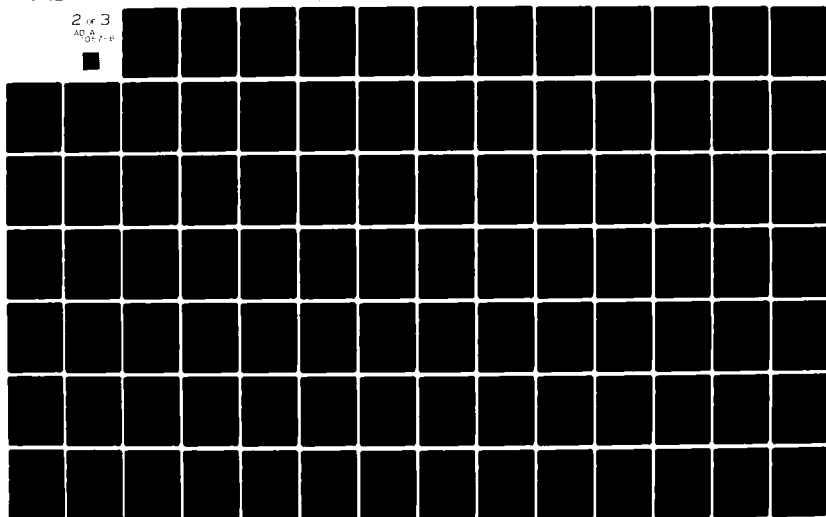
NAVAL POSTGRADUATE SCHOOL MONTEREY CA  
COMPUTER PROGRAM APPLICATIONS TO TACTICAL MISSILE CONCEPTUAL DE--ETC(U)  
JUN 81 M D SULLIVAN

F/G 16/4

UNCLASSIFIED

NL

2 of 3  
AD A  
105 788



```

10004 IF (IBACK.EQ.1) GO TO 204
20 WRITE (6,17) TAC
20 * FORMAT (1X,12,'INPUT TARGET RANGE FROM MISSILE LAUNCH SITE (METERS
    , DECIMAL):')
    READ (6,17) IRT
    IF (IBACK.EQ.1) GO TO 204
10005 WRITE (6,21)
21 * FORMAT (1X,12,'INPUT TARGET SPEED (METERS/SECOND, DECIMAL):')
    READ (6,17) TSP
    IF (IBACK.EQ.1) GO TO 204
10006 WRITE (6,22)
22 * FORMAT (1X,12,'INPUT TARGET LATERAL ACCELERATION (M/SEC/SEC, DECIM
    *AL):')
    READ (6,17) TAC
    IF (IBACK.EQ.1) GO TO 204
10007 WRITE (6,23)
23 * FORMAT (1X,12,'INPUT TARGET ALPHA (DEGREES, DECIMAL):')
    READ (6,17) TAL
    IF (IBACK.EQ.1) GO TO 204
10008 WRITE (6,25)
25 * FORMAT (1X,12,'INPUT MISSILE SPEED (METERS/SECOND, DECIMAL):')
    READ (6,17) MSP
    IF (IBACK.EQ.1) GO TO 204
10009 WRITE (6,26)
26 * FORMAT (1X,12,'INPUT MISSILE RANGE FROM LAUNCH SITE (METERS, DECIM
    *AL):')
    READ (6,17) IRM

C COVER PAGE PRINTOUT
IBACK=1
204 CALL SCREEN
    ILOS=1
    WRITE (6,33)
33 * FORMAT (1X,128,'PROBLEM PARAMETERS')
132 * FORMAT (1X,16,'DELTA NAV LOS, IRT, TSP, TAC, TAL, MSP, IRM
    +T16,'02) NAVIGATION CONSTANT, T39, F10.4, SECONDS',
    +T16,'03) LINE-OF-SIGHT ANGLE, T39, F10.3, DEGREES',
    +T16,'04) TARGET RANGE, T39, F10.3, METERS',
    +T16,'05) TARGET SPEED, T39, F10.3, METERS/SEC',
    +T16,'06) TARGET ACCELERATION, T39, F10.3, M/SEC/SEC',
    +T16,'07) TARGET ALPHA, T39, F10.3, DEGREES',
    +T16,'08) MISSILE SPEED, T39, F10.3, METERS/SEC',
    +T16,'09) MISSILE RANGE, T39, F10.3, METERS',
    WRITE (6,150)
150 * FORMAT (1X,15,'IS THIS DATA SUMMARY CORRECT? (00=YES, IF NO,
    *T15, ENTER THE TWO DIGIT NUMBER OF THE INCORRECT ITEM.

```

LPA00520  
 LPA00530  
 LPA00540  
 LPA00550  
 LPA00560  
 LPA00570  
 LPA00580  
 LPA00590  
 LPA00600  
 LPA00610  
 LPA00620  
 LPA00630  
 LPA00640  
 LPA00650  
 LPA00660  
 LPA00670  
 LPA00680  
 LPA00690  
 LPA00700  
 LPA00710  
 LPA00720  
 LPA00730  
 LPA00740  
 LPA00750  
 LPA00760  
 LPA00770  
 LPA00780  
 LPA00790  
 LPA00800  
 LPA00810  
 LPA00820  
 LPA00830  
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 LPA00850  
 LPA00860  
 LPA00870  
 LPA00880  
 LPA00890  
 LPA00900  
 LPA00910  
 LPA00920  
 LPA00930  
 LPA00940  
 LPA00950  
 LPA00960  
 LPA00970  
 LPA00980  
 LPA00990

```

      *T15, '({TWO-DIGIT INTEGER})')
      READ (6,161)AGAIN
161  FORMAT (112)
      IF (AGAIN.EQ.00) GO TO 205
      GO TO (10001,10002,10003,10004,10005,10006,10007,10008,10009),
      *AGAIN
C
C 205      TTH=LOS+TAL
      MTH=LOS+MAL
      LOS=DETORA(LOS)
      TAL=DETORA(TAL)
      TTH=DETORA(TTH)
      MAL=DETORA(MAL)
      MTH=DETORA(MTH)
C
C      IF (TITLE.EQ.1) GO TO 299
C  LINE OF SIGHT GUIDANCE INTERCEPT TRAJECTORY CALCULATIONS
      ILOS=0
      IPRO=1
C
C  PROGRAM
      R1=IRT
      P1=LOS
      A1=TAL
      T1=TTH
      R2=IRM
      A2=ARSIN(SIN(A1)*TSP*IRM/(MSP*IRT))
      MAL=A2
      MTH=LDS+MAL
      T2=MTH
      I=1
      H=0
      D(I)=0
      R(I)=IRA
      A(I)=0
      XM(I)=0
      YM(I)=0
      XT(I)=(R1-R2)*COS(P1)
      YT(I)=(R1-R2)*SIN(P1)
210  I=I+1
      IF (I.LT.9999) GO TO 211
      CALL SCREEN
      WRITE (6,212)
212  *PROGRAM',IX,'YOU HAVE SUCCESSFULLY EXCEEDED THE CAPABILITY OF THIS
      *ITERATIONS TO COMPLETE

```

LPA01000  
 LPA01010  
 LPA01020  
 LPA01030  
 LPA01040  
 LPA01050  
 LPA01060  
 LPA01070  
 LPA01080  
 LPA01090  
 LPA01100  
 LPA01110  
 LPA01120  
 LPA01130  
 LPA01140  
 LPA01150  
 LPA01160  
 LPA01170  
 LPA01180  
 LPA01190  
 LPA01200  
 LPA01210  
 LPA01220  
 LPA01230  
 LPA01240  
 LPA01250  
 LPA01260  
 LPA01270  
 LPA01280  
 LPA01290  
 LPA01300  
 LPA01310  
 LPA01320  
 LPA01330  
 LPA01340  
 LPA01350  
 LPA01360  
 LPA01370  
 LPA01380  
 LPA01390  
 LPA01400  
 LPA01410  
 LPA01420  
 LPA01430  
 LPA01440  
 LPA01450  
 LPA01460  
 LPA01470

```

*THE SOLUTION./,IX.*IF YOU STRONGLY DESIRE A SOLUTION FOR THIS ENCLPA01480
*OUNTER, INCREASE./,IX.*THE SIZE OF YOUR TIME INCREMENT AND RERUN. LPA01490
* IT IS ALSO STRONGLY RECOMMENDED./,IX.*THAT YOU REVIEW THE GEOMETRLPA01500
*Y OF THE ENCOUNTER TO ENSURE IT IS POSSIBLE./,IX.*FOR THE ENCOUNTERLPA01510
* R TO OCCUR.*/
GO TO 999
211 T3=TAC/TSP
P3=TSP*SIN(A1)/R1
A3=T3-P3
R3=TSP*COS(A1)
R4=MSP*COS(A2)
D6=R4*TSP*SIN(A1)
D7=R2*TSP*A3*COS(A1)
D8=-R3*MSP*SIN(A2)
D9=R1*MSP*COS(A2)
A4=(D6+D7+D8)/D9
T4=A4+P3
T1=T1+DEL*T3
P1=P1+DEL*P3
A1=A1+DEL*A3
R1=R1+DEL*R3
R2=R2+DEL*R4
A2=A2+DEL*A4
T2=T2+DEL*T4
A(I1)=MSP*T4
T2=A2+P1
220 R(I1)=R1-R2
XM(I1)=XM(I-1)+DEL*MSP*COS(T2)
YM(I1)=YM(I-1)+DEL*MSP*SIN(T2)
XT(I1)=XT(I-1)+DEL*TSP*COS(T1)
YT(I1)=YT(I-1)+DEL*TSP*SIN(T1)
D(I1)=D(I-1)+DEL
IF (R(I1).GT.0) GO TO 210
T5=DEL*(I-1)
CALL SORT
CALL OUTPUT
C
C
C 299 IF (TITLE.EQ.0) GO TO 999
C
C PROPORTIONAL NAVIGATION GUIDANCE INTERCEPT TRAJECTORY CALCULATIONS
ILOS=1
I PRO=0
C
C PROGRAM
P1=LOS
A1=TAL
LPA01520
LPA01530
LPA01540
LPA01550
LPA01560
LPA01570
LPA01580
LPA01590
LPA01600
LPA01610
LPA01620
LPA01630
LPA01640
LPA01650
LPA01660
LPA01670
LPA01680
LPA01690
LPA01700
LPA01710
LPA01720
LPA01730
LPA01740
LPA01750
LPA01760
LPA01770
LPA01780
LPA01790
LPA01800
LPA01810
LPA01820
LPA01830
LPA01840
LPA01850
LPA01860
LPA01870
LPA01880
LPA01890
LPA01900
LPA01910
LPA01920
LPA01930
LPA01940
LPA01950

```

```

T1=TTH
A2=ARSIN(SIN(A1)*TSP/MSP)
MAL=A2
MTH=MAL+LOS
T2=MTH
I=1
M=0
R(I)=IRT-IRM
A(I)=MAC
D(I)=0
XM(I)=0
YM(I)=R(I)*COS(P1)
XT(I)=R(I)*SIN(P1)
YT(I)=R(I)*SIN(P1)
I=I+1
310 IF (I.LT.999) GO TO 311
CALL SCREEN
WRITE (6,212)
GO TO 999
311 XM(I)=XM(I-1)+MSP*COS(T2)*DEL
YM(I)=YM(I-1)+MSP*SIN(T2)*DEL
XT(I)=XT(I-1)+TSP*COS(T1)*DEL
YT(I)=YT(I-1)+TSP*SIN(T1)*DEL
R2=TSP*COS(A1)-MSP*COS(A2)
D8=NAV*MSP*TAC*COS(A1)/R(I-1)
D9=A(I-1)*(2*R2+NAV*MSP*COS(A2))/R(I-1)
A3=D8-D9
T(I)=(I-1)*DEL
D2=(TSP*SIN(A1)-MSP*SIN(A2))/R(I-1)
D6=TAC/TSP
D7=NAV*D2
P2=D6-D2
P3=D7-D2
R(I)=R(I-1)+DEL*R2
A(I)=A(I-1)+DEL*A3
P1=P1+DEL*D2
T1=T1+DEL*D6
T2=T2+DEL*D7
A1=A1+DEL*P2
A2=A2+DEL*P3
320 D(I)=D(I-1)+DEL
330 IF (R(I).GT.0) GO TO 310
T5=DEL*(I-1)
CALL SORT
CALL OUTPUT
C
999 CALL SCREEN
C

```

LPA01960  
 LPA01970  
 LPA01980  
 LPA01990  
 LPA02000  
 LPA02010  
 LPA02020  
 LPA02030  
 LPA02040  
 LPA02050  
 LPA02060  
 LPA02070  
 LPA02080  
 LPA02090  
 LPA02100  
 LPA02110  
 LPA02120  
 LPA02130  
 LPA02140  
 LPA02150  
 LPA02160  
 LPA02170  
 LPA02180  
 LPA02190  
 LPA02200  
 LPA02210  
 LPA02220  
 LPA02230  
 LPA02240  
 LPA02250  
 LPA02260  
 LPA02270  
 LPA02280  
 LPA02290  
 LPA02300  
 LPA02310  
 LPA02320  
 LPA02330  
 LPA02340  
 LPA02350  
 LPA02360  
 LPA02370  
 LPA02380  
 LPA02390  
 LPA02400  
 LPA02410  
 LPA02420  
 LPA02430

```

398 WRITE (6,410)
410 FORMAT (/'X','DO YOU WANT TO RUN THIS PROBLEM AGAIN? 0=YES, 1=NO')
READ (6,16) ID0
IF (ID0.EQ.1) GO TO 420
LOS=RATODE(L0S)
TAL=RATODE(TAL)
MAL=RATODE(MAL)
GO TO 204
420 WRITE (6,430)
430 FORMAT (/'X','DO YOU WANT TO RUN A NEW PROBLEM? 0=YES, 1=NO')
READ (6,16) ID0
IF (ID0.EQ.0) GO TO 1
NRUN=99
WRITE (7,144) NRUN,I
145 FORMAT (/'#')
144 FORMAT (I2,I4)
STOP
END

C
SUBROUTINE SCREEN
WRITE (6,600)
600 FORMAT (/'X','CLEAR SCREEN AND ENTER "0"'')
READ (6,16) ISCR
16 FORMAT (I11)
RETURN
END

C
SUBROUTINE SORT
DIMENSION A(9999),XM(9999),YM(9999),XT(9999),YT(9999)
REAL A,M,XM,YM,XT,YT,XPOS,XNEG,YPOS,YNEG
INTEGER I,W,Z
COMMON/BLOCK1/A,XM,YM,XT,YT,M,XPOS,XNEG,YPOS,YNEG,I
XPOS=0.0
XNEG=0.0
YPOS=0.0
YNEG=0.0
Z=1
DO 10 W=1,Z
IF (ABS(A(W)).GT.ABS(M)) M=A(W)
IF (XT(W).GT.XPOS) XPOS=XT(W)
IF (XM(W).GT.XNEG) XNEG=XM(W)
IF (YT(W).LT.YNEG) YNEG=YT(W)
IF (XM(W).LT.XNEG) XNEG=XM(W)
IF (YT(W).GT.YPOS) YPOS=YT(W)
IF (YM(W).GT.YPOS) YPOS=YM(W)

```

LPA02440  
 LPA02450  
 LPA02460  
 LPA02470  
 LPA02480  
 LPA02490  
 LPA02500  
 LPA02510  
 LPA02520  
 LPA02530  
 LPA02540  
 LPA02550  
 LPA02560  
 LPA02570  
 LPA02580  
 LPA02590  
 LPA02600  
 LPA02610  
 LPA02620  
 LPA02630  
 LPA02640  
 LPA02650  
 LPA02660  
 LPA02670  
 LPA02680  
 LPA02690  
 LPA02700  
 LPA02710  
 LPA02720  
 LPA02730  
 LPA02740  
 LPA02750  
 LPA02760  
 LPA02770  
 LPA02780  
 LPA02790  
 LPA02800  
 LPA02810  
 LPA02820  
 LPA02830  
 LPA02840  
 LPA02850  
 LPA02860  
 LPA02870  
 LPA02880  
 LPA02890  
 LPA02900  
 LPA02910

```

      IF (YT(W)-LT.YNEG) YNEG=YT(W)
      IF (YM(W)-LT.YNEG) YNEG=YM(W)
10  CONTINUE
    RETURN
  END

  SUBROUTINE OUTPUT
    REAL D,XM,YM,XT,YT,R,A,M,T5,M1,LOS1,TAL1,MAL1,E,F,G
    REAL DEL,NAV,LOS,IRT,IRM,TSP,TAC,TAL,MSP,MAC,MAL
    INTEGER ISAVE,M1,NRUN,ILOS,IPRO,II
    DIMENSION D(9999),XM(9999),YM(9999),XT(9999),YT(9999)
    DIMENSION R(9999),A(9999)
    COMMON/BLOCK1/A,XM,YM,XT,YT,M,XPOS,XNEG,YPOS,YNEG,I
    COMMON/BLOCK2/DEL,NAV,LOS,IRT,IRM,TSP,TAC,TAL,MSP,MAC,MAL,D,R,T5,
    *ISAVE,NRUN,ILOS,IPRO
    RATODE(X)=(X/(2*3.1415926535))*360

    M1=M/9.80665
    IF (ISAVE.EQ.0) GO TO 250

    CALL SCREEN
    IF (ILOS.EQ.0) WRITE (6,133)
    IF (IPRO.EQ.0) WRITE (6,134)
    WRITE (6,170)
    DO 240 W=1,I,25
      WRITE (6,107) D(W),XM(W),YM(W),XT(W),YT(W),R(W),A(W)
240  CONTINUE
      WRITE (6,107) D(I-1),XM(I-1),YM(I-1),XT(I-1),YT(I-1),
    *R(I-1),A(I-1)
107  FORMAT (1X,F6.3,5(2X,F8.1),2X,F10.3)
135  WRITE (6,135) M,M1,T5
    *T15,IS,TIME TO INTERCEPT,OR,F9.2,GWS./I
    *T15,THE TIME TO INTERCEPT,IS,F6.3,SECONDS.I)
143  WRITE (6,143)
    *DO YOU WISH TO INCLUDE THIS OUTPUT IN THE PRINTOUT ANL
    *D THE PLOT?/IX,(REMEMBER THAT ALL PLOTS FROM A SINGLE SESSION
    *ILL OVERLAY EACH OTHER.)/,IX,0=YES,1=NO.)
16  READ (6,16) ISAVE
    IF (ISAVE.EQ.1) GO TO 270

250  NRUN=NRUN+1
    IF (NRUN.LT.10) GO TO 255
    WRITE (6,25)
253  FORMAT (1X, YOU HAVE REQUESTED MORE THAN 9 ENCOUNTER SITUATIONS BEL

```



```

* SAVED AND PLOTTED' /, IX, WHICH, UNFORTUNATELY, IS NOT POSSIBLE.
* F YOU WANT ADDITIONAL PLOTS, EXIT THE' /, IX, PROGRAM, OUTPUT THE
* ST 9 SITUATIONS AND RE-ENTER THE PROGRAM BY TYPING' /, IX, "LPATH"
* ND ENTERING' /, IX, "LPATH"
GO TO 270
255 WRITE (8,32) NRUN
32 FORMAT (/ / IX, '$$$$ RUN NUMBER ', I2)
33 WRITE (8,33)
33 FORMAT (I25, 'PROBLEM PARAMETERS')
DR=IRI-IRM
YALI=RAATODE(TAL)
MALI=RAATODE(MAL)
LOSI=RAATODE(LOS)
WRITE (8,34) DEL, NAV, LOS1, DR, TSP, TAC, TALI, MSP, MALI
34 FORMAT (IX, T13, '01) TIME INCREMENT', T39, F10.4, ' SECONDS' /,
+ T13, '02) NAVIGATION CONSTANT', T39, F10.3, ' DEGREES' /,
+ T13, '03) LINE-OF-SIGHT ANGLE', T39, F10.3, ' METERS' /,
+ T13, '04) INITIAL SEPARATION', T39, F10.3, ' METERS' /,
+ T13, '05) TARGET SPEED', T39, F10.3, ' METERS/SEC' /,
+ T13, '06) TARGET ACCELERATION', T39, F10.3, ' M/SEC' /,
+ T13, '07) TARGET ALPHA', T39, F10.3, ' DEGREES' /,
+ T13, '08) MISSILE SPEED', T39, F10.3, ' METERS/SEC' /,
+ T13, '09) MISSILE INITIAL ALPHA', T39, F10.3, ' DEGREES' /,
IF (ILOS.EQ.0) WRITE (8,133)
133 FORMAT (/ T12, 'LINE OF SIGHT GUIDANCE INTERCEPT TRAJECTORY')
IF (IPRU.EQ.0) WRITE (8,134)
134 FORMAT (/ T07, 'PROPORTIONAL NAVIGATION GUIDANCE INTERCEPT TRAJECTORY')
* Y. )
WRITE (8,170)
170 FORMAT (IX, 'PROBLEM', T13, '---POSITION COORDINATES (METERS)---',
+ T52, 'RANGE', T62, '1X, TIME(S)', T15, 'XM', T25, 'YM', T35,
+ XT, T45, 'YT', T51, '(METERS)', T61, '(M/S/S)')
I1=(I/25)+2
E=25.
F=I
DO 5 J=1,50
G=F-E
IF (G.EQ.0.) GO TO 10
E=E+25.
5 CONTINUE
GO TO 20
10 I1=I-I
20 CONTINUE (I2,I4)
140 WRITE (7,140) NRUN, I1
FORMAT (I2, I4)
DO 260 W=1, I25
WRITE (8,107) D(W), XM(W), YM(W), XT(W), YT(W), R(W), A(W)
WRITE (7,141) XM(W), YM(W), XT(W), YT(W)

```

```

260 CONTINUE
WRITE (8,107) D(I-1),XM(I-1),YM(I-1),XT(I-1),YT(I-1),R(I-1),A(I-1)
WRITE (7,141) XM(I),YM(I),XT(I),YT(I)
141 FORMAT (4(F10.3))
WRITE (8,135) M,M1,T5
WRITE (7,141) XPDS,XNEG,YPOS,YNEG
270 ISAVE=1
CONTINUE
RETURN
END

```

```

LPA03880
LPA03890
LPA03900
LPA03910
LPA03920
LPA03930
LPA03940
LPA03950
LPA03960
LPA03970

```

```

//PATHPLOT JOB (1414,0483), 'LINDSEY', CLASS=B
//EXEC FRTXCLGP
//FORT -SYN DO *
C LPATH PLOTTING ROUTINE(MAXIMUM OF 9 SIMULTANEOUS PLOTS)
C READ IN DATA
C
REAL XM, YM, XT, YT, XPOS, XNEG, YPOS, YNEG, X, Y, XMAX, XMIN, YMAX, YMIN
REAL XMININ, YMININ, N, XSPAN, YSPAN, SCALES, XO, YO, SYMB
INTEGER K, J, N1, N2
DIMENSION XM(500), Y(500), XT(500,9), YT(500,9)
DIMENSION X(500), Y(500), SYMB(9)
DIMENSION I(9)
DATA SYMB/1.,2.,3.,4.,5.,6.,7.,8.,9./
XMAX=0.0
XMIN=0.0
YMAX=0.0
YMIN=0.0
100 READ (5,105) NRUN, I(NRUN)
105 FORMAT (12,14)
IF (NRUN.EQ.99) GO TO 120
N=NRUN
DO 110 K=1,500
READ (5,115) XM(K,N), YM(K,N), XT(K,N), YT(K,N)
IF (K.EQ.1(N)) GO TO 117
CONTINUE
110 FORMAT (4,F10.3)
115 READ (5,115) XPOS, XNEG, YPOS, YNEG
117 IF (XPOS.GT.XMAX) XMAX=XPOS
IF (XNEG.LT.XMIN) XMIN=XNEG
IF (YPOS.GT.YMAX) YMAX=YPOS
IF (YNEG.LT.YMIN) YMIN=YNEG
GO TO 100
120 CONTINUE
C
INITIALIZE PLOTTING
CALL PLOTS(0,0,0)
C
ESTABLISH PLOT "WINDOW"
XSPAN=XMAX-XMIN
YSPAN=YMAX-YMIN
IF ((YSPAN/7.0).GT.(XSPAN/9.0)) GO TO 130
SCALES=XSPAN/9.0
YMININ=YMIN/SCALES
YMAX=(7.0+YMININ)*SCALES
YSPAN=YMAX-YMIN
GO TO 135
130 SCALES=YSPAN/7.0
XMININ=XMIN/SCALES

```

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LPA00040
LPA00050
LPA00060
LPA00070
LPA00080
LPA00090
LPA00100
LPA00110
LPA00120
LPA00130
LPA00140
LPA00150
LPA00160
LPA00170
LPA00180
LPA00190
LPA00200
LPA00210
LPA00220
LPA00230
LPA00240
LPA00250
LPA00260
LPA00270
LPA00280
LPA00290
LPA00300
LPA00310
LPA00320
LPA00330
LPA00340
LPA00350
LPA00360
LPA00370
LPA00380
LPA00390
LPA00400
LPA00410
LPA00420
LPA00430
LPA00440
LPA00450
LPA00460
LPA00470
LPA00480
LPA00490
LPA00500
LPA00510

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LPA00520  
LPA00530  
LPA00540  
LPA00550  
LPA00560  
LPA00570  
LPA00580  
LPA00590  
LPA00600  
LPA00610  
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LPA00630  
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LPA00660  
LPA00670  
LPA00680  
LPA00690  
LPA00700  
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LPA00920  
LPA00930  
LPA00940  
LPA00950  
LPA00960  
LPA00970  
LPA00980  
LPA00990

```

135 C      XMAX=(9.0+XMININ)*SCALES
      XSPAN=XMAX-XMIN
      CONTINUE

      C      LOCATE ORIGIN OF AXES
      CALL PLOT(2.2,-3)

      C      SCALE X VALUES TO 9.0 INCH AXIS AND Y VALUES TO 7.0 INCH AXIS
      AND PLOT THEM
      X(1)=XMIN
      X(2)=XMAX
      X(3)=XMAX
      X(4)=0.0
      X(5)=0.0
      Y(1)=YMAX
      Y(2)=YMAX
      Y(3)=YMIN
      Y(4)=0.0
      Y(5)=0.0
      CALL SCALE(X,9.0,3,1)
      CALL SCALE(Y,7.0,3,1)
      CALL AXIS(0.0,0.0,REFERENCE DIRECTION,-19,9.0,0.0,XMIN,SCALES)
      CALL AXIS(0.0,0.0,0.0,+1,7.0,90.0,YMIN,SCALES)

      C      DO 160 K=1,N
      Z=I(K)

      C      PLOT TARGET PATH
      DO 140 J=1,500
        X(J)=XT(J,K)
        Y(J)=YT(J,K)
        IF (J.EQ.Z) GO TO 145
      CONTINUE
      X(Z+1)=XMIN
      X(Z+2)=SCALES
      Y(Z+1)=YMIN
      Y(Z+2)=SCALES
      CALL LINE(X,Y,Z,1,+Z,5)

      C      PLOT MISSILE PATH
      DO 150 J=1,500
        X(J)=XM(J,K)
        Y(J)=YM(J,K)
        IF (J.EQ.Z) GO TO 155
      CONTINUE
      X(Z+1)=XMIN
      X(Z+2)=SCALES
      Y(Z+1)=YMIN
      Y(Z+2)=SCALES

```

LPA01000  
 LPA01010  
 LPA01020  
 LPA01030  
 LPA01040  
 LPA01050  
 LPA01060  
 LPA01070  
 LPA01080  
 LPA01090  
 LPA01100  
 LPA01110  
 LPA01120  
 LPA01130  
 LPA01140  
 LPA01150  
 LPA01160

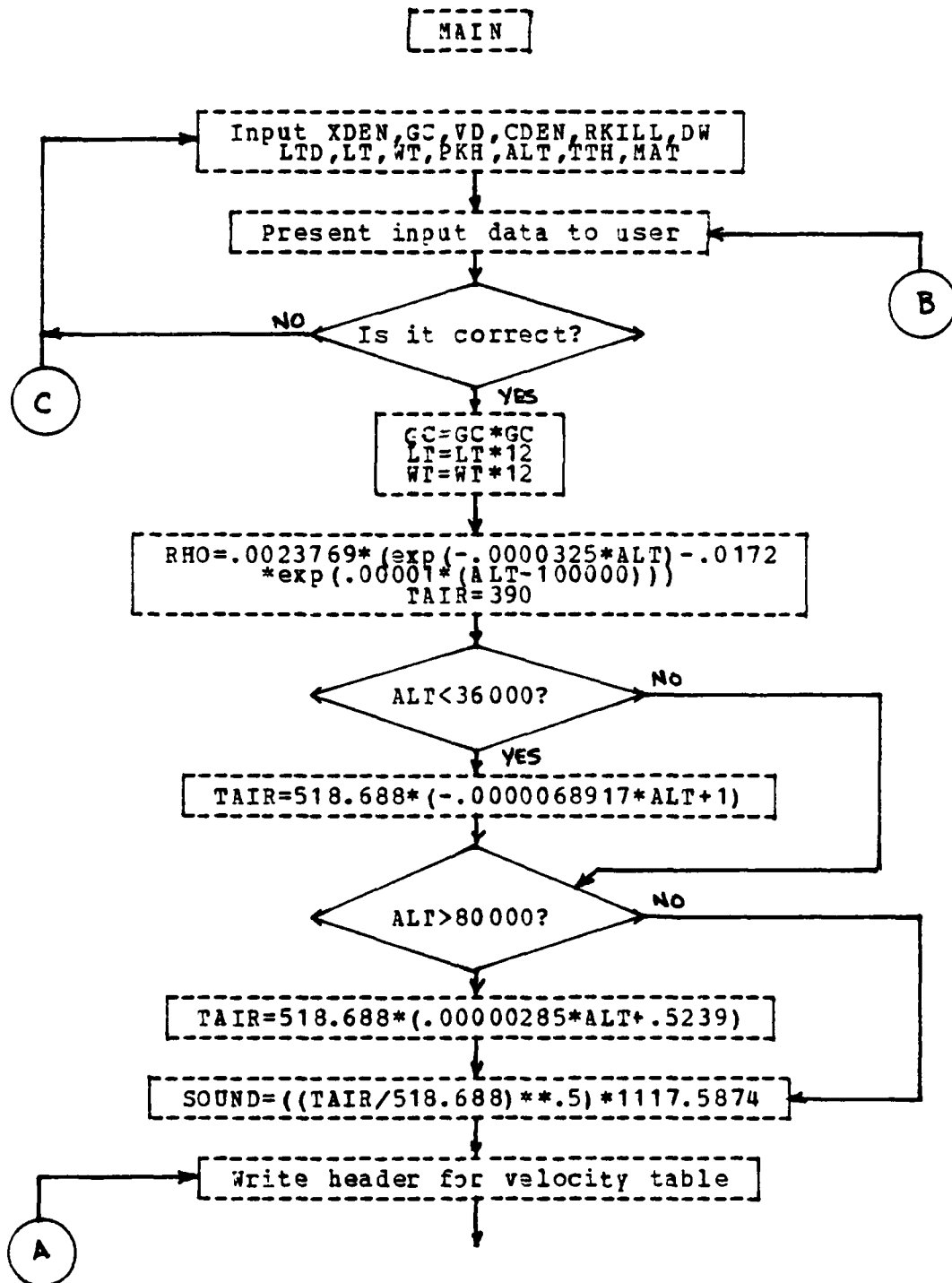
```

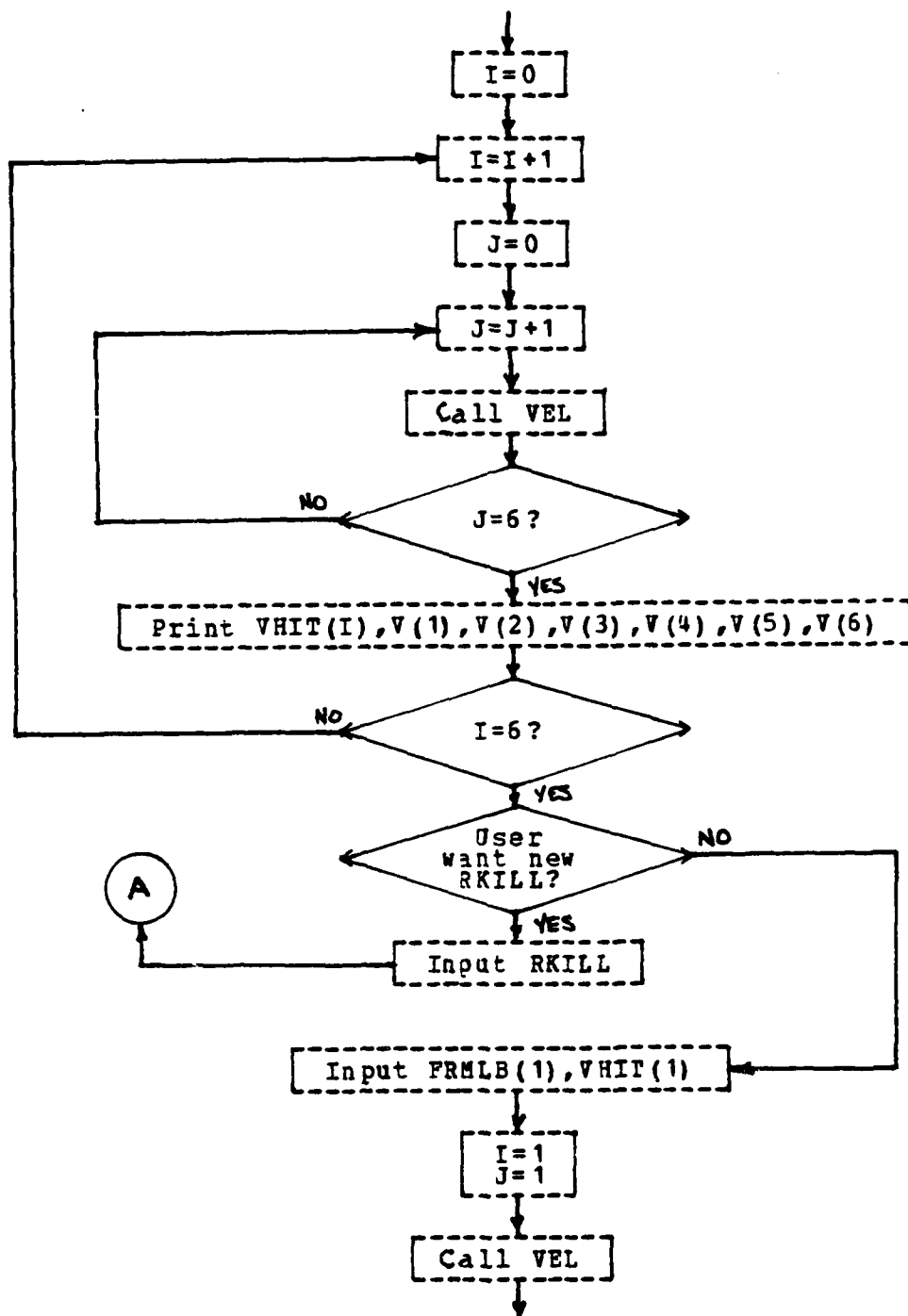
Y(Z+2)=SCALES
CALL LINE(X,Y,Z,1,+Z,0)
XO=X{Z}/SCALES
YO=Y{Z}/SCALES
CALL NUMBER(XO,YO,0.1,SYMB(K),0.0,-1)

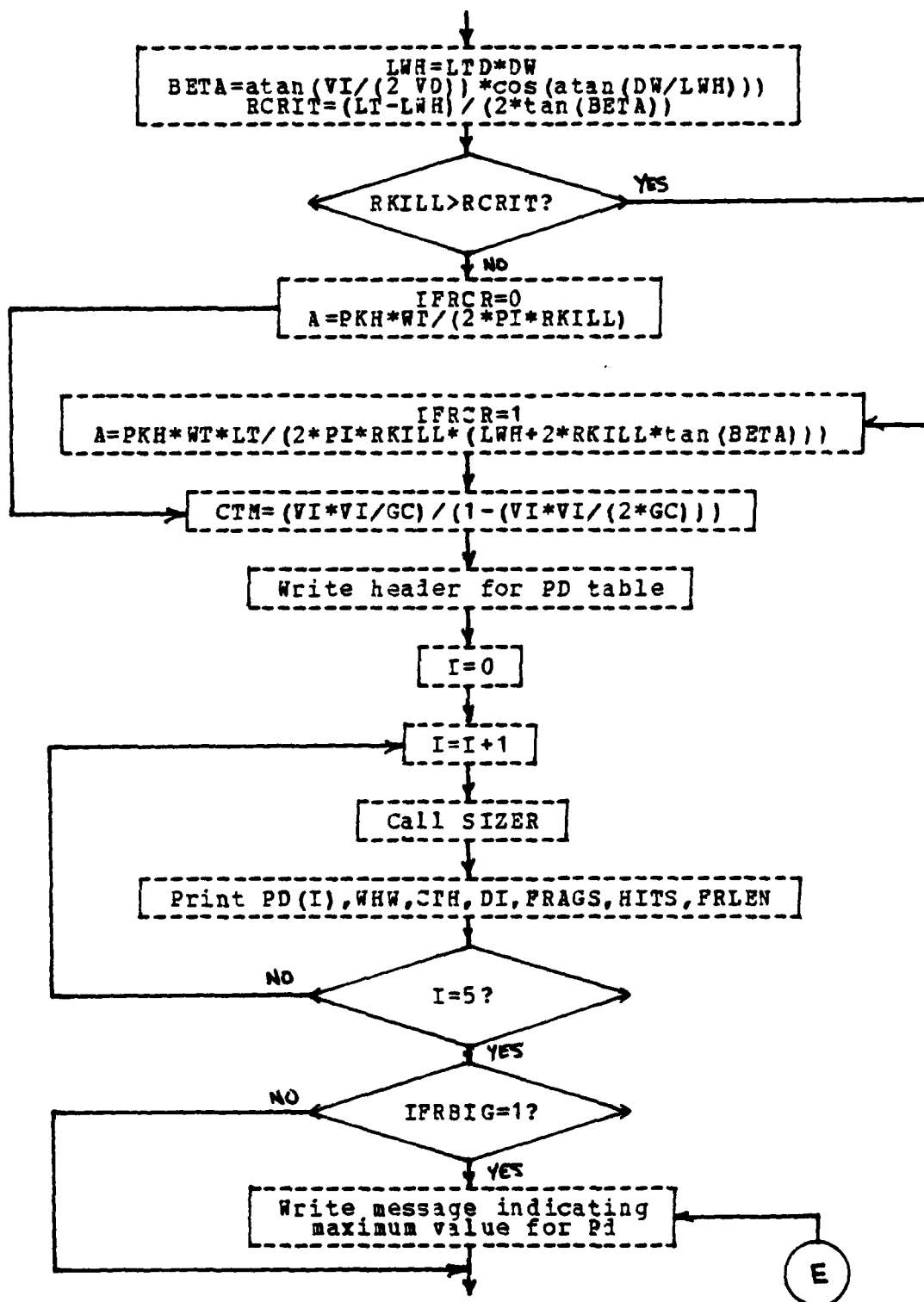
C 160 CONTINUE
C
C      END OF PLOTTING
CALL PLOT(0.0,0.,+999)
STOP
END

/*GO.PLOTPARM DD *
&PLOT SCALE=0.5 &END
/*GO.SYSIN DD *
  
```

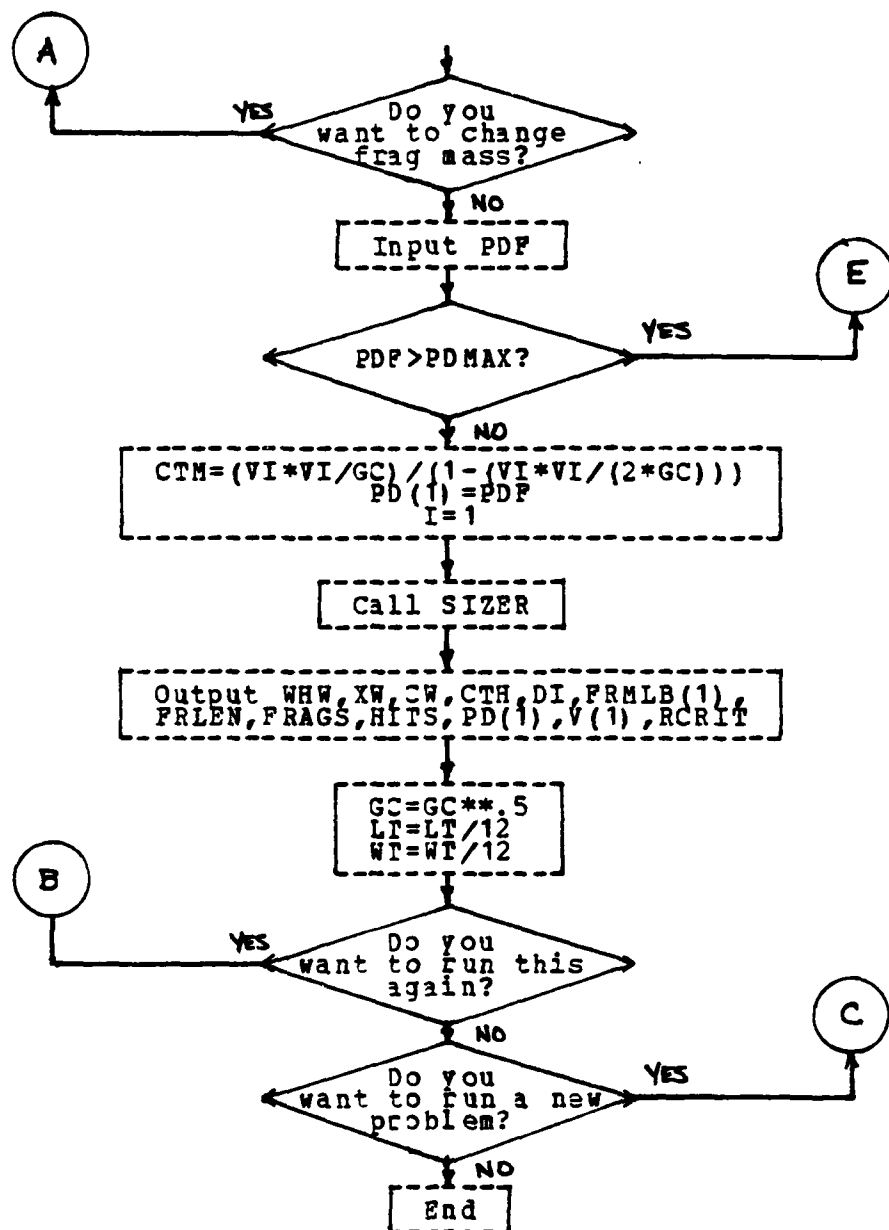
# APPENDIX C. WARHEAD DESIGN PROGRAM FLOWCHART











Subroutine VEL

FRAREA = (FRMLB(J)/CDEN)\*\*(2/3)  
R = (TTH\*MAT)/(FRAREA\*\*.5)

BLV(J) + 1.02546\*(1431.6875\*R) - (564.1857\*R\*R)  
+ (136.7064\*R\*\*3) - (8.77447\*R\*\*%)  
BLV(J) = BLV(J) \* (.26/CDEN)

K = RHO\*FRAREA\*0.65/FRMLB(J)  
V(J) = VHT(I) \* exp(K\*RKILL)  
M = V(J)/SOUND  
T = (1+.2\*M\*\*2)\*TAIR

Return

Subroutine SIZER

IFRBIG=0

SD

IFRCR=1?

YES

NO

BU = (2\*CTN\*(CDEN/XDEN) + 1)\*FRMLB(1)\*RKILL\*12  
BL = 5\*CDEN\*PKH\*WT  
RW = ((-BU/BL)\*alog(1-PD(I)))\*\* (1/3)

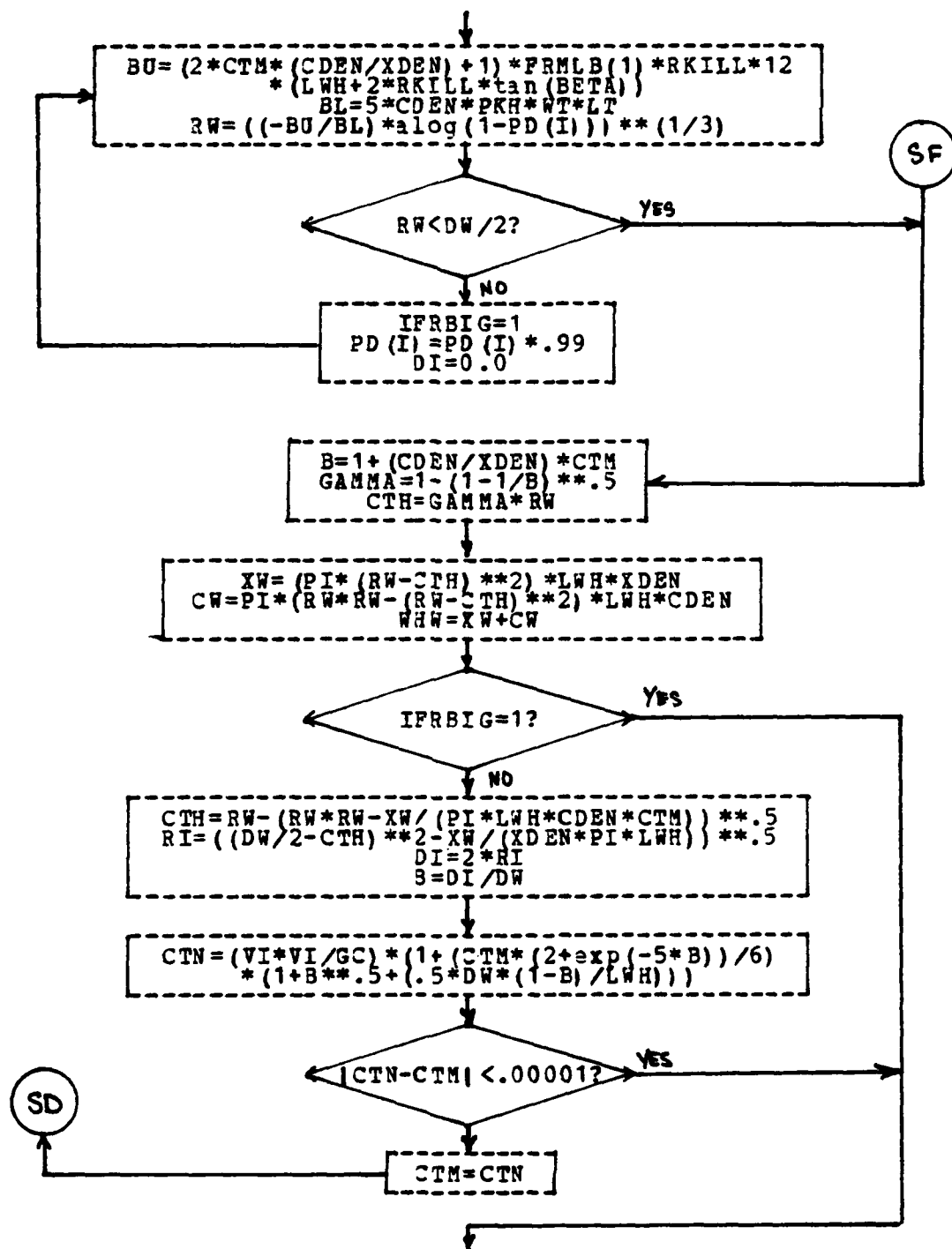
RW < DW/2?

YES

SF

NO

IFRBIG=1  
PD(I) = PD(I) \*.99  
DI=0.0



$$\text{FRAGS} = (\text{CDEN} * 5 * \text{PI} / \text{FRMLB}(1)) * (2 * \text{RW} * \text{RW} * \text{CTH} - \text{RW} * \text{CTH} * \text{CTH})$$

$$\text{FRLN} = (\text{FRMLB}(1) / (\text{CTH} * \text{CDEN})) ** .5$$

$$\text{HITS} = \text{FRAGS} * \text{A}$$

Return

#### APPENDIX D. WARHEAD DESIGN PROGRAM LISTING

This program has two major sections; the executive routine and the FORTRAN IV computational program. The executive routine establishes the required file definitions and initiates operation of the computational program.

The computational program, LBOMB FORTRAN, consists of four subprogram divisions. The MAIN program accepts the input data, calculates the atmospheric characteristics, and formats and displays the output to the user and sends it to the printer file. Subroutine VEL calculates the initial velocity required to propel a given mass a specified distance through the atmosphere with a particular residual velocity remaining. It also determines the ballistic limit velocities for the situation. Subroutine SIZER sizes the warhead for a given Pd value. It also produces the charge-to-mass ratio, the number of fragments, the fragment size, and the average number of hits received by the target. Subroutine SCREEN prompts the user to clear the terminal screen for proper positioning of the displayed data.

FILE: LBOMB EXEC A NAVAL POSTGRADUATE SCHOOL

FILEDEF 08 DISK LBOMB OUTPUT A0 (PERM  
&BEGTYPE

YOU WILL HAVE THE OPTION TO OBTAIN A HARDCOPY PRINTOUT  
OF THE LAST SOLUTION THAT YOU SOLVE. YOU MAY RERUN THE  
PROGRAM AS OFTEN AS YOU WISH BUT THE LAST RUN IS THE RUN  
THAT IS RECORDED.

&END  
LOAD LBOMB  
START  
&BEGTYPE

TO OBTAIN A HARDCOPY PRINTOUT OF THE RESULTS, TYPE  
"PRINT LBOMB OUTPUT" AND ENTER. THE OUTPUT WILL BE  
PRINTED ON THE VM PRINTER IN ROOM 140 AND WILL BE  
IDENTIFIED BY YOUR USER NUMBER AND LABEL NAME. IT  
USUALLY REQUIRES SEVERAL MINUTES TO OBTAIN THE  
PRINTOUT.

&END

```

C LBOMB SIZING PROGRAM
C WARHEAD SIZING PROGRAM
C LT. M.D. SULLIVAN, USN
C PROGRAM COORDINATOR: PROFESSOR GERALD LINDSEY, 3 JUNE 1981
C DEPT OF AERONAUTICS

REAL FRMLB, VHT, PD, BLV, CDEN, TTH, MAT, RHO, RKILL, SOUND, TAIR, V, T, XDEN
REAL CTM, PKH, WT, DW, CTH, CTN, WHW, FRAGS, FRLEN, HITS, A, GC, VD, LTD, LT
REAL ALT, LWH, BETA, VI, RCRT, DI, PDF
INTEGER I, J, K, IWANT, IFRCR, FRMGR, IFRBIG
DIMENSION FRMLB(6), VHT(6), PD(5), BLV(6), V(6)
DATA FRMLB/ .0071428, .0142857, .0214285, .0285714, .0357142, .0428571/
DATA VHT/ 1000., 2000., 3000., 4000., 5000., 6000./
DATA PD/ .999, .99, .98, .95, .90/
DATA FRMGR/ 50, 100, 150, 200, 250, 300/
PI=3.1415926

C
100 FORMAT (F15.5)
110 FORMAT (I2)
120 FORMAT (I1)
1000 CALL SCREEN
IFBACK=0
WRITE (6, 1010)
1010 FORMAT (1X, 1010)
6001 WRITE (6, 1020)
1020 FORMAT (1X, 1) INPUT THE FOLLOWING DATA AS DECIMAL NUMBERS ONLY: '/'
READ (5, 100) XDEN
IF (IFBACK.EQ.1) GO TO 1500
6002 WRITE (6, 1030)
1030 FORMAT (1X, 2) INPUT EXPLOSIVE GURNEY CONSTANT (FT/SEC): '/'
READ (5, 100) GC
IF (IFBACK.EQ.1) GO TO 1500
6003 WRITE (6, 1040)
1040 FORMAT (1X, 3) INPUT EXPLOSIVE DETONATION VELOCITY (FT/SEC): '/'
READ (5, 100) VD
IF (IFBACK.EQ.1) GO TO 1500
6004 WRITE (6, 1050)
1050 FORMAT (1X, 4) INPUT CASE MATERIAL DENSITY (LB/CU.IN): '/'
READ (5, 100) CDEN
IF (IFBACK.EQ.1) GO TO 1500
6005 WRITE (6, 1060)
1060 FORMAT (1X, 5) INPUT DESIRED KILL RADIUS (FT): '/'
READ (5, 100) RKILL
IF (IFBACK.EQ.1) GO TO 1500
6006 WRITE (6, 1070)

```

LB000040  
 LB000050  
 LB000060  
 LB000070  
 LB000080  
 LB000090  
 LB000100  
 LB000110  
 LB000120  
 LB000130  
 LB000140  
 LB000150  
 LB000160  
 LB000170  
 LB000180  
 LB000190  
 LB000200  
 LB000210  
 LB000220  
 LB000230  
 LB000240  
 LB000250  
 LB000260  
 LB000270  
 LB000280  
 LB000290  
 LB000300  
 LB000310  
 LB000320  
 LB000330  
 LB000340  
 LB000350  
 LB000360  
 LB000370  
 LB000380  
 LB000390  
 LB000400  
 LB000410  
 LB000420  
 LB000430  
 LB000440  
 LB000450  
 LB000460  
 LB000470  
 LB000480  
 LB000490  
 LB000500  
 LB000510

LB000520  
LB000530  
LB000540  
LB000550  
LB000560  
LB000570  
LB000580  
LB000590  
LB000600  
LB000610  
LB000620  
LB000630  
LB000640  
LB000650  
LB000660  
LB000670  
LB000680  
LB000690  
LB000700  
LB000710  
LB000720  
LB000730  
LB000740  
LB000750  
LB000760  
LB000770  
LB000780  
LB000790  
LB000800  
LB000810  
LB000820  
LB000830  
LB000840  
LB000850  
LB000860  
LB000870  
LB000880  
LB000890  
LB000900  
LB000910  
LB000920  
LB000930  
LB000940  
LB000950  
LB000960  
LB000970  
LB000980  
LB000990

```

1070  FORMAT (IX, 6) INPUT WARHEAD DIAMETER (IN):')
      READ (5,100) DW
      IF (IFBACK.EQ.1) GO TO 1500
1007  WRITE (6,1080)
1080  FORMAT (IX, 7) INPUT WARHEAD LENGTH-TO-DIAMETER RATIO:')
      READ (5,100) LTD
      IF (IFBACK.EQ.1) GO TO 1500
1008  WRITE (6,1090)
1090  FORMAT (IX, 6) INPUT TARGET LENGTH (FT):')
      READ (5,100) LT
      IF (IFBACK.EQ.1) GO TO 1500
1009  WRITE (6,1100)
1100  FORMAT (IX, 9) INPUT TARGET WIDTH (FT):')
      READ (5,100) WT
      IF (IFBACK.EQ.1) GO TO 1500
1010  WRITE (6,1110)
1110  FORMAT (IX, 10) INPUT TARGET VULNERABILITY, P(K/H):')
      READ (5,100) PKH
      IF (IFBACK.EQ.1) GO TO 1500
1011  WRITE (6,1120)
1120  FORMAT (IX, 11) INPUT TARGET ALTITUDE (FT):')
      READ (5,100) ALT
      IF (IFBACK.EQ.1) GO TO 1500
1012  WRITE (6,1130)
1130  FORMAT (IX, 12) INPUT TARGET SKIN THICKNESS (IN):')
      READ (5,100) TTH
      IF (IFBACK.EQ.1) GO TO 1500
1013  WRITE (6,1140)
1140  FORMAT (IX, 13) INPUT SKIN MATERIAL CODE: 1.0=ALUMINUM',
      *32X, 2.0=FIBERGLASS/KEVLAR',
      *32X, 3.0=STEEL',
      READ (5,100) MAT
      IF (IFBACK.EQ.1) GO TO 1500

C 1500  CALL SCREEN
      REWIND 08
      IFBACK=1
      WRITE (6,1510) XDEN,GC,VD,CDEN,RKILL,DW,LTD
1510  WRITE (6,1510) XDEN,GC,VD,CDEN,RKILL,DW,LTD
      FORMAT (IX, 1) THE FOLLOWING IS A SUMMARY OF THE INPUT DATA:/',
      *1X, 01) EXPLOSIVE GURNEY CONSTANT, T40, F10.5, LB/CU.IN./,
      *1X, 02) EXPLOSIVE DETONATION VELOCITY, T40, F10.2, FT/SEC./,
      *1X, 03) EXPLOSIVE GURNEY CONSTANT, T40, F10.5, LB/CU.IN./,
      *1X, 04) CASE MATERIAL DENSITY, T40, F10.4, LB/CU.IN./,
      *1X, 05) DESIRED KILL RADIUS, T40, F10.1, FEET./,
      *1X, 06) DESIRED KILL RADIUS, T40, F10.2, INCHES./,
      *1X, 07) WARHEAD DIAMETER, T40, F10.2,
      WRITE (6,1520) LT,WT,PKH,ALT,TTH

```



```

1520 WRITE (8,1520) LT,WT,PKH,ALT,TTH
      FORMAT (1X,08) TARGET LENGTH,T40,F10.2, FEET/,
      *1X,09) TARGET WIDTH,T40,F10.2, FEET/,
      *1X,10) TARGET VULNERABILITY,PK/H,T40,F10.3/,
      *1X,11) TARGET ALTITUDE,T40,F10.0, FEET/,
      *1X,12) TARGET SKIN THICKNESS,T40,F10.3, INCHES)
      IF (MAT.EQ.1) WRITE (8,1530)
      IF (MAT.EQ.2) WRITE (8,1530)
1530 FORMAT (1X,13) TARGET SKIN MATERIAL,T40, ALUMINUM)
      IF (MAT.EQ.2) WRITE (8,1540)
      IF (MAT.EQ.13) WRITE (8,1540)
1540 FORMAT (1X,13) TARGET SKIN MATERIAL,T40, FIBERGLASS)
      IF (MAT.EQ.3) WRITE (8,1550)
      IF (MAT.EQ.13) WRITE (8,1550)
1550 FORMAT (1X,13) TARGET SKIN MATERIAL,T40, STEEL)
1560 FORMAT (1X,13) TARGET SKIN MATERIAL,T40, STEEL)
      *1X,14) IF NO, ENTER THE TWO-DIGIT NUMBER OF THE WRONG ENTRY.}
      READ (5,110) IGO TO
      IF (IGO EQ.00) GO TO 1600
      GO TO (6001,6002,6003,6004,6005,6006,6007,6008,6009,6010,6011,6012,
      * 6013), IGO TO

C 1600 GC=GC*GC
      LT=LT*12.
      WT=WT*12.

C      RHO=.0023769*(EXP(-.0000325*ALT)-.0172*EXP(.00001*(ALT-100000.)))
      TAIR=390.
      IF (ALT.LT.36000.) TAIR=518.688*{-.0000068917*ALT+1.}
      IF (ALT.GT.80000.) TAIR=518.688*{.00000285*ALT+.5239}
      SOUND=((TAIR/518.688)**.5)*1117.5874

C 1990 CALL SCREEN
      VMLB(1)=1000.
      VMLB(1)=0071428
      WRITE (6,2000) RKILL
      WRITE (8,2000) RKILL
      FORMAT (1X,1) INITIAL VELOCITY TABLE FOR,F6.1, FT KILL RADIUS/,
      *2X,1) IMPACT,25X,1) FRAGMENT MASSES/,
      *1X,1) VELOCITY,T14,150 GR.,T23,100 GR.,T43,200 GR.
      * 153,250 GR.,T63,300 GR.)
      DO 2030 I=1,6
      DO 2010 J=1,6
      CALL VEL (FMLB,VHIT,BLV,V,CDEN,TTH,MAT,RHO,RKILL,SOUND,
      * TAIR,T,I,J)
      CONTINUE
      WRITE (6,2020) VHIT(I),(V(K),K=1,6)

```

L8001000  
 L8001010  
 L8001020  
 L8001030  
 L8001040  
 L8001050  
 L8001060  
 L8001070  
 L8001080  
 L8001090  
 L8001100  
 L8001110  
 L8001120  
 L8001130  
 L8001140  
 L8001150  
 L8001160  
 L8001170  
 L8001180  
 L8001190  
 L8001200  
 L8001210  
 L8001220  
 L8001230  
 L8001240  
 L8001250  
 L8001260  
 L8001270  
 L8001280  
 L8001290  
 L8001300  
 L8001310  
 L8001320  
 L8001330  
 L8001340  
 L8001350  
 L8001360  
 L8001370  
 L8001380  
 L8001390  
 L8001400  
 L8001410  
 L8001420  
 L8001430  
 L8001440  
 L8001450  
 L8001460  
 L8001470

```

2020 WRITE (8,2020) VHT(1), (V(K),K=1,6)
2030 FORMAT (3X,F5.0,6(4X,F6.0))
CONTINUE
2035 WRITE (6,2035) (BLV(I),I=1,6)
WRITE (8,2035) (BLV(I),I=1,6)
2045 FORMAT (1X,'BALLISTIC',1X,'LIMIT',7X,F5.0,5(5X,F5.0))
WRITE (6,2045)
2045 FORMAT (7,1X,'DO YOU WANT A NEW KILL RADIUS? (1=YES,0=NO)')
READ (5,120) IWANT
IF (IWANT.EQ.0) GO TO 2049
WRITE (6,2046)
2046 FORMAT (1X,'INPUT NEW KILL RADIUS (FEET, DECIMAL):')
READ (5,100) RKILL
GO TO 1990
2049 WRITE (6,2050)
2050 FORMAT (1X,'INPUT DESIRED FRAGMENT MASS (GRAINS, DECIMAL):')
READ (5,100) FRMLB(1)
2051 WRITE (8,2051) FRMLB(1)
FORMAT (7,1X,'FRAGMENT MASS:...',F6.1,' GRAINS')
FRMLB(1)=FRMLB(1)*.000142856973
2060 WRITE (6,2060)
2060 FORMAT (1X,'INPUT DESIRED IMPACT VELOCITY (FT/SEC, DECIMAL):')
READ (5,100) VHT(1)
2061 WRITE (8,2061) VHT(1)
FORMAT (1X,'IMPACT VELOCITY.....',F6.0,' FT/SEC./')
CALL SCREEN
I=1
J=1
* CALL VEL (FRMLB,VHT,BLV,V,COEN,TTH,MAT,RHO,RKILL,SOUND,TAIR,T,I,JL)
VI=V(J)
C 2100 CONTINUE
LWH=LTD*DW
BETA=ATAN(VI/(2.*VD)*COS(ATAN(DW/LWH)))
RCRIT=(LT-LWH)/(2.*TAN(BETA))
IF (RKILL.GT.RCRIT) GO TO 2105
IFRCR=0
A=PKH*WT/(2.*PI*RKILL)
GO TO 2110
2105 IFRCR=1
A=PKH*WT*LT/(2.*PI*RKILL*(LWH+2.*RKILL*TAN(BETA)))
C 2110 CONTINUE
CTM=(VI*VI/GC)/(1.-(VI*VI/(2.*GC)))
2115 CONTINUE
WRITE (6,2120)
WRITE (8,2120)

```

```

LB001480
LB001490
LB001500
LB001510
LB001520
LB001530
LB001540
LB001550
LB001560
LB001570
LB001580
LB001590
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LB001610
LB001620
LB001630
LB001640
LB001650
LB001660
LB001670
LB001680
LB001690
LB001700
LB001710
LB001720
LB001730
LB001740
LB001750
LB001760
LB001770
LB001780
LB001790
LB001800
LB001810
LB001820
LB001830
LB001840
LB001850
LB001860
LB001870
LB001880
LB001890
LB001900
LB001910
LB001920
LB001930
LB001940
LB001950

```

```

2120 FORMAT (T13,'WARHEAD',T25,'CASE',T36,'CORE',T43,'-----FRAGMENT',B001960
*5-----/
*6X,'PD',T14,'WEIGHT',T23,'THICKNESS',T34,'DIAMETER',T44,
*NUMBER,T15,'ON TARGET',T64,'LENGTH')
DO 2200 I=1,5
* CALL SIZER (FRMLB,PD,CDEN,XDEN,CTM,RKILL,PKH,WT,DW,CTH,GC,WHW,
* LT,VI,DI,LWH,BETA,FRAGS,FRLEN,HITS,A,XW,CW,IFRBIG,IFRCR,I)
WRITE (6,2160) PD(I),WHW,CTH,DI,FRAGS,HITS,FRLEN
WRITE (8,2160) PD(I),WHW,CTH,DI,FRAGS,HITS,FRLEN
2200 CONTINUE
2160 FORMAT (1X,F8.3,6(2X,F8.2))
2205 IF (PD(I).LT..999) WRITE (6,2210)
IF (PD(I).LT..999) WRITE (8,2210)
2210 FORMAT (1X,'THE FIRST PD TERM IS THE HIGHEST ATTAINABLE WITH THE
* IVEN',1X,'KILL RADIUS AND FRAGMENT SIZE.')
2215 WRITE (6,2220)
2220 FORMAT (1X,'DO YOU WANT TO CHANGE YOUR FRAGMENT SIZE? (1=YES,0=NO)')
*
READ (5,120) IWANT
IF (IWANT.EQ.1) GO TO 1990
2225 WRITE (6,2230)
2230 FORMAT (1X,'INPUT DESIRED PD (DECIMAL):')
READ (5,100) PDF
IF (PDF.LT.PD(I)) GO TO 2228
WRITE (6,2229)
2229 FORMAT (1X,'TOO LARGE PD CANNOT BE GREATER THAN THE FIRST ONE ON
* THE LIST ABOVE ',1X,'TRY AGAIN')
GO TO 2225
2228 CALL SCREEN
WRITE (8,2231) PDF
2231 FORMAT (1X,'KILL PROBABILITY: ',F6.3/)
CTM=(VI*VI/GC)/(1.-(VI*VI/(2.*GC)))
PD(I)=PDF
I=1
* CALL SIZER (FRMLB,PD,CDEN,XDEN,CTM,RKILL,PKH,WT,DW,CTH,GC,WHW,
* LT,VI,DI,LWH,BETA,FRAGS,FRLEN,HITS,A,XW,CW,IFRBIG,IFRCR,I)
FRMLB(I)=FRMLB(1)/.000142856973
WRITE (6,2300)
WRITE (8,2300)
2300 FORMAT (1X,'WARHEAD DESCRIPTION-----')
WRITE (6,2310) WHW,XW,CW,CTH,DI,FRMLB(I)
WRITE (8,2310) WHW,XW,CW,CTH,DI,FRMLB(I)
2310 FORMAT (1X,'WARHEAD WEIGHT',T35,F8.2,' POUNDS',/,
*4X,'EXPLOSIVE WEIGHT',T35,F8.2,' POUNDS',/,
*4X,'CASE THICKNESS',T35,F8.4,' INCHES',/,
*4X,'CORE DIAMETER',T35,F8.2,' INCHES',/,
*4X,'FRAGMENT WEIGHT',T35,F8.2,' GRAINS')

```

```

2320 WRITE (6,2320) FRLEN,FRLEN,CTH,FRAGS,HITS,PD(1),V(1),RCRIT
      * INCHES,4X,FRAGMENT DIMENSIONS,126,F5.3,1X,F5.3,1X,F5.3,
      * INCHES,4X,NUMBER OF FRAGMENTS,135,F8.0/,
      *X,NUMBER OF HITS ON TARGET,135,F8.0/,
      *X,PROBABILITY OF KILL (PD),135,F8.3/,
      *X,INITIAL FRAGMENT VELOCITY,135,F8.1, FT/SEC,/,
      *X,CRITICAL MISS DISTANCE,135,F8.1, FEET,/)

C
GC=GC*.5
LT=LT/12.
FRMLB(1)=.0071428
VHIT(1)=1000.
PD(1)=.999

C
2400 WRITE (6,2400)
      *FORMAT (1X,DO YOU WANT TO RUN THIS PROBLEM AGAIN? (1=YES,0=NO)*)
      IF (IWANT.EQ.1) GO TO 1500
      WRITE (6,2410)
2410 FORMAT (1X,DO YOU WANT TO RUN A NEW PROBLEM? (1=YES,0=NO)*)
      IF (IWANT.EQ.1) GO TO 1000
      CALL SCREEN
      RETURN
      END

C
SUBROUTINE VEL (FRMLB,VHIT,BLV,V,CDEN,TTH,MAT,RHO,RKILL,SOUND,
      *TAIR,TIJJ)
      REAL FRAREA,FRMLB,CDEN,R,TTH,MAT,BLV,K,RHO,V,VHIT,RKILL,M,SOUND
      REAL TTAIR
      DIMENSION FRMLB(6),BLV(6),V(6),VHIT(6)

      FRAREA=(FRMLB(J)/CDEN)**(2./3.)
      R=(TTH*MAT)/(FRAREA*.5)
      BLV(J)=1.02546+(1431.6875*R)-(564.1857*R*R)+(136.7064*R**3.)-(8.77
      *47*R**4.)
      BLV(J)=BLV(J)*(.26/CDEN)
      K=RHO*FRAREA*.65/FRMLB(J)
      V(J)=VHIT(1)*EXP(K*RKILL)
      M=V(J)/SOUND
      T=(1+.2*M**2.)*TAIR
      RETURN
      END

```

```

LB002440
LB002450
LB002460
LB002470
LB002480
LB002490
LB002500
LB002510
LB002520
LB002530
LB002540
LB002550
LB002560
LB002570
LB002580
LB002590
LB002600
LB002610
LB002620
LB002630
LB002640
LB002650
LB002660
LB002670
LB002680
LB002690
LB002700
LB002710
LB002720
LB002730
LB002740
LB002750
LB002760
LB002770
LB002780
LB002790
LB002800
LB002810
LB002820
LB002830
LB002840
LB002850
LB002860
LB002870
LB002880
LB002890
LB002900
LB002910

```

CC

C

```

SUBROUTINE SIZER (FRMLB,PD,CDEN,XDEN,CTM,RKILL,PKH,WT,DW,CTH,
*GC,WT,LT,VI,DI,LWH,BETA,FRAGS,FRLEN,HITS,A,XW,CW,IFRBIG,IFRCR,I)
REAL PI,BU,BL,CDEN,XDEN,CTM,RKILL,FRMLB,PKH,WT,GAMMA,B,LT
REAL RW,PD,DW,DI,CTH,XW,CW,LWH,WHW,RI,CTN,VI,GC,FRAGS,FRLEN,HITS
INTEGER IFRBIG,IFRCR,I
DIMENSION FRMLB(6),PD(5)
PI=3.1415926
IFRBIG=0
10 IF (IFRCR.EQ.1) GO TO 25
BU=(2.*CTM*(CDEN/XDEN)+1.)*FRMLB(1)*RKILL*12.
BL=5.*CDEN*PKH*WT
20 RW=(((-BU/BL)*ALOG(1.-PD(I)))*1./3.)
IF (RW.LT.DW/2.) GO TO 30
IFRBIG=1
PD(I)=PD(I)*.99
DI=0.0
GO TO 20
25 BU=(2.*CTM*(CDEN/XDEN)+1.)*FRMLB(1)*RKILL*12.*(LWH+2.*RKILL*TAN(B
*TA))
BL=5.*CDEN*PKH*WT*LT
26 RW=(((-BU/BL)*ALOG(1.-PD(I)))*1./3.)
IF (RW.LT.DW/2.) GO TO 30
IFRBIG=1
PD(I)=PD(I)*.99
DI=0.0
GO TO 26
30 CONTINUE
B=1.+(CDEN/XDEN)*CTM
GAMMA=1.-1./B)**.5
CTH=GAMMA*RW
XW=(PI*(RW-CTH)**2.)*LWH*XDEN
CW=PI*(RW*RW-(RW-CTH)**2.)*LWH*CDEN
WHW=XW+CW
IF (IFRBIG.EQ.1) GO TO 50
CTH=RW-((RW*RW-XW)/(PI*LWH*CDEN*CTM))**.5
RI=((DW/2.-CTH)**2.-XW/(XDEN*PI*LWH))**.5
DI=2*RI
B=DI/DW
40 CTN=(VI*VI/GC)*(1.+(CTM*(2.+EXP(-5.*B))/6.)*(1.+B**5+1.5*DW*(1.-B
*)/LWH))
IF (ABS(CTN-CTM).LT..00001) GO TO 50
CTM=CTN
GO TO 10

```

LB002920  
 LB002930  
 LB002940  
 LB002950  
 LB002960  
 LB002970  
 LB002980  
 LB002990  
 LB003000  
 LB003010  
 LB003020  
 LB003030  
 LB003040  
 LB003050  
 LB003060  
 LB003070  
 LB003080  
 LB003090  
 LB003100  
 LB003110  
 LB003120  
 LB003130  
 LB003140  
 LB003150  
 LB003160  
 LB003170  
 LB003180  
 LB003190  
 LB003200  
 LB003210  
 LB003220  
 LB003230  
 LB003240  
 LB003250  
 LB003260  
 LB003270  
 LB003280  
 LB003290  
 LB003300  
 LB003310  
 LB003320  
 LB003330  
 LB003340  
 LB003350  
 LB003360  
 LB003370  
 LB003380  
 LB003390

```

50 FRAGS=(CDEN*5.*PI/FRMLB(1))*(2.*RW*RW*CTH-RW*CTH*CTH)
   FRLEN=(FRMLB(1))/(CTH*CDEN)**.5
   HITS=FRAGS*A
   RETURN
   END

```

CCC

```

SUBROUTINE SCREEN
WRITE(6,600)
600 FORMAT(IX,'CLEAR SCREEN AND ENTER "0"')
16 READ(6,16) ISCR
16 FORMAT(111)
RETURN
END

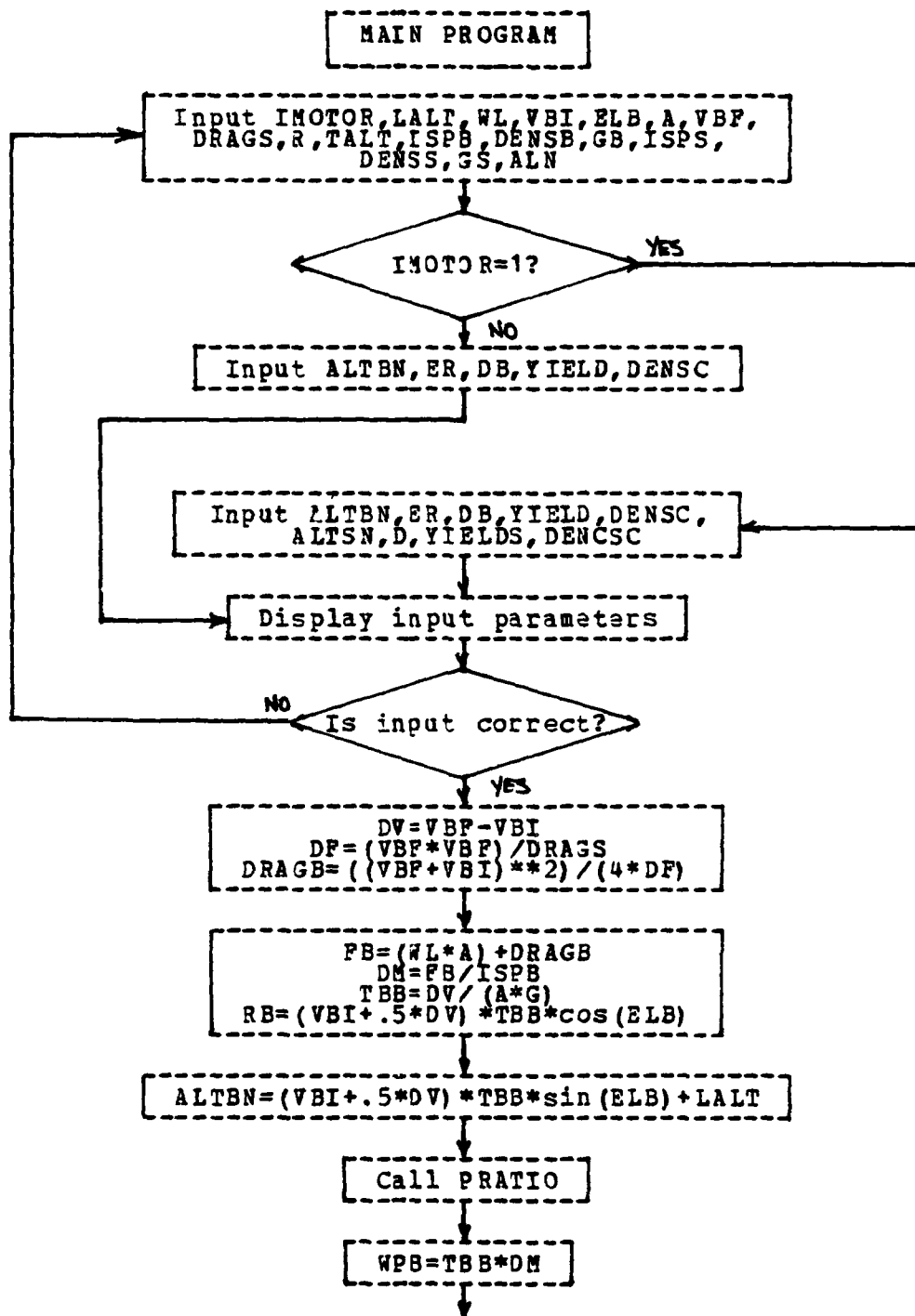
```

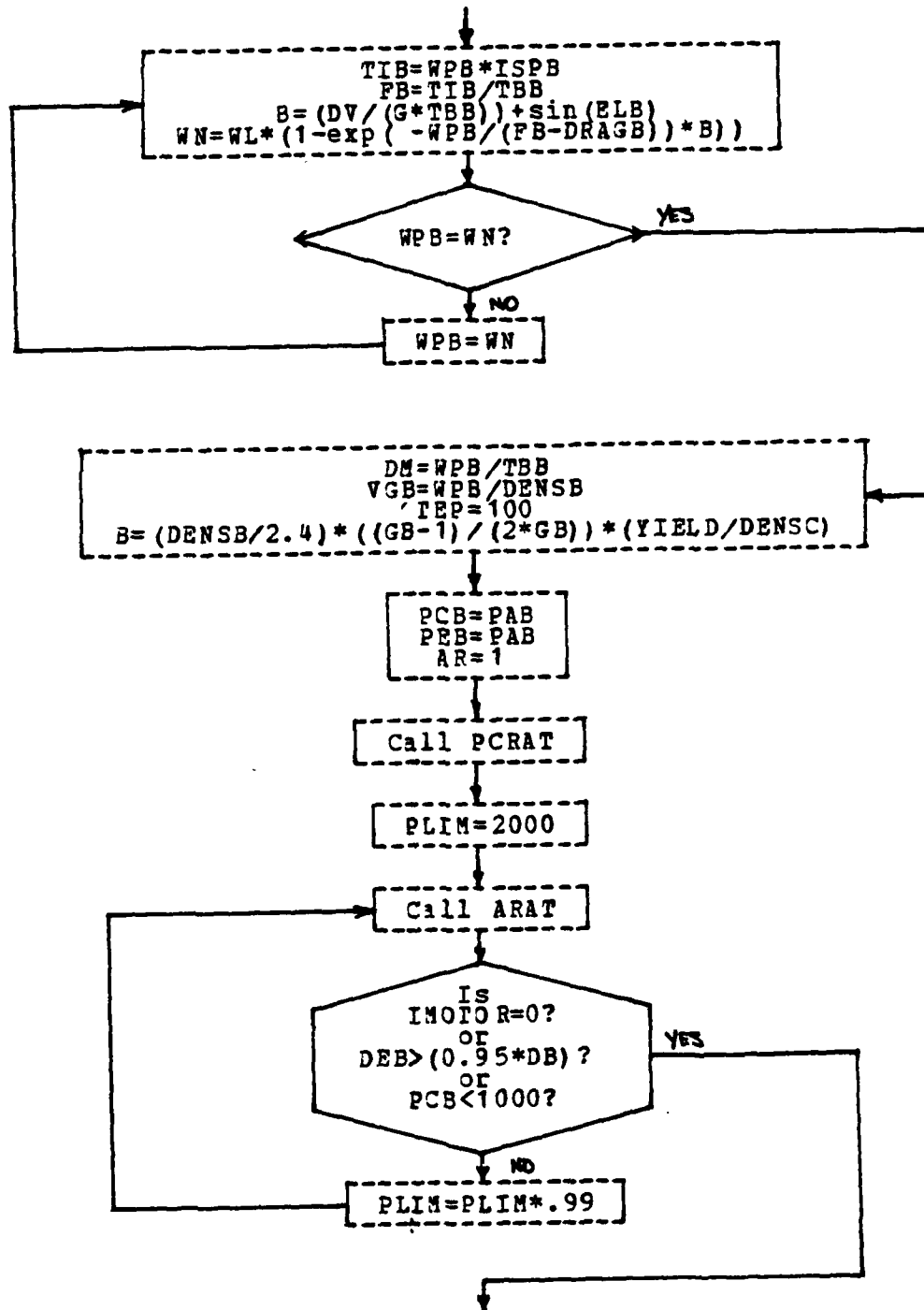
```

LB003400
LB003410
LB003420
LB003430
LB003440
LB003450
LB003460
LB003470
LB003480
LB003490
LB003500
LB003510
LB003520
LB003530
LB003540
LB003550

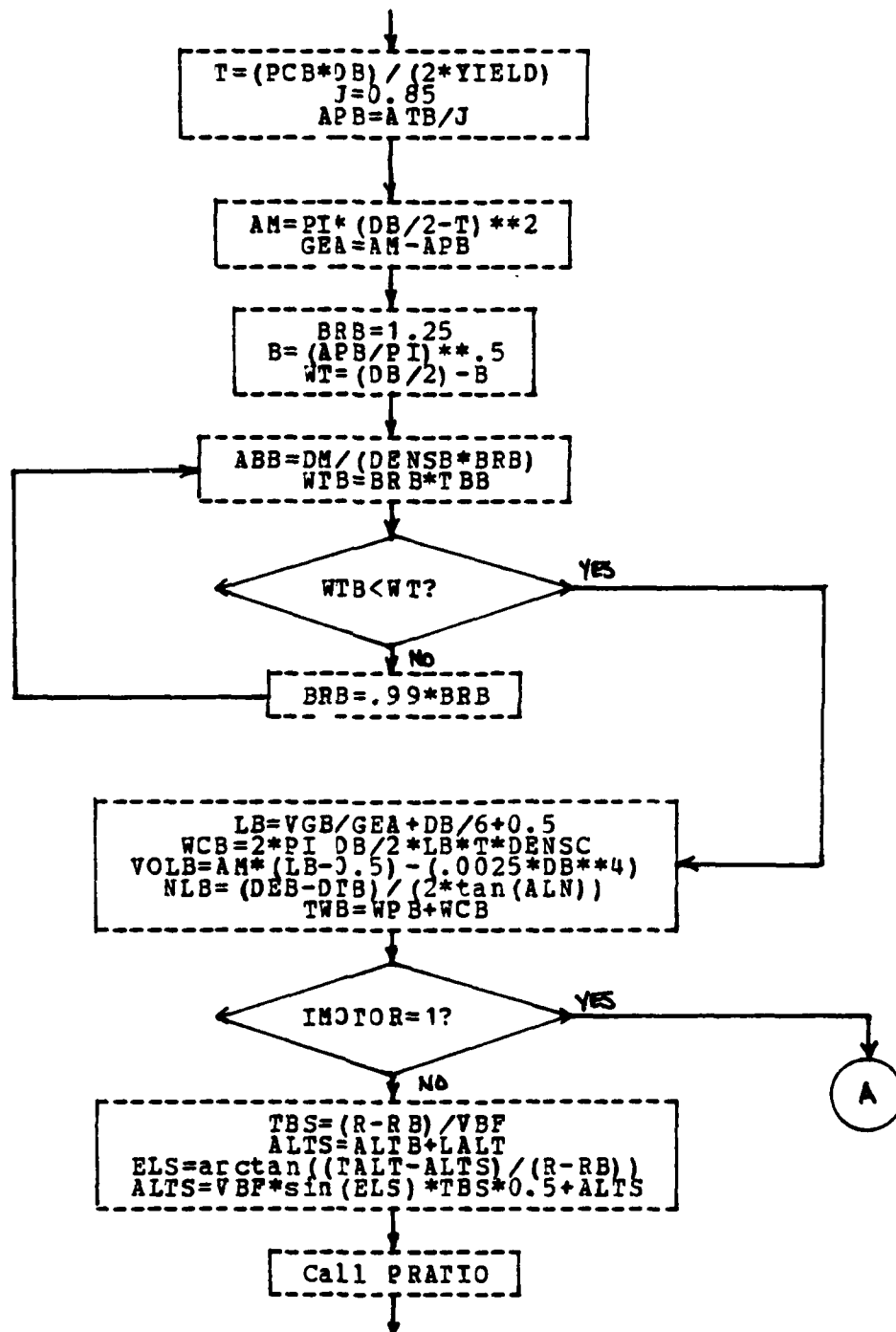
```

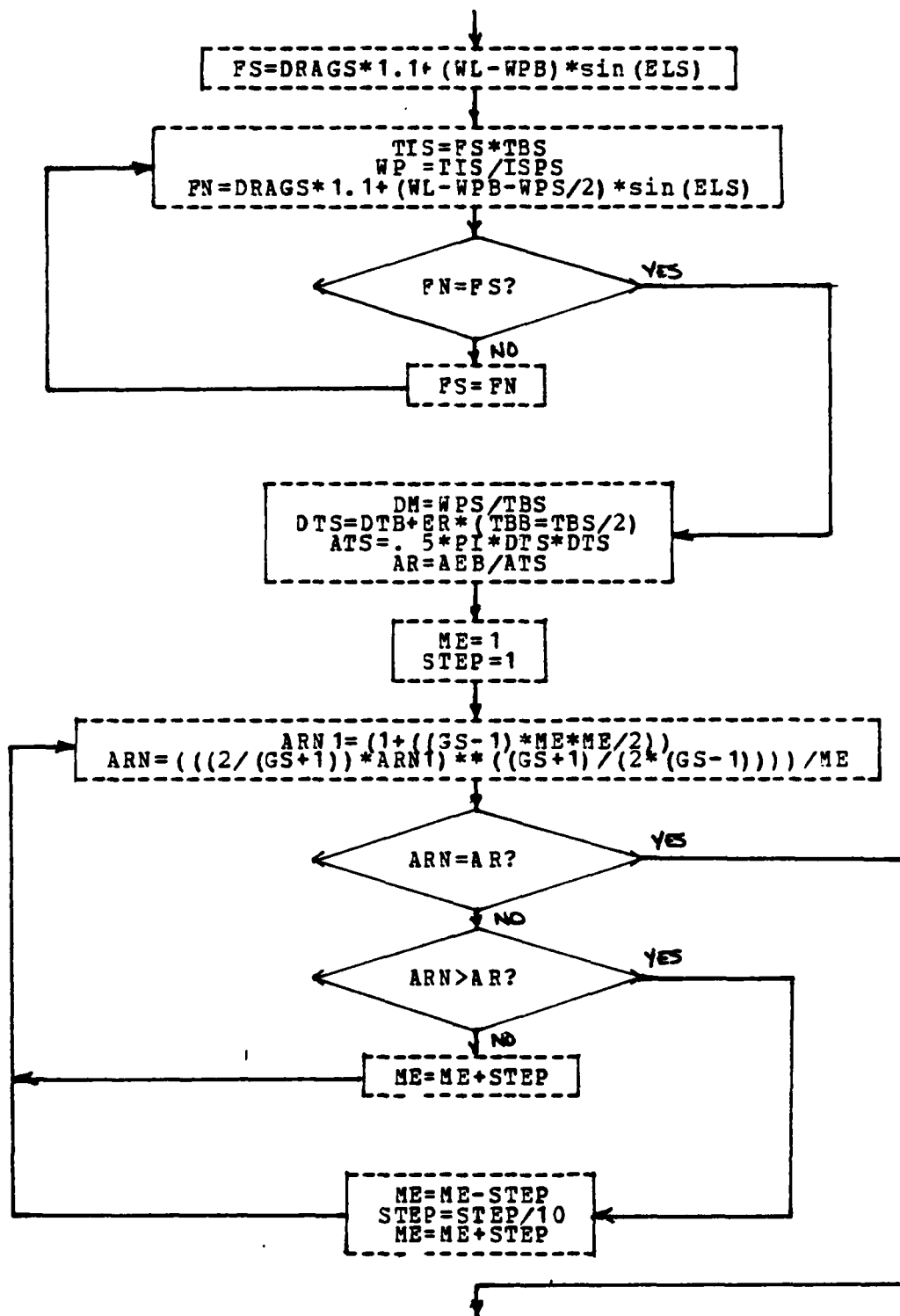
# APPENDIX E. PROPULSION SIZING PROGRAM FLOWCHART

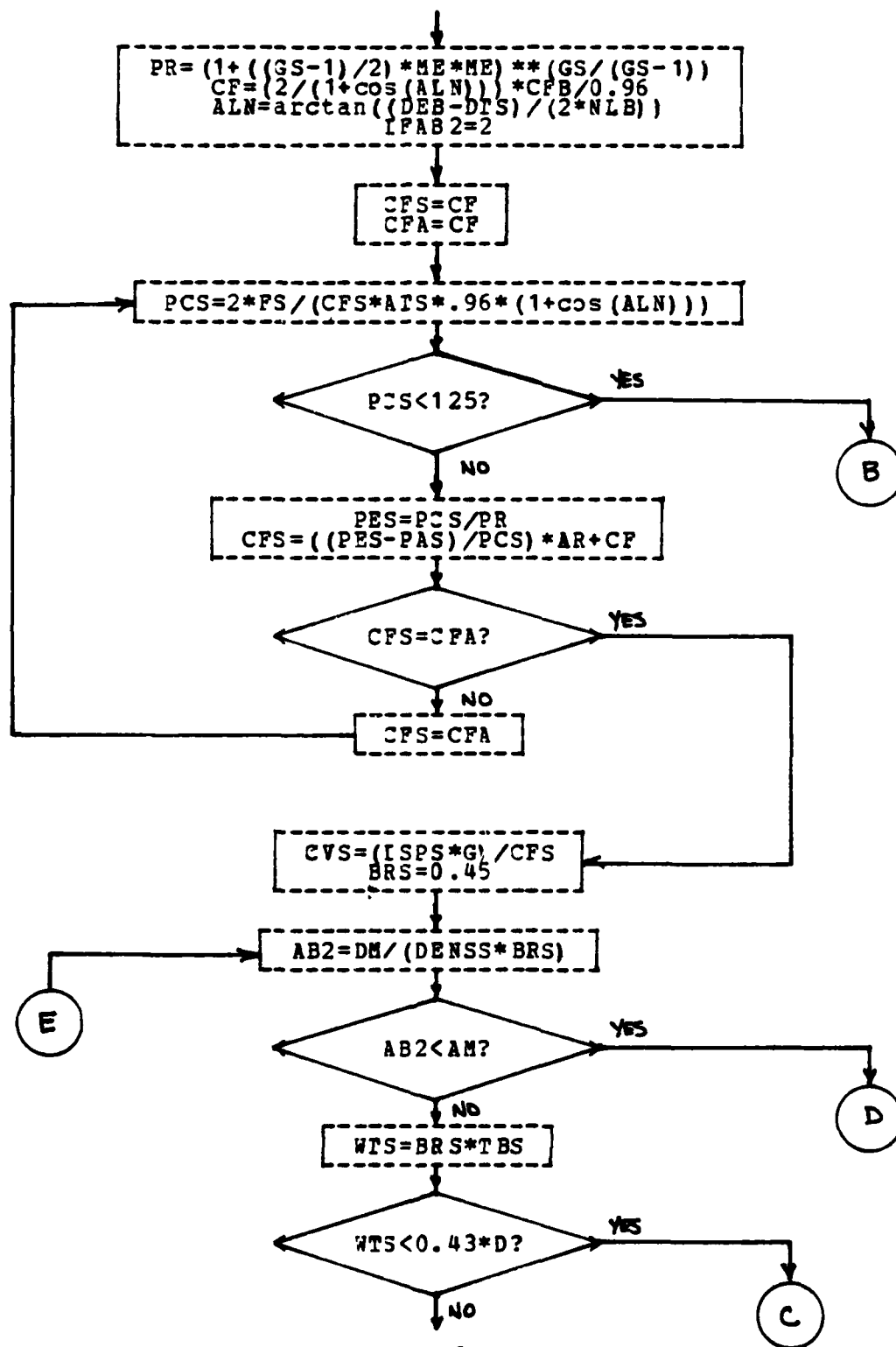


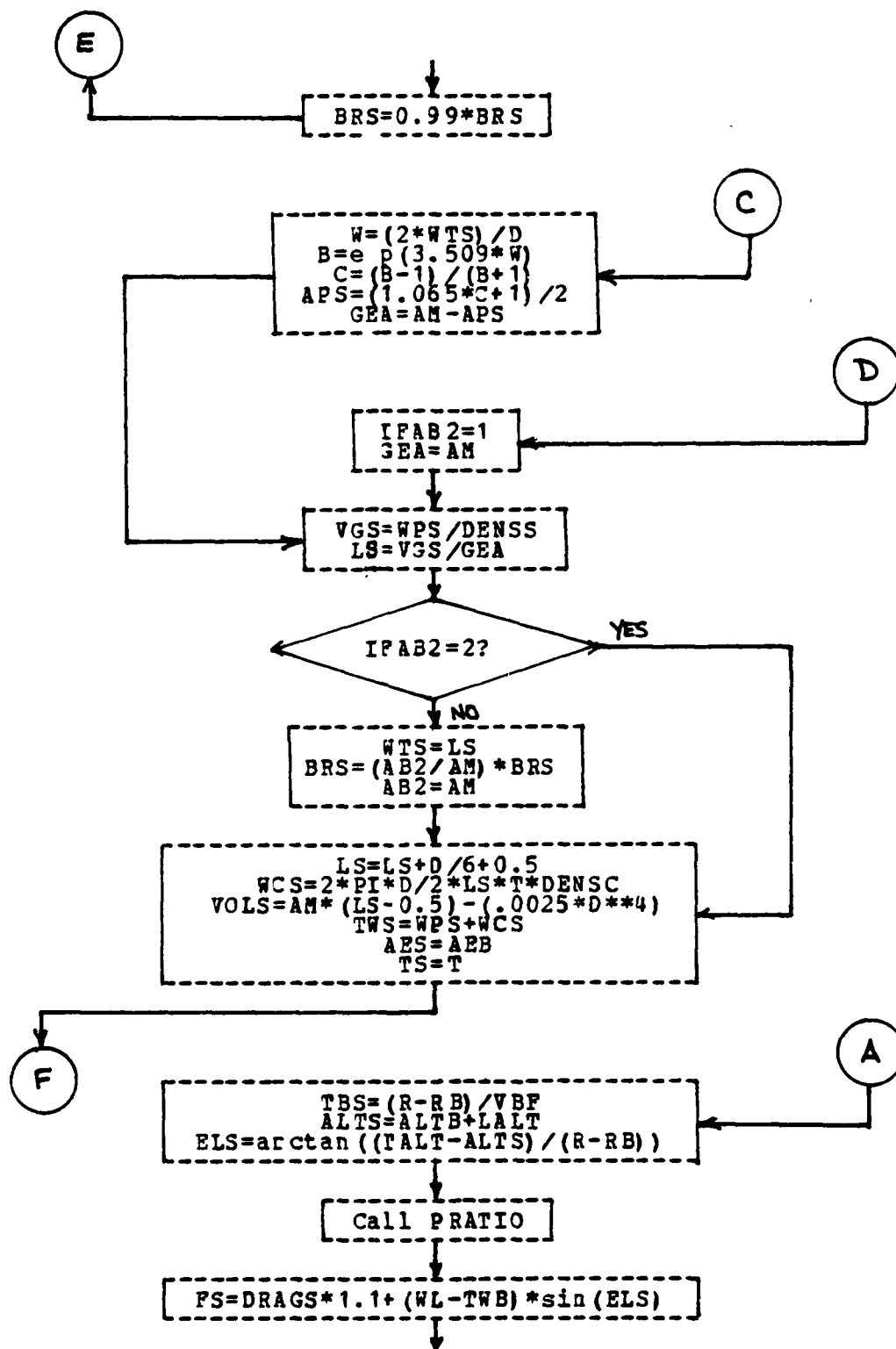


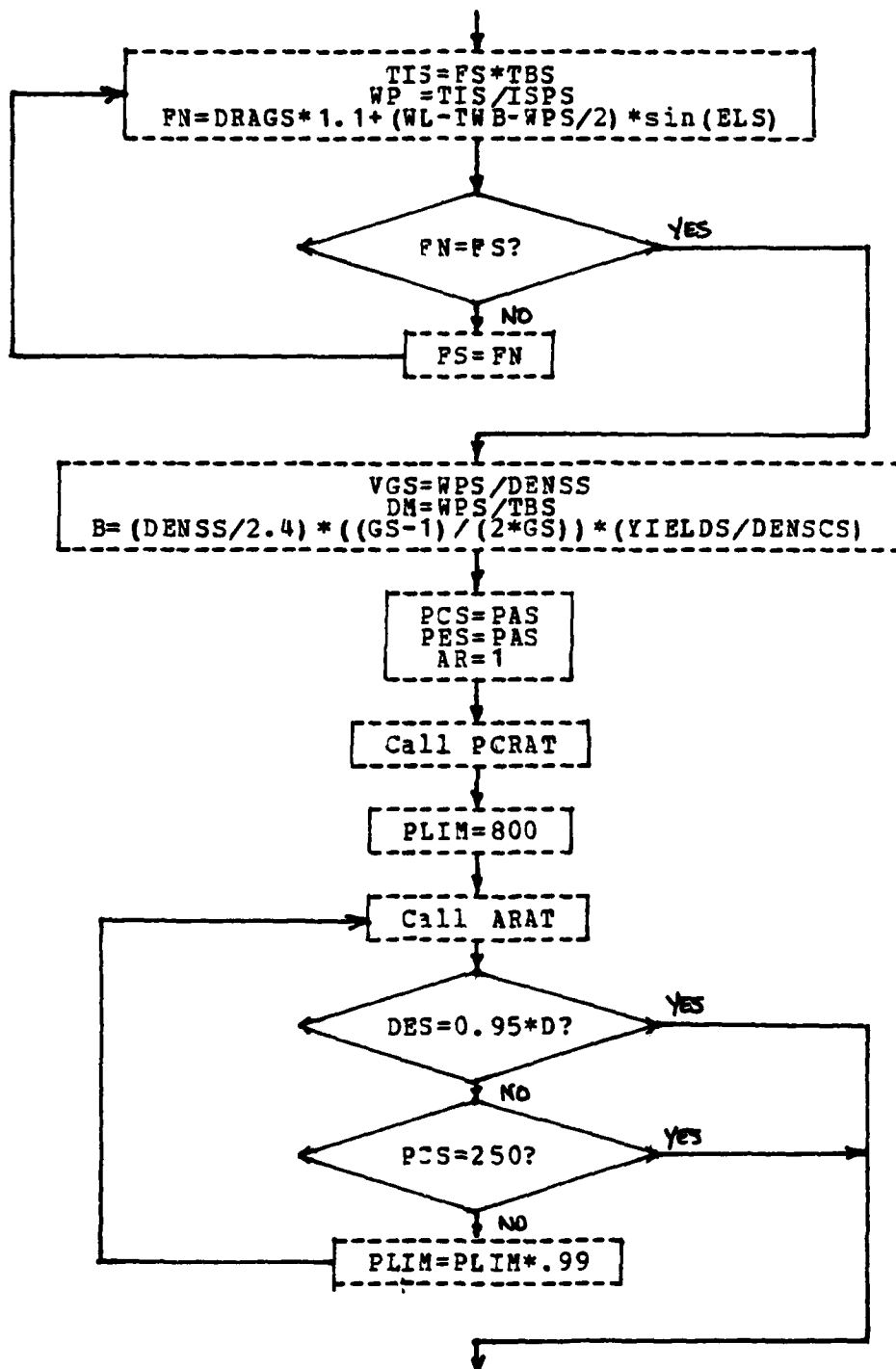


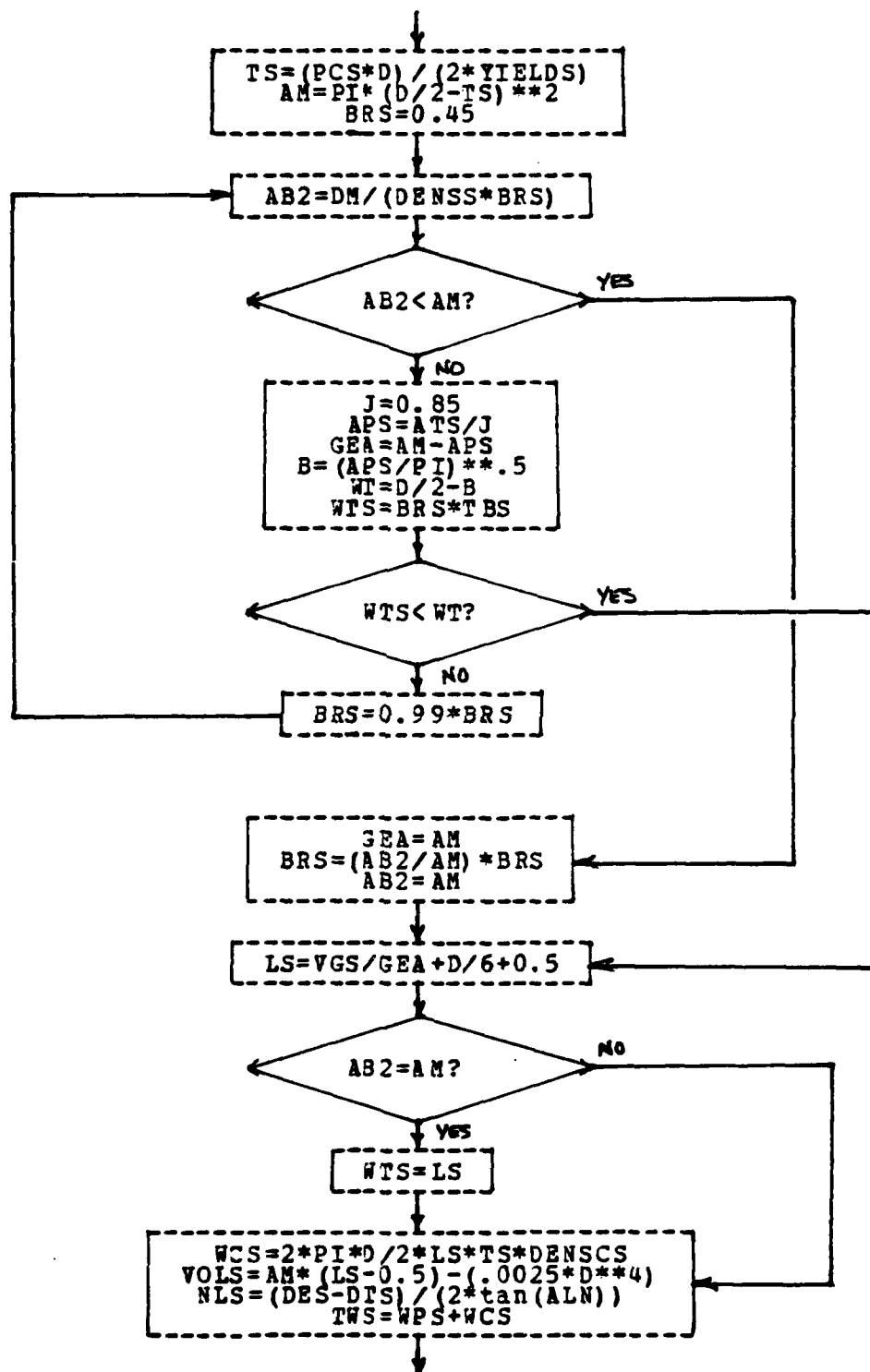


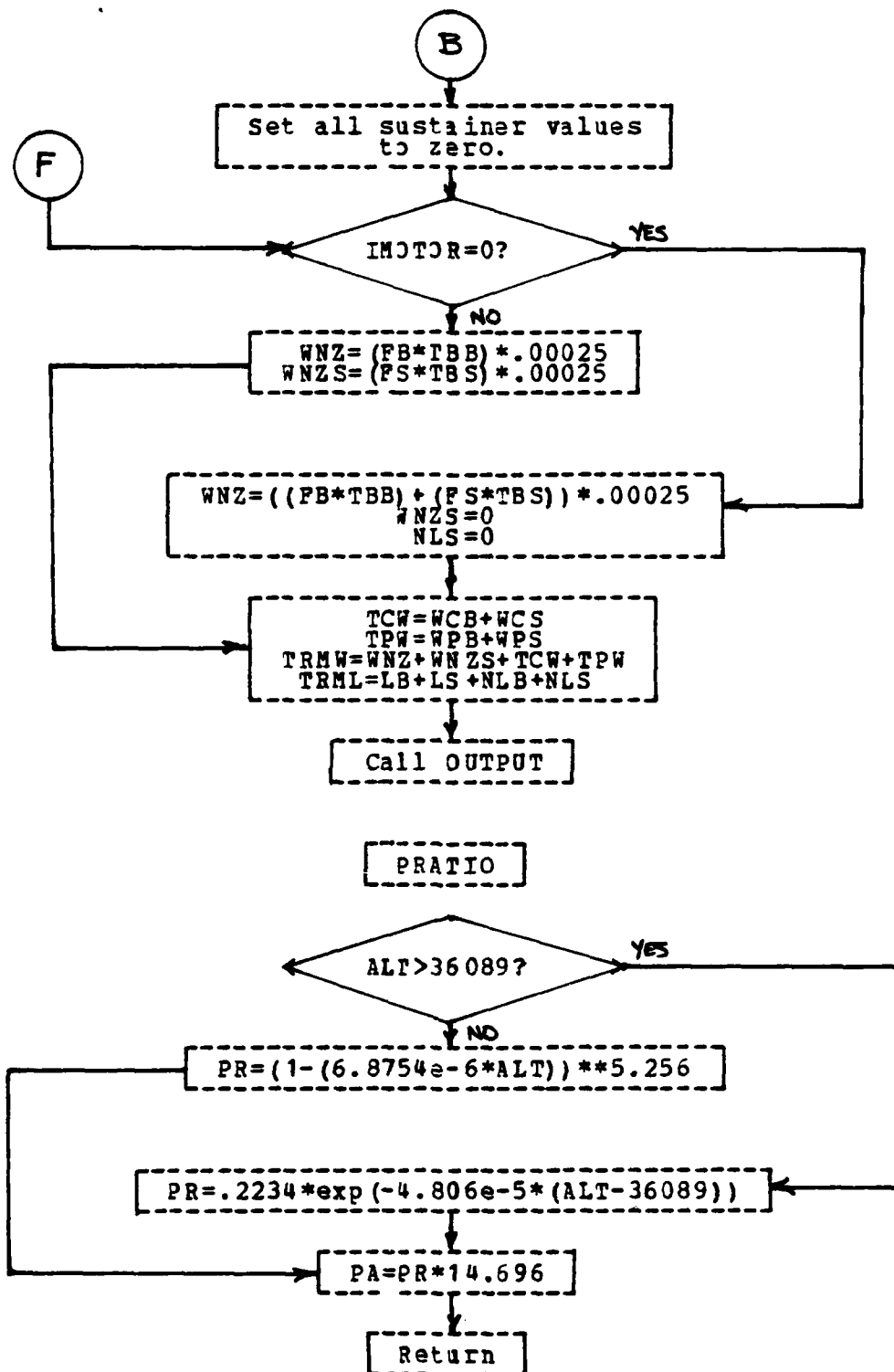


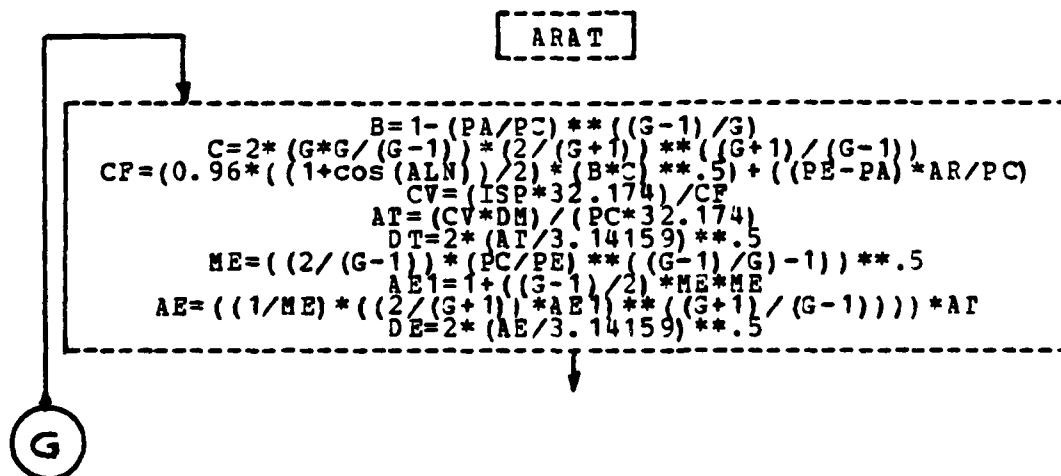
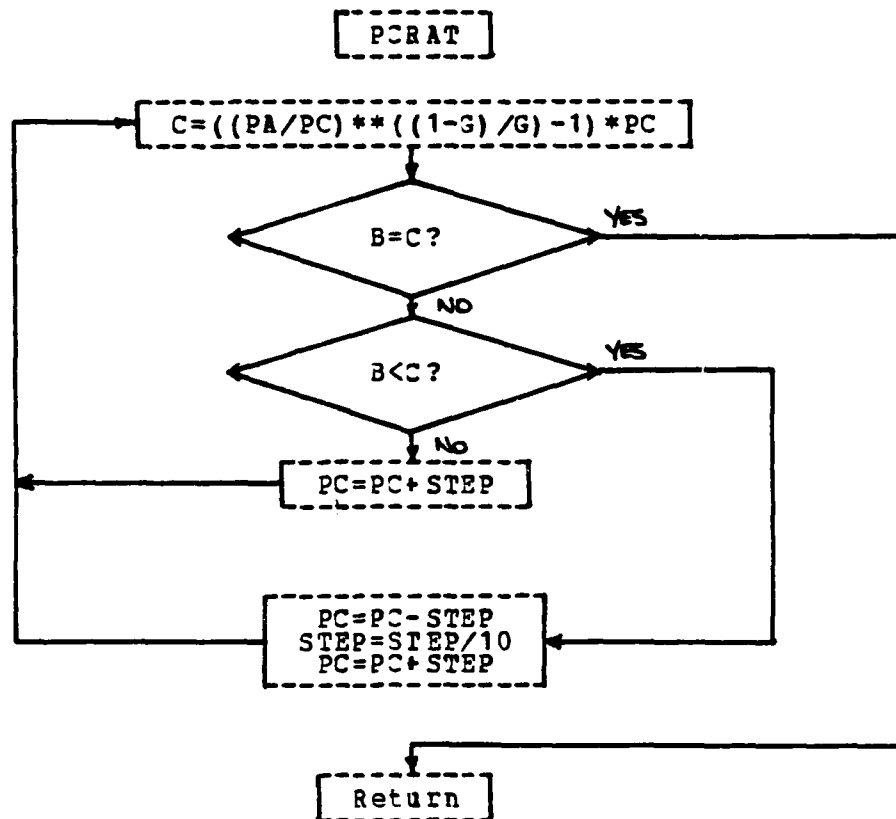




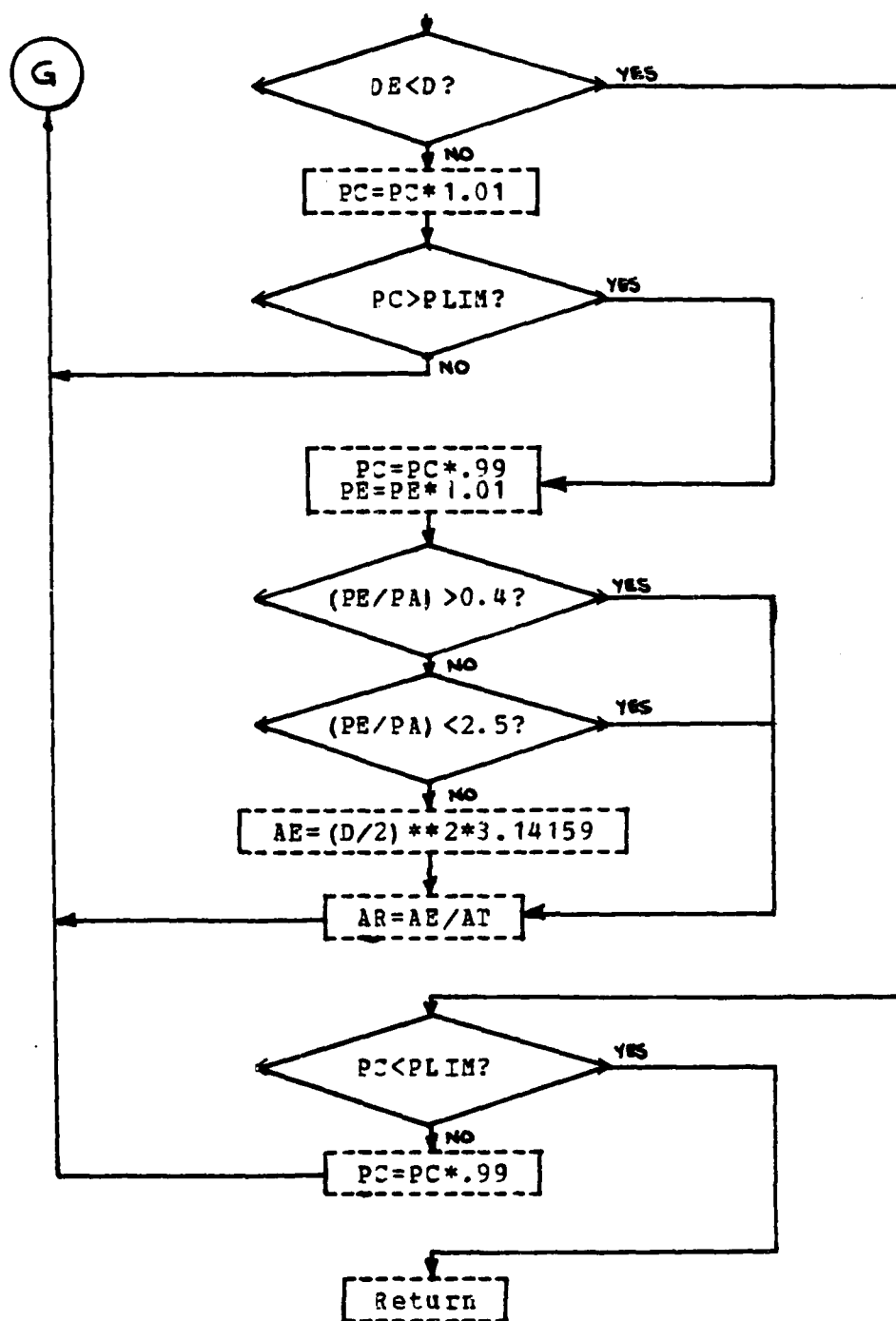












## APPENDIX F. PROPULSION SIZING PROGRAM LISTING

Following this page is the program listing for the Propulsion Sizing Program. It has two segments; the executive routine and the FORTRAN IV computational program. The executive routine establishes the required file definitions and initiates operation of the computational program.

The computational program, LPROP FORTRAN, consists of six subprogram divisions. The MAIN program accepts the input data from the user and performs the guiding calculations for the booster and sustainer motors. Subroutine PRATIO determines the ambient pressures at the design altitudes. Subroutine PCRAT defines the optimum chamber pressure to ambient pressure ratio with respect to the case material properties. Subroutine ARAT solves for the area ratio of the nozzle and tries to size the nozzle to the missile diameter by varying the chamber pressure, characteristic velocity, and thrust coefficient. Subroutine SCREEN is used to prompt the user to clear the terminal screen for proper positioning of the output. And subroutine OUTPUT formats the calculated solutions and provides them to the user and to the printer file, if so directed by the user.

FILE: LPROP EXEC A NAVAL POSTGRADUATE SCHOOL  
FILEDEF 08 DISK LPROP OUTPUT A0 (RECFM VA BLOCK 133 PERM  
&BEGTYPE

YOU WILL HAVE THE OPTION TO OBTAIN A HARDCOPY PRINTOUT OF  
AS MANY ALTERNATIVES AS YOU WISH. THE PROGRAM WILL ASK  
YOU IF YOU DESIRE TO SAVE A PARTICULAR RUN, SIMPLY ANSWER  
ACCORDINGLY.

&END  
LOAD LPROP  
START  
&BEGTYPE

TO OBTAIN A HARDCOPY PRINTOUT OF THE RESULTS, TYPE "PRINT  
LPROP OUTPUT" AND ENTER. THE OUTPUT WILL BE PRINTED ON  
THE VM PRINTER IN ROOM 140 AND WILL BE IDENTIFIED BY YOUR  
USER NUMBER AND LABEL NAME. IT USUALLY REQUIRES SEVERAL  
MINUTES TO OBTAIN THE PRINTOUT.

&END



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6005 READ (5,11001) ELB TO 1260
1005 IF (ICOR.EQ.1) GO TO 1260
      FORMAT (IX,INPUT AVERAGE ACCELERATION DURING BOOST (G*MS**))
      READ (5,11001) A TO 1260
6006 IF (ICOR.EQ.1) GO TO 1260
1006 IF (ICOR.EQ.1) GO TO 1260
      FORMAT (IX,INPUT CRUISE VELOCITY (FT/SEC**))
      READ (5,11001) VBF TO 1260
6007 IF (ICOR.EQ.1) GO TO 1260
1007 IF (ICOR.EQ.1) GO TO 1260
      FORMAT (IX,INPUT DRAG ON MISSILE AT CRUISE VELOCITY (POUNDS**))
      READ (5,11001) DRAGS TO 1260
6008 IF (ICOR.EQ.1) GO TO 1260
1008 IF (ICOR.EQ.1) GO TO 1260
      FORMAT (IX,INPUT MAXIMUM RANGE (NAUTICAL MILES**))
      READ (5,11001) R TO 1260
6009 IF (ICOR.EQ.1) GO TO 1260
1009 IF (ICOR.EQ.1) GO TO 1260
      FORMAT (IX,INPUT FINAL (TARGET) ALTITUDE (FEET**))
      READ (5,11001) TAL TO 1260
6010 IF (ICOR.EQ.1) GO TO 1260
1010 IF (ICOR.EQ.1) GO TO 1260
      FORMAT (IX,INPUT BOOSTER PROPELLANT SPECIFIC IMPULSE (SECONDS**))
      READ (5,11001) ISPB TO 1260
6011 IF (ICOR.EQ.1) GO TO 1260
1011 IF (ICOR.EQ.1) GO TO 1260
      FORMAT (IX,INPUT BOOSTER PROPELLANT DENSITY (LBS/CU.IN**))
      READ (5,11001) DENS8 TO 1260
6012 IF (ICOR.EQ.1) GO TO 1260
1012 IF (ICOR.EQ.1) GO TO 1260
      FORMAT (IX,INPUT BOOSTER EXHAUST SPECIFIC HEAT RATIO**)
      READ (5,11001) GB TO 1260
6013 IF (ICOR.EQ.1) GO TO 1260
1013 IF (ICOR.EQ.1) GO TO 1260
      FORMAT (IX,INPUT SUSTAINER PROPELLANT SPECIFIC IMPULSE (SEC**))
      READ (5,11001) ISPS TO 1260
6014 IF (ICOR.EQ.1) GO TO 1260
1014 IF (ICOR.EQ.1) GO TO 1260
      FORMAT (IX,INPUT SUSTAINER PROPELLANT DENSITY (LBS/CU.IN**))
      READ (5,11001) DENS9 TO 1260
6015 IF (ICOR.EQ.1) GO TO 1260
1015 IF (ICOR.EQ.1) GO TO 1260
      FORMAT (IX,INPUT SUSTAINER EXHAUST SPECIFIC HEAT RATIO**)
      READ (5,11001) GS TO 1260
6016 IF (ICOR.EQ.1) GO TO 1260
1016 IF (ICOR.EQ.1) GO TO 1260
      FORMAT (IX,INPUT NOZZLE HALF ANGLE (DEGREES**))

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LPR00520  
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 LPR00990

LPRO1000  
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LPRO1080  
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LPRO1190  
LPRO1200  
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LPRO1400  
LPRO1410  
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LPRO1430  
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LPRO1450  
LPRO1460  
LPRO1470

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6017 READ (5,1100) ALN
1017 IF (ICOR.EQ.1) GO TO 1260
      WRITE (6,1017)
      FORMAT (1X,INPUT NOZZLE DESIGN ALTITUDE (FEET))
6018 READ (5,1100) ALTB
1018 IF (ICOR.EQ.1) GO TO 1260
      WRITE (6,1018)
      FORMAT (1X,INPUT NOZZLE EROSION RATE (IN/SEC))
6019 READ (5,1100) ER
1019 IF (ICOR.EQ.1) GO TO 1260
      WRITE (6,1019)
      FORMAT (1X,INPUT MISSILE DIAMETER (INCHES))
      READ (5,1100) DB
      D=DB
      IF (ICOR.EQ.1) GO TO 1260
      WRITE (6,1020)
      FORMAT (1X,INPUT YIELD STRENGTH OF CASE MATERIAL (PSI))
      READ (5,1100) YIELD
      YELDS=YIELD
      IF (ICOR.EQ.1) GO TO 1260
      WRITE (6,1021)
      FORMAT (1X,INPUT DENSITY OF THE CASE MATERIAL (LB/CU.IN))
      READ (5,1100) DENS
      DENS=SCS=DENS
      IF (ICOR.EQ.1) GO TO 1260
      GO TO 1201
90 CONTINUE
6022 WRITE (6,1022)
1022 IF (ICOR.EQ.1) GO TO 1260
      WRITE (6,1022)
      FORMAT (1X,INPUT BOOSTER NOZZLE DESIGN ALTITUDE (FEET))
      READ (5,1100) ALTB
      IF (ICOR.EQ.1) GO TO 1260
      WRITE (6,1023)
      FORMAT (1X,INPUT BOOSTER DIAMETER (INCHES))
      READ (5,1100) DB
      IF (ICOR.EQ.1) GO TO 1260
      WRITE (6,1024)
      FORMAT (1X,INPUT YIELD STRENGTH OF BOOSTER CASE MATERIAL (PSI))
      READ (5,1100) YIELD
      IF (ICOR.EQ.1) GO TO 1260
      WRITE (6,1025)
      FORMAT (1X,INPUT DENSITY OF BOOSTER CASE MATERIAL (LBS/CU.IN))
      READ (5,1100) DENS
      IF (ICOR.EQ.1) GO TO 1260
      WRITE (6,1026)
      FORMAT (1X,INPUT SUSTAINER NOZZLE DESIGN ALTITUDE (FEET))
      READ (5,1100) ALTB
      IF (ICOR.EQ.1) GO TO 1260

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6027 WRITE (6,1027)
1027 FORMAT (1X, INPUT SUSTAINER DIAMETER (INCHES))
READ (5,1100) D
IF (ICOR.EQ.1) GO TO 1260
6028 WRITE (6,1028)
1028 FORMAT (1X, INPUT YIELD STRENGTH OF SUSTAINER CASE MATERIAL (PSI))
READ (5,1100) YIELDS
IF (ICOR.EQ.1) GO TO 1260
6029 WRITE (6,1029)
1029 FORMAT (1X, INPUT DENSITY OF SUSTAINER CASE MATERIAL (LBS/CU.IN))
READ (5,1100) DENSCS
IF (ICOR.EQ.1) GO TO 1260
1201 CONTINUE
CALL SCREEN
WRITE (6,1202)
1202 FORMAT (1X, REVIEW THE FOLLOWING LIST OF INPUT PARAMETERS AND RECORD THE NUMBERS, 1X, OF THOSE TO BE CHANGED.//)
ICOR=1
WRITE (6,1210) LALT,WL,VBI,ELB,A,VBF,DRAGS,R,TALT,ISPB,DENSB,GB
1210 FORMAT (1X, SUMMARY OF INPUT PARAMETERS=====,
+5X,.01) LAUNCH ALTITUDE, T45, F12.1, FEET,
+5X,.02) LAUNCH HEIGHT, T45, F12.2, POUNDS,
+5X,.03) LAUNCH VELOCITY, T45, F12.1, FT/SEC,
+5X,.04) LAUNCH ANGLE, T45, F12.1, DEGREES,
+5X,.05) AVERAGE ACCELERATION, T45, F12.2, G'S,
+5X,.06) CRUISE VELOCITY, T45, F12.1, FT/SEC,
+5X,.07) DRAG AT CRUISE VELOCITY, T45, F12.1, POUNDS,
+5X,.08) MAXIMUM RANGE, T45, F12.0, MILES,
+5X,.09) FINAL (TARGET) ALTITUDE, T45, F12.1, FEET,
+5X,.10) BOOSTER PROPELLANT SPECIFIC IMPULSE, T45, F12.1, SEC,
+5X,.11) BOOSTER PROPELLANT DENSITY, T45, F12.4, LBS/CU.IN,
+5X,.12) BOOSTER EXHAUST SPECIFIC HEAT RATIO, T45, F7.5)
WRITE (6,1220) ISPB,DENSB,GS,ALN
1220 FORMAT (5X,.13) SUSTAINER PROPELLANT SPECIFIC IMPULSE, T50, F7.1,
+ SEC,
+5X,.14) SUSTAINER PROPELLANT DENSITY, T45, F12.4, LBS/CU.IN,
+5X,.15) SUSTAINER EXHAUST SPECIFIC HEAT RATIO, T45, F7.5,
+5X,.16) NOZZLE HALF ANGLE, T45, F12.2, DEGREES,
IF (IMOTOR.EQ.1) GO TO 1240
WRITE (6,1230) ALTN,ER,DB,YIELD,DENSC
1230 FORMAT (5X,.17) NOZZLE DESIGN ALTITUDE, T45, F12.1, FEET,
+5X,.18) NOZZLE EROSION RATE, T45, F12.5, IN/SEC,
+5X,.19) MISSILE DIAMETER, T45, F12.1, INCHES,
+5X,.20) YIELD STRENGTH OF CASE MATERIAL, T45, F12.1, PSI,
+5X,.21) DENSITY OF CASE MATERIAL, T45, F12.4, LBS/CU.IN,
GO TO 1250
1240 WRITE (6,1245) ALTN,DB,YIELD,DENSC,ALTN,D,YIELDS,DENSCS
1245 FORMAT (5X,.17) BOOSTER DESIGN ALTITUDE, T45, F12.1, FEET,

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+ /5X, .18) BOOSTER DIAMETER, T45, F12.2, INCHES, LPR01960
+ /5X, .19) YIELD STRENGTH OF BOOSTER CASE, T45, F12.1, PSI, LPR01970
+ /5X, .20) DENSITY OF BOOSTER CASE MATERIAL, T45, F12.4, LBS/CU.IN, LPR01980
+ /5X, .21) SUSTAINER DESIGN ALTITUDE, T45, F12.1, FEET, LPR01990
+ /5X, .22) SUSTAINER DIAMETER, T45, F12.2, INCHES, LPR02000
+ /5X, .23) YIELD STRENGTH OF SUSTAINER CASE, T45, F12.1, PSI, LPR02010
+ /5X, .24) DENSITY OF SUSTAINER CASE MATERIAL, T45, F12.4, LBS/CU.IN, LPR02020
+ , LPR02030
1250 CONTINUE LPR02040
WRITE (6, 1254) LPR02050
1254 FORMAT (/IX, 'HOW MANY INPUT PARAMETERS DO YOU WISH TO CHANGE? (TWO LPR02060
+ DIGIT INTEGER, PLEASE)') LPR02070
READ (5, 1110) N LPR02080
IF (N.EQ.0) GO TO 1301 LPR02090
DO 1260 I=1, N LPR02100
1255 WRITE (6, 1256) LPR02110
1256 FORMAT (IX, 'INPUT TWO DIGIT ITEM NUMBER OF PARAMETER TO BE CHANL LPR02120
+ GED.') LPR02130
READ (5, 1110) IGO LPR02140
IF ((IGO.GE.1).AND.(IGO.LE.24)) GO TO 1258 LPR02150
WRITE (6, 1257) IGO LPR02160
FORMAT (IX, 'WRONG ', I2, ' IS NOT A VALID CHOICE. TRY AGAIN.') LPR02170
GO TO 1255 LPR02180
IF ((IMOTOR.EQ.1).AND.(IGO.GT.16)) IGO=IGO+5 LPR02190
GO TO (6001, 6002, 6003, 6004, 6005, 6006, 6007, 6008, 6009, 6010, 6011, LPR02200
+ 6012, 6013, 6014, 6015, 6016, 6017, 6018, 6019, 6020, 6021, 6022, 6023, 6024, LPR02210
+ 6025, 6026, 6027, 6028, 6029), IGO LPR02220
1260 CONTINUE LPR02230
GO TO 1201 LPR02240
1301 CONTINUE LPR02250
CALL SCREEN LPR02260
PI=3.1415927 LPR02270
G=32.174 LPR02280
ALN=DETORA(ALN) LPR02290
ELB=DETORA(ELB) LPR02300
R=R*6080. LPR02310
C=====BOOSTER MOTOR CALCULATIONS===== LPR02320
C LPR02330
DV=VBF-VBI LPR02340
DF=(VBF*VBF)/DRAGS LPR02350
DRAGB=(VBF*VBI)**2./(4.*DF) LPR02360
FB=(WLA+A)+DRAGB LPR02370
DM=FB/ISP8 LPR02380
TBB=DV/(A*G) LPR02390
RB=(VBI+0.5*DV)*TBB*COS(ELB) LPR02400
ALT8=(VBI+0.5*DV)*TBB*SIN(ELB)+LALT LPR02410
CALL PRATIO (ALTN, PAB) LPR02420
LPR02430

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C 100 WPB=TBB*DM
      TIB=WPB*ISPB
      FB=TIB/TBB
      B=DV/(G*TBB)+SIN(ELB)
      WN=WL*(1.-EXP((-WPB/(FB-DRAGB))*B))
      IF (ABS(WPB-WN).LT.0.01) GO TO 110
      WPB=WN
      GO TO 100

C 110 CONTINUE
      WPB=WN
      DM=WPB/TBB

C 113 CONTINUE
      VGB=WPB/DENSB
      STEP=100.
      B=(DENSB/2.4)*((GB-1.)/(2.*GB))*(YIELD/DENSC)
      PCB=PAB
      PEB=PAB
      AR=1.
      IFDLMB=0
      CALL PCRRAT (PAB,PCB,GB,B,STEP)
      PLIM=2000.
      140 CALL ARAT (PAB,PCB,GB,PEB,ISPB,DB,CFB,CVB,ATB,DTB,AEB,DEB,IFDLMB,
      +IFPCB,AR,ALN,DM,PLIM,IMOTOR)
      IF ((IMOTOR.EQ.0).OR.(DEB.GE.(0.95*DB))).OR.(PCB.LT.1000) GO TO 150
      PLIM=PLIM*.99
      GO TO 140

C 150 CONTINUE
      Y=(PCB*DB)/(2.*YIELD)
      J=0.85
      160 APB=ATB/J
      AM=PI*(DB/2.-T)**2.
      GEA=AM-APB
      IFBRB=0
      BRB=1.25
      B=(APB/PI)**0.5
      C=DB/2.-B

C 165 ABB=DM/(DENSB*BRB)
      WTB=BRB*TBB
      IF (WTB.LT.C) GO TO 170
      BRB=0.99*BRB
      IFBRB=1
      GC TO 165

C

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LPR02440
LPR02450
LPR02460
LPR02470
LPR02480
LPR02490
LPR02500
LPR02510
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LPR02570
LPR02580
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LPR02600
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LPR02870
LPR02880
LPR02890
LPR02900
LPR02910

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170 LB=VGB/GEA
LB=LB+DB/6+.05
WCB=2.*PI*DB/2.*LB*T*DENSCL
VOLB=AM*((LB-0.5)-(.0025*DB**4.))
NLB=(DEB-DTB)/(2*TAN(ALN))
TWB=WPB+WCB
      WRITE (6,9000)
      FORMAT (IX,'MADE IT THIS FAR.')
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9000 IFBSTO=1
      IF (RB.GT.R) GO TO 999
      IFBSTO=0
      IF (IMOTOR.EQ.1) GO TO 300
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C=====SUSTAINER MOTOR CALCULATIONS (COMMON NOZZLE)=====
C
200 TBS=(R-RB)/VBF
      ALTS=ALTB+LALT
      ELS=ATAN((TALT-ALTS)/(R-RB))
      ALTS=VBF*SIN(ELS)*TBS*0.5+ALTS
      CALL PRATIO (ALTSN,PAS)
      FS=DRAGS*1.1+(WL-WPB)*SIN(ELS)
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C 201 TIS=FS*TBS
      WPS=TIS/ISPS
      FN=DRAGS*1.1+(WL-WPB-WPS/2)*SIN(ELS)
      IF (ABS(FN-FS).LT.0.01) GO TO 210
      FS=FN
      GO TO 201
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```

C 210 CONTINUE
      FS=FN
      DM=WPS/TBS
      DTS=DTB+ER*(TBB+TBS*0.5)
      ATS=.25*PI*DTS*DTS
      AR=ARB/ATS
      ME=1.
      STEP=1.
```

```

C 220 ARN1=1.+(GS-1.)*ME*ME/2.
      ARN=((GS+1.)*ARN1)**((GS+1.)/(2.*(GS-1.)))/ME
      IF (ABS(ARN-AR).LT.0.001) GO TO 240
      IF (ARN.GT.AR) GO TO 230
      ME=ME+STEP
      GO TO 220
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230 CONTINUE
      ME=ME-STEP
      STEP=STEP/10.
      ME=ME+STEP
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LPR03400  
LPR03410  
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LPR03450  
LPR03460  
LPR03470  
LPR03480  
LPR03490  
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LPR03860  
LPR03870

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C 240 GO TO 220
      CONTINUE
      PR=(1.+(GS-1.)/2.)*ME*ME)**(GS/(GS-1.))
      CF=(2/(1.+COS(ALN)))*CFB/0.96
      ALN=ATAN(DEB-DTS)/(2.*NLB)
      CFS=CF
      CFA=CF
      IFPCS=0
      IFAB2=2
      IFBRS=0

C 250 PCS=2.*FS/(CFS*ATS*0.96*(1.+COS(ALN)))
      IF (PCS.GT.125.) GO TO 251
      IFAB2=0
      IFBRS=1
      IFPCS=2
      GO TO 999
      PES=PCS/PR
      CFS=((PES-PAS)/PCS)*AR+CF
      IF (ABS(CFS-CFA).LT.0.001) GO TO 260
      CFA=CFS
      GO TO 250

251

C 260 CONTINUE
      CVS=(1/SPS*G)/CFS
      BRS=0.45

C 270 AB2=DM/(DENSS*BRS)
      IF (AB2.LT.AM) GO TO 280
      WTS=BRS*1BS
      IF (WTS.LT.(0.43*D)) GO TO 275
      BRS=0.99*BRS
      IFBRS=1
      GO TO 270

C 275 W=(2.*WTS)/D
      B=EXP(3.509*W)
      C=(B-1.)/(B+1.)
      APS=(1.065*C+1.)/2.
      GEA=AM-APS
      GO TO 285

280 IFAB2=1
      GEA=AM

285 VGS=WPS/DENSS
      LS=VGS/GEA
      IF (IFAB2.EQ.2) GO TO 290
      WTS=LS

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BRS=(AB2/AM)*BRS
AB2=AM
IFBRS=1

C 290 CONTINUE
LS=LS+D/6+.5
WCS=2*PI*D/2.*LS*T*DENS
VOLS=AM*(LS-.5)-(.0025*D**4.)
TWS=WPS+WCS
AES=1000000000000000000.
ATS=100000000000000000.
TS=T
GO TO 998

C=====SUSTAINER MOTOR CALCULATIONS (STAGED MOTORS)=====
C 300 TBS=(R-RB)/VBF
ALTS=ALTB+LALT
ELS=ATAN((TALT-ALTS)/(R-RB))
CALL PRATIO (ALTSN,PAS)
FS=DRAGS*1.1+(WL-TWB)*SIN(ELS)

C 305 TIS=FS*TBS
WPS=TIS/ISPS
FN=DRAGS*1.1+(WL-TWB-WPS/2.)*SIN(ELS)
IF (ABS(FN-FS).LT.0.01) GO TO 310
FS=FN
GO TO 305

C 310 CONTINUE
VGS=WPS/DENSS
DM=WPS/TBS
STEP=100.
B=(DENSS/2.4)*((GS-1.)/(2.*GS))*(YIELDS/DENSCS)
PCS=PAS
PES=PAS
AR=1.
IFDLM=0
CALL PCRAT (PAS,PCS,GS,B,STEP)
PLIM=800.
315 CALL ARAT (PAS,PCS,GS,PES,ISPS,D,CFS,CVS,ATS,DTS,AES,DES,IFDLM,
+IFPCS,AR,ALN,DM,PLIM,MOTOR)
IF ((DES*GE.(0.95*DI)).OR.(PCS.LT.250)) GO TO 320
PLIM=PLIM*.99
GO TO 315

C 320 CONTINUE
TS=(PCS*DI)/(2.*YIELDS)

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LPR03880  
 LPR03890  
 LPR03900  
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 LPR03980  
 LPR03990  
 LPR04000  
 LPR04010  
 LPR04020  
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 LPR04210  
 LPR04220  
 LPR04230  
 LPR04240  
 LPR04250  
 LPR04260  
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 LPR04280  
 LPR04290  
 LPR04300  
 LPR04310  
 LPR04320  
 LPR04330  
 LPR04340  
 LPR04350

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AM=PI*(D/2.-TS)**2.
BRS=0.45
IFAB2=2
IFBRS=0

C 330 AB2=DM/(DENS*BR)
      IF (AB2.LT.AM) GO TO 340
      J=0.85
      APS=ATS/J
      GEA=AM-APS
      B=(APS/PI)**0.5
      C=D/2.-B
      WTS=BR*TS
      IF (WTS.LT.C) GO TO 360
      BRS=0.99*BR
      IFBRS=1
      GO TO 330

C 340 CONTINUE
      IFAB2=1
      GEA=AM
      BRS=(AB2/AM)*BR
      AB2=AM

C 360 CONTINUE
      LS=VGS/GEA
      LS=LS+D/3.+0.5
      LB=LB+DB/6.
      IF (AB2.EQ.AM) WTS=LS
      WCS=2.*PI*D/2.*LS*TS*DENS*CS
      VOL=AM*(LS-0.5)-(.0025*D**4.)
      NLS=(DES-DTS)/(2.*TAN(ALN))
      WTS=WPS+WCS
      GO TO 998

C=====
C 999 WPS=0.
      WCS=0.
      TWS=0.
      CFS=0.
      CVS=0.
      FTS=0.
      TBS=0.
      PCS=0.
      ABS=0.
      WTS=0.
      APS=0.

```

```

LPR04360
LPR04370
LPR04380
LPR04390
LPR04400
LPR04410
LPR04420
LPR04430
LPR04440
LPR04450
LPR04460
LPR04470
LPR04480
LPR04490
LPR04500
LPR04510
LPR04520
LPR04530
LPR04540
LPR04550
LPR04560
LPR04570
LPR04580
LPR04590
LPR04600
LPR04610
LPR04620
LPR04630
LPR04640
LPR04650
LPR04660
LPR04670
LPR04680
LPR04690
LPR04700
LPR04710
LPR04720
LPR04730
LPR04740
LPR04750
LPR04760
LPR04770
LPR04780
LPR04790
LPR04800
LPR04810
LPR04820
LPR04830

```

```

BRS=0.
VLS=0.
VOLTS=0.
ATS=0.
AES=0.
NLS=0.
TS=0.
998 IF (IMOTOR.EQ.0) GO TO 910
    WNZ=(FB*TBBS)*.00025
    WNZS=(FS*TBBS)*.00025
    GO TO 915
910 WNZ=((FB*TBBS)+(FS*TBBS))*0.00025
    WNZS=0.
915 TCW=WCB+WCS
    TPW=WPB+WPS
    TRMW=WNZ+WNZS+TCW+TPW
    IF TRMW=0
    IF (TRMW.GT.(0.75*WL)) IFTRMW=1
    IF (TRMW.LT.(0.25*WL)) IFTRMW=1
    TRML=LB+LS+NLB+NLS
    IFTRML=0
    IF (TRML.GT.(15.*D)) IFTRML=1
    IF (IMOTOR.EQ.0) WNZS=1000000000000000000000.
    IF (IMOTOR.EQ.0) NLS=1000000000000000000000.
    ALN=ATAN((DEB-DTB)/(2.*NLB))
    ALB=RATODE(ALN)
    R=R/6080.
    CALL OUTPUT
    WRITE (6,800)
    FORMAT (1X,'DO YOU WANT TO REPEAT THIS PROBLEM?')
    READ (5,1120) IRPT
    IF (IRPT.EQ.1) GO TO 1201
    WRITE (6,810)
    FORMAT (1X,'DO YOU WANT TO RUN A NEW PROBLEM?')
    READ (5,1120) IRPT
    IF (IRPT.EQ.1) GO TO 997
    CALL SCREEN
    STOP
    END
SUBROUTINE PRATIO (ALT,PA)
REAL ALT,PA,PR
IF (ALT.GT.36089.) GO TO 10
PR=(1.-(.6.8754E-6*ALT))**5.256

```

```

C      CALL OUTPUT
      WRITE (6,800)
      FORMAT (1X,'DO YOU WANT TO REPEAT THIS PROBLEM? (0=NO,1=YES)')
      800 READ (5,1120) IRPT
      IF (IRPT.EQ.1) GO TO 1201
      WRITE (6,810)
      810 FORMAT (1X,'DO YOU WANT TO RUN A NEW PROBLEM? (0=NO,1=YES)')
      READ (5,1120) IRPT
      IF (IRPT.EQ.1) GO TO 997
      CALL SCREEN
      STOP
      END
      SUBROUTINE PRATIO (ALT,PA)
      REAL ALT,PA,PR
      IF (ALT.GT.36089.) GO TO 10
      PR=(1.-(6.8754E-6*ALT))**5.256

```

```

C
10 GO TO 20
20 PR=.2234*EXP(-4.806E-5*(ALT-36089.))
20 PA=PR*14.696
20 RETURN
END

SUBROUTINE PCRAT (PA,PC,G,B,STEP)
REAL PA,PC,G,B,STEP
C=((PA/PC)*{(1.-G)/G)-1.)*PC
IF (ABS(B-C).LT.0.01) GO TO 30
IF (B.LT.C) GO TO 20
PC=PC+STEP
GO TO 10
20 CONTINUE
PC=PC-STEP
STEP=STEP/10.
PC=PC+STEP
GO TO 10
30 CONTINUE
RETURN
END

C
SUBROUTINE ARAT (PA,PC,G,PE,ISP,D,CF,CV,AT,DT,AE,DE,IFDL,IFPC,AR,
+ALN,DM,PLIM,IMOTOR)
REAL PA,PC,G,PE,ISP,D,CF,CV,AT,DT,AE,DE,B,C,ME,ALN,DM,AR,PLIM
INTEGER IFDL,IFPC,IMOTOR
IFPC=0
10 B=1.-(PA/PC)*{(G-1.)/G}
C=2.*(G*(G-1.))*{(2.)/(G+1.))*{(G+1.)/(G-1.)}
CF=(0.96*(1.+COS(ALN))/2.)*(B*C)**0.5)+{(PE-PA)*AR/PC}
CV=(ISP*32.174)/CF
AT=2*(AT/3.1415927)**0.5
ME=((2.)/(G-1.))*{(PC/PE)**((G-1.)/G)-1.))*0.5
AE1=1.+(G-1.)/2.)*ME*ME
AE=((1.)/ME)*{(2.)/(G+1.))*AE1**((G+1.)/(2.)*(G-1.)))*AT
DE=2.*(AE/3.1415927)**0.5
IF ((DE.LE.D).AND.((IMOTOR.EQ.1)) GO TO 30
IF ((PE/PA).LT.0.5).OR.((PE/PA).GT.2.2)) GO TO 30
IFDL=1
PC=PC/.999
IF (PC.GT.PLIM) GO TO 20
GO TO 10
20 PC=PC*.999
PE=PE/.999
IF (((PE/PA).GT.0.4).AND.((PE/PA).LT.2.5)) GO TO 25
LPR05320
LPR05330
LPR05340
LPR05350
LPR05360
LPR05370
LPR05380
LPR05390
LPR05400
LPR05410
LPR05420
LPR05430
LPR05440
LPR05450
LPR05460
LPR05470
LPR05480
LPR05490
LPR05500
LPR05510
LPR05520
LPR05530
LPR05540
LPR05550
LPR05560
LPR05570
LPR05580
LPR05590
LPR05600
LPR05610
LPR05620
LPR05630
LPR05640
LPR05650
LPR05660
LPR05670
LPR05680
LPR05690
LPR05700
LPR05710
LPR05720
LPR05730
LPR05740
LPR05750
LPR05760
LPR05770
LPR05780
LPR05790

```

```

      AE=(D/2.)*2.*3.1415927
      AR=AE/AT
      IFPC=1
      GO TO 10
30    CONTINUE
      IF (PC.LT.PLIM) GO TO 40
      PC=PC*.999
      GO TO 10
40    RETURN
      ENC

      SUBROUTINE SCREEN
      WRITE (6,600)
      FORMAT (1X,'CLEAR SCREEN AND ENTER "0"')
      READ (5,16) ISCR
      IF (ISCR.EQ.0) GO TO 10
      RETURN
      END

      SUBROUTINE OUTPUT
      REAL WPB,WCS,TWB,CFB,CVB,FB,TBB,RB,PCB,ABB,WTB,APB,LB,VOLB,ATB,BRB
      REAL WPS,WCS,TWS,CFS,CVS,FS,TBW,TPW,TBW,TRML,T,AES
      REAL NLB,AEB,WNZ,TPW,TBW,TRML,T,AES
      REAL VBF,VBI,YIELD,DENSC,ALN,ER,D,R,WL,A,ELB,ISPB
      REAL DENSC,GB,LALT,DRAGS,TALT,ISPS,GS,DENSC,DB
      REAL YIELDS,DENSCS,TS,WNZS,NLS,ALTN,ALTSN
      INTEGER IFBRB,IFDLMB,IFAB2,IFBRS,IFPCB,IFTRMW,IFBSTD,IFTRML,IFPCS
      COMMON WPB,WCS,TWB,CFB,CVB,FB,TBB,RB,PCB,ABB,WTB,APB,LB,VOLB
      COMMON ATB,BRCB,NLB,AEB,WNZ,TPW,TBW,TRML,T
      COMMON WPS,WCS,TWS,CFS,CVS,FS,TBW,TPW,TBW,TRML,T
      COMMON VBF,VBI,YIELD,DENSC,ALN,ER,D,R,WL,A,ELB,ISPB
      COMMON DENSC,GB,LALT,DRAGS,TALT,ISPS,GS,DENSC,DB
      COMMON YIELDS,DENSCS,TS,WNZS,NLS,ALTN,ALTSN
      COMMON IFBRB,IFDLMB,IFAB2,IFBRS,IFPCB,IFTRMW,IFBSTD,IFTRML,IFPCS
      COMMON IFDLMS,IMOTOR
      WRITE (6,1000)
      FORMAT (1X,'BOOSTER',T55,'SUSTAINER')
      WRITE (6,1010) WPB,WPS,WCS,WCB,MCS,TWB,TWS,CFB,CFS,CVB,CVS,FB,FS
      FORMAT (1X,'PROPELLANT WEIGHT',T35,F7.2,' LBS',T55,F7.2,' LBS',/
      +1X,'CASING WEIGHT',T35,F7.2,' LBS',T55,F7.2,' LBS',/
      +1X,'TOTAL WEIGHT',T35,F7.2,' LBS',T55,F7.2,' LBS',/
      +1X,'THRUST COEFFICIENT',T35,F7.4,' FT/SEC',T55,F7.1,' FT/SEC',
      +1X,'THRUST VELOCITY',T35,F7.1,' LBS',T55,F7.1,' LBS',/
      +1X,'CHARACTER',T35,F7.1,' LBS',T55,F7.1,' LBS',/
      WRITE (6,1020) TBB,TBS,RB,PCB,PCS,ABB,AB2,WTB,WTS,APB,APS

```



LPR06280  
LPR06290  
LPR06300  
LPR06310  
LPR06320  
LPR06330  
LPR06340  
LPR06350  
LPR06360  
LPR06370  
LPR06380  
LPR06390  
LPR06400  
LPR06410  
LPR06420  
LPR06430  
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LPR06460  
LPR06470  
LPR06480  
LPR06490  
LPR06500  
LPR06510  
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LPR06580  
LPR06590  
LPR06600  
LPR06610  
LPR06620  
LPR06630  
LPR06640  
LPR06650  
LPR06660  
LPR06670  
LPR06680  
LPR06690  
LPR06700  
LPR06710  
LPR06720  
LPR06730  
LPR06740  
LPR06750

```

1250 IF (IFAB2.EQ.1) WRITE (6,1250)
    FORMAT (/IX,'THE SUSTAINER MOTOR HAS AN END-BURNING GRAIN.')
```

LPR06760  
LPR06770  
LPR06780  
LPR06790  
LPR06800  
LPR06810  
LPR06820  
LPR06830  
LPR06840  
LPR06850  
LPR06860  
LPR06870  
LPR06880  
LPR06890  
LPR06900  
LPR06910  
LPR06920  
LPR06930  
LPR06940  
LPR06950  
LPR06960  
LPR06970  
LPR06980  
LPR06990  
LPR07000  
LPR07010  
LPR07020  
LPR07030  
LPR07040  
LPR07050  
LPR07060  
LPR07070  
LPR07080  
LPR07090  
LPR07100  
LPR07110  
LPR07120  
LPR07130  
LPR07140  
LPR07150  
LPR07160  
LPR07170  
LPR07180  
LPR07190  
LPR07200  
LPR07210  
LPR07220  
LPR07230

```

1260 IF (IFTRM.EQ.1) WRITE (6,1260)
    FORMAT (/IX,'ESTIMATION OF LAUNCH WEIGHT IS REQUIRED FOR THESE
+ISSILE PERFORMANCE.'/IX,'PARAMETERS.')
```

```

1270 IF (IFTRML.EQ.1) WRITE (6,1270)
    FORMAT (/IX,'ENLARGEMENT OF DIAMETER IS RECOMMENDED DUE TO A VERY
+HIGH LENGTH-TO-DIAMETER.'/IX,'RATIO FOR THE MOTOR.')
```

```

1300 WRITE (6,1300)
    FORMAT (/IX,'DO YOU WANT TO HAVE THIS AS HARDCOPY OUTPUT? (0=NO,1=
+YES).')
```

```

1310 READ (5,1310) ICOPY
    FORMAT (I1)
    IF (ICOPY.EQ.0) GO TO 1500
```

```

208 IF (IMOTOR.EQ.0) WRITE (8,208)
    FORMAT (/IX,'INTEGRAL MOTORS (COMMON NOZZLE)')
```

```

209 IF (IMOTOR.EQ.1) WRITE (8,209)
    FORMAT (/IX,'STAGED MOTORS (INDEPENDENT NOZZLES)')
```

```

210 WRITE (8,210) ALT,BN,ELB,A,VBF,DRAGS,R,TALT,ISPB,DENSB,GB
    FORMAT (IX,'SUMMARY OF INPUT PARAMETERS=====',
+ /5X,'1) LAUNCH ALTITUDE',T45,F12.1,' FEET',
+ /5X,'2) LAUNCH WEIGHT',T45,F12.2,' POUNDS',
+ /5X,'3) LAUNCH VELOCITY',T45,F12.1,' FT/SEC',
+ /5X,'4) LAUNCH ANGLE',T45,F12.1,' DEGREES',
+ /5X,'5) AVERAGE ACCELERATION',T45,F12.2,' G'S',
+ /5X,'6) CRUISE VELOCITY',T45,F12.1,' FT/SEC',
+ /5X,'7) DRAG AT CRUISE VELOCITY',T45,F12.1,' POUNDS',
+ /5X,'8) MAXIMUM RANGE',T45,F12.0,' MILES',
+ /5X,'9) FINAL (TARGET) ALTITUDE',T45,F12.1,' FEET',
+ /5X,'10) BOOSTER PROPELLANT SPECIFIC IMPULSE',T45,F12.1,' SEC',
+ /5X,'11) BOOSTER PROPELLANT DENSITY',T45,F12.4,' LBS/CU.IN',
+ /5X,'12) BOOSTER EXHAUST SPECIFIC HEAT RATIO',T50,F7.5)
    WRITE (8,220) ISPB,DENSB,GB,ALN
```

```

220 FORMAT (5X,'13) SUSTAINER PROPELLANT SPECIFIC IMPULSE',T50,F7.1,
+ , SEC',
+ /5X,'14) SUSTAINER PROPELLANT DENSITY',T45,F12.4,' LBS/CU.IN',
+ /5X,'15) SUSTAINER EXHAUST SPECIFIC HEAT RATIO',T50,F7.5,
+ /5X,'16) NOZZLE HALF ANGLE',T45,F12.2,' DEGREES')
    IF (IMOTOR.EQ.1) GO TO 240
```

```

230 WRITE (8,230) ALT,BN,ER,DB,YIELD,DENSC
    FORMAT (5X,'17) NOZZLE DESIGN ALTITUDE',T45,F12.1,' FEET',
+ /5X,'18) NOZZLE EROSION RATE',T45,F12.5,' IN/SEC',
+ /5X,'19) MISSILE DIAMETER',T45,F12.1,' INCHES',
+ /5X,'20) MISSILE STRENGTH OF CASE MATERIAL',T45,F12.1,' PSI',
+ /5X,'21) YIELD STRENGTH OF CASE MATERIAL',T45,F12.4,' LBS/CU.IN',
    GO TO 249
```

```

240 WRITE (8,245) ALT,BN,DB,YIELD,DENSC,ALTN,D,YIELDS,DENSC S
```

```

245 FORMAT (5X,'17) BOOSTER DESIGN ALTITUDE','T45,F12.1,' FEET',  

+ /5X,'18) BOOSTER DIAMETER','T45,F12.2,' INCHES',  

+ /5X,'19) STRONGTH OF BOOSTER CASE','T45,F12.1,' PSI',  

+ /5X,'20) YIELD STRENGTH OF BOOSTER MATERIAL','T45,F12.4,' LBS/CU.IN',  

+ /5X,'21) DENSITY OF BOOSTER MATERIAL','T45,F12.5,' FEET',  

+ /5X,'22) SUSTAINER DESIGN ALTITUDE','T45,F12.1,' PSI',  

+ /5X,'23) SUSTAINER DIAMETER','T45,F12.2,' INCHES',  

+ /5X,'24) SUSTAINER LENGTH OF SUSTAINER MATERIAL','T45,F12.4,' LBS/CU.IN'  

+ ,/  

249 CONTINUE  

WRITE (8,1000)  

WRITE (8,1010)  

WRITE (8,1020)  

WRITE (8,1030)  

WRITE (8,1040)  

IF (IFBSC.EQ.0) GO TO 250  

IF (IFPCCS.EQ.0) WRITE (8,1206)  

IF (IFPCCS.EQ.1) WRITE (8,1210)  

IF (IFFBRS.EQ.1) WRITE (8,1220)  

IF (IFDLMB.EQ.1) WRITE (8,1230)  

IF (IFPCBS.EQ.1) WRITE (8,1233)  

IF (IFDIMS.EQ.1) WRITE (8,1235)  

IF (IFAB2.EQ.1) WRITE (8,1245)  

IF (IFBRS.EQ.1) WRITE (8,1250)  

IF (IFAB2.EQ.1) WRITE (8,1260)  

IF (IFTRML.EQ.1) WRITE (8,1270)  

CONTINUE  

RETURN  

END  

1500

```

## APPENDIX G. AERODYNAMIC COEFFICIENTS PROGRAM LISTING

This program is divided into three major subdivisions; the executive routines, the FORTRAN II/IV computational program, and the FORTRAN IV plotting program. The executive routines are used to establish the required file definitions, initiate operation of the computational program, supervise the transfer of data to the plotting program, and provide operational information to the user at appropriate times.

The computational program, LAERO1 FORTRAN, consists of five subprogram divisions. The MAIN program accepts the input data, conducts calculations not done by other subroutines, formats the calculated data and provides the output data to the user, the printer file, and the plot program data file. Subroutine GEOSUB calculates the missile wetted area and the Reynolds number per foot based on the flight altitude. Subroutine CLASJB calculates the aerodynamic surface lift-curve slopes. Subroutine CATSUB calculates center of pressure locations, cross-flow drag coefficients, and interference factors. Subroutine SCREEN prompts the user to clear the terminal screen for proper positioning of the output.

The plot program, AEROPLOT FORTRAN, is structured for direct submission to the MVS batch reader from the 3278 terminal. No cards need to be punched or read. However, attention must be given to the correct JCL accounting data in the first line of the program; those shown in the listing are for illustrative purposes only. This program receives the data from the computational program and produces a group of six charts for each Mach number entered. The plots represent the relationships of  $C_l$  to  $\alpha$ ,  $C_m$ ,  $C_n$ ,  $C_d$ ,  $C_a$ , and  $C_{di}$ . The program can produce up to 24 sets of plots for a single run.

FILE: LAERO1 EXEC A NAVAL POSTGRADUATE SCHOOL  
 FILEDEF 08 DISK LAERO1 OUTPUT AO (RECFM VA BLOCK 133 PERM  
 FILEDEF 07 DISK LAERO1 PLOT AO (RECFM VA BLOCK 80 PERM  
 &BEGTYPE  
 YOU WILL HAVE THE OPPORTUNITY TO OBTAIN BOTH A HARDCOPY  
 PRINTOUT AND A SET OF PLOTS FOR ONE SET OF INPUT PARAMETERS  
 EACH TIME YOU ENTER THIS PROGRAM. THE PROGRAM MAY BE  
 RE-RUN CONTINUOUSLY AND YOU WILL HAVE THE OPTION TO CHANGE  
 INPUT PARAMETERS FOR EACH SUCCESSIVE RUN, BUT YOU CAN  
 OBTAIN THE PRINTOUT AND PLOTS PERTAINING TO THE LAST RUN  
 ONLY. IF ADDITIONAL OUTPUT IS REQUIRED, RE-ENTER THE  
 PROGRAM.  
 &END  
 LOAD LAERO1  
 START  
 &BEGTYPE

TO OBTAIN THE HARDCOPY PRINTOUT OF THE DATA TABLES, TYPE  
 AND ENTER:

LAERO1PR

TO OBTAIN THE VERSATEC PLOT OF THE TABULAR DATA, TYPE AND  
 ENTER:

LAERO1PL

&END

FILE: LAERO1PR EXEC A NAVAL POSTGRADUATE SCHOOL  
 PRINT LAERO1 OUTPUT (LINECOUN 70  
 &BEGTYPE  
 THE OUTPUT WILL BE PRINTED ON THE VM PRINTER IN ROOM 140  
 AND WILL BE IDENTIFIED WITH YOUR USER NUMBER AND LAST NAME.  
 IT USUALLY REQUIRES SEVERAL MINUTES TO OBTAIN THE PRINTOUT.  
 &END

FILE: LAERO1PL EXEC A NAVAL POSTGRADUATE SCHOOL  
 COPY LAERO1 PLOT A LAERO PLOTDATA A PLOT LAERO1 A  
 EXEC SUBMIT PLOT LAERO1 A  
 ERASE PLOT LAERO1 A  
 &BEGTYPE  
 THE PLOT WILL BE DRAWN IN THE COMPUTER ROOM AND PLACED OVER  
 THE ALPHABETIZED OUTPUT FILE IN ROOM 140. IT WILL BE  
 IDENTIFIED BY "AEROFILE" AND USUALLY REQUIRES MANY MINUTES  
 (HOURS, DAYS) TO OBTAIN.  
 &END





LAE01000  
 LAE01010  
 LAE01020  
 LAE01030  
 LAE01040  
 LAE01050  
 LAE01060  
 LAE01070  
 LAE01080  
 LAE01090  
 LAE01100  
 LAE01110  
 LAE01120  
 LAE01130  
 LAE01140  
 LAE01150  
 LAE01160  
 LAE01170  
 LAE01180  
 LAE01190  
 LAE01200  
 LAE01210  
 LAE01220  
 LAE01230  
 LAE01240  
 LAE01250  
 LAE01260  
 LAE01270  
 LAE01280  
 LAE01290  
 LAE01300  
 LAE01310  
 LAE01320  
 LAE01330  
 LAE01340  
 LAE01350  
 LAE01360  
 LAE01370  
 LAE01380  
 LAE01390  
 LAE01400  
 LAE01410  
 LAE01420  
 LAE01430  
 LAE01440  
 LAE01450  
 LAE01460  
 LAE01470

```

DO 10000 I=1, IDT
  WRITE (6, 10450)
  FORMAT(1X, '***INPUT CONTROL DEFLECTION (DECIMAL NUMBER)*')
10450 READ 1070, XDT(I)
10000 IF(IABC.EQ.1)GO TO 1100
60004 WRITE (6, 10040)
10040 FORMAT(1X, 'INPUT NUMBER OF MACH NUMBERS (LESS THAN 25)*')
  DO 20000 I=1, IM
    WRITE (6, 10460)
    FORMAT(1X, '***INPUT MACH NUMBER (DECIMAL NUMBER)*')
20000 READ 1070, VXXM(I)
60005 IF(IABC.EQ.1)GO TO 1100
10050 WRITE (6, 10050)
  FORMAT(1X, 'INPUT NUMBER OF ANGLES OF ATTACK (LESS THAN 25)*')
  READ 1060, IAL
  ICL=IAL
DO 30000 I=1, IAL
  WRITE (6, 10470)
  FORMAT(1X, '***INPUT ANGLE OF ATTACK (DECIMAL NUMBER)*')
30000 READ 1070, XAL(I)
60006 IF(IABC.EQ.1)GO TO 1100
10060 WRITE (6, 10060)
  FORMAT(1X, 'INPUT NUMBER OF CONFIGURATIONS*')
  READ 1060, NBODY
  IF(IABC.EQ.1)GO TO 1100
60007 WRITE (6, 10070)
10070 FORMAT(1X, 'INPUT, 01=NON-DELTA WING, 02=DELTA WING*')
  READ 1060, ISWPW
  IF(IABC.EQ.1)GO TO 1100
60008 WRITE (6, 10080)
10080 FORMAT(1X, '00=NO BODY AFTER WING, 01=BODY AFTER WING*')
  READ 1060, IAFBW
  IF(IABC.EQ.1)GO TO 1100
60009 WRITE (6, 10090)
10090 FORMAT(1X, 'INPUT WING SWEEP CONSTANT*')
  WRITE (6, 55001)
55001 *1X, '00=UNSWEEP LEADING EDGE, 01=SWEPT LEADING EDGE*')
  READ 1060, ISWEPW
  IF(IABC.EQ.1)GO TO 1100
60010 WRITE (6, 10100)
10100 FORMAT(1X, 'INPUT NUMBER OF WINGS*')
  READ 1060, NWING
  IF(IABC.EQ.1)GO TO 1100
60011 WRITE (6, 10110)
10110 FORMAT(1X, 'INPUT, 01=NON-DELTA TAIL, 02=DELTA TAIL*')
  READ 1060, ISWPT

```



```

60012 IF(IABC.EQ.1)GO TO 1100
10120 WRITE (6,10120)
      FORMAT(1X,'06=NO BODY AFTER TAIL, 01=BODY AFTER TAIL')
      READ 1060,1AFBT
      IF(IABC.EQ.1)GO TO 1100
60013 WRITE (6,10130)
10130 FORMAT(1X,'INPUT TAIL SWEEP CONSTANT')
      WRITE (6,55001)
      READ 1060,1SWPT
      IF(IABC.EQ.1)GO TO 1100
60014 WRITE (6,10140)
10140 FORMAT(1X,'INPUT NUMBER OF TAILS')
      READ 1060,1NTAIL
      IF(IABC.EQ.1)GO TO 1100
90002 WRITE (6,99998)
99998 *1X,'INPUT THE FOLLOWING DATA AS DECIMAL NUMBERS './
60015 WRITE (6,10150)
10150 FORMAT(1X,'INPUT TIP-TO-CHORD RATIO OF WING')
      READ 1070,1XLAMW
      IF(IABC.EQ.1)GO TO 1100
60016 WRITE (6,10160)
10160 FORMAT(1X,'INPUT LEADING EDGE SWEEP OF WING,(DEGS)')
      READ 1070,1CLAMW
      IF(IABC.EQ.1)GO TO 1100
60017 WRITE (6,10170)
10170 FORMAT(1X,'INPUT WING SPAN, INCLUDE BODY')
      READ 1070,1BW
      IF(IABC.EQ.1)GO TO 1100
60018 WRITE (6,10180)
10180 FORMAT(1X,'INPUT WING ROOT CHORD (AT BODY JUNCTION)')
      READ 1070,1CROOTW
      IF(IABC.EQ.1)GO TO 1100
60019 WRITE (6,10190)
10190 FORMAT(1X,'INPUT EXPOSED WING AREA (2 PANELS)')
      READ 1070,1SW
      IF(IABC.EQ.1)GO TO 1100
60020 WRITE (6,10200)
10200 FORMAT(1X,'INPUT WING MEAN GEOMETRIC CHORD')
      READ 1070,1XMACW
      IF(IABC.EQ.1)GO TO 1100
60021 WRITE (6,10210)
10210 FORMAT(1X,'INPUT DISTANCE FROM NOSE TO WING LEADING EDGE')
      READ 1070,1XWING
      IF(IABC.EQ.1)GO TO 1100
60022 WRITE (6,10220)
10220 FORMAT(1X,'INPUT WING THICKNESS-TC-CHORD RATIO')
      READ 1070,1TOVCH

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LAE01480
LAE01490
LAE01500
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LAE01930
LAE01940
LAE01950

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60023 IF(IABC.EQ.1100 TO 1100
10230 WRITE(6,10230)
      FORMAT(IX,INPUT TIP-TO-ROOT CHORD RATIO OF TAIL*)
      READ 1070,XLAMT
      IF(IABC.EQ.1100 TO 1100
60024 WRITE(6,10240)
10240 FORMAT(IX,INPUT TAIL LEADING EDGE SWEEP (DEGS)*)
      READ 1070,CLAMT
      IF(IABC.EQ.1100 TO 1100
60025 WRITE(6,10250)
10250 FORMAT(IX,INPUT TAIL SPAN, INCLUDING BODY*)
      READ 1070,BT
      IF(IABC.EQ.1100 TO 1100
60026 WRITE(6,10260)
10260 FORMAT(IX,INPUT TAIL ROOT CHORD*)
      READ 1070,CROOT
      IF(IABC.EQ.1100 TO 1100
60027 WRITE(6,10270)
10270 FORMAT(IX,INPUT EXPOSED TAIL AREA (2 PANELS)*)
      READ 1070,ST
      IF(IABC.EQ.1100 TO 1100
60028 WRITE(6,10280)
10280 FORMAT(IX,INPUT TAIL MEAN GEOMETRIC CHORD*)
      READ 1070,XMCT
      IF(IABC.EQ.1100 TO 1100
60029 WRITE(6,10290)
10290 FORMAT(IX,INPUT DISTANCE FROM NOSE TO TAIL LEADING EDGE*)
      READ 1070,XTAIL
      IF(IABC.EQ.1100 TO 1100
60030 WRITE(6,10300)
10300 FORMAT(IX,INPUT TAIL THICKNESS-TC-CHORD RATIO*)
      READ 1070,TDVCT
      IF(IABC.EQ.1100 TO 1100
60031 WRITE(6,10310)
10310 FORMAT(IX,INPUT ALTITUDE*)
      READ 1070,HT
      IF(IABC.EQ.1100 TO 1100
60032 WRITE(6,10320)
10320 FORMAT(IX,INPUT BODY DIAMETER*)
      READ 1070,D
      IF(IABC.EQ.1100 TO 1100
60033 WRITE(6,10330)
10330 FORMAT(IX,INPUT MISSILE LENGTH*)
      READ 1070,XL
      IF(IABC.EQ.1100 TO 1100
60034 WRITE(6,10340)
10340 FORMAT(IX,INPUT NOSE LENGTH*)
      READ 1070,XLNOSE

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LAE01970
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LAE01990
LAE02000
LAE02010
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60035 IF(IABC.EQ.1)GO TO 1100
10350 WRITE(6,10350)
      FORMAT(IX,'INPUT CG LOCATION (FROM NDSE)')
      READ 1070,XCG
60036 IF(IABC.EQ.1)GO TO 1100
10360 WRITE(6,10360)
      FORMAT(IX,'INPUT REFERENCE AREA')
      READ 1070,AREA
60037 IF(IABC.EQ.1)GO TO 1100
10370 WRITE(6,10370)
      FORMAT(IX,'INPUT REFERENCE LENGTH')
      READ 1070,XREF
60038 IF(IABC.EQ.1)GO TO 1100
10380 WRITE(6,10380)
      FORMAT(IX,'ENGINE CODE, 0.0=TURBOFAN, 1.0=ROCKET')
      READ 1070,ENGINE
60039 IF(IABC.EQ.1)GO TO 1100
10390 WRITE(6,10390)
      FORMAT(IX,'INLET CODE, 0.0=FLUSH, 1.0=EXTENDED')
      READ 1070,ENLET
60040 IF(IABC.EQ.1)GO TO 1100
10400 WRITE(6,10400)
      FORMAT(IX,'INPUT BOATTAIL ANGLE (DEGS)')
      READ 1070,BETA
60041 IF(IABC.EQ.1)GO TO 1100
10410 WRITE(6,10410)
      FORMAT(IX,'INPUT BASE DIAMETER')
      READ 1070,DBASE
60042 IF(IABC.EQ.1)GO TO 1100
10420 WRITE(6,10420)
      FORMAT(IX,'INPUT NOZZLE EXIT DIAMETER')
      READ 1070,DJET
60043 IF(IABC.EQ.1)GO TO 1100
10430 WRITE(6,10430)
      FORMAT(IX,'INPUT BOATTAIL LENGTH')
      READ 1070,XLABOD
60044 IF(IABC.EQ.1)GO TO 1100
10440 WRITE(6,10440)
      FORMAT(IX,'INPUT PROTUBERANCE DRAG')
      READ 1070,CDPROT
      IF(IABC.EQ.1)GO TO 1100
C 1100 REWIND 08
      REWIND 07
      CALL SCREEN
1110 WRITE(6,1110)
      *TITL9,TITL0,TITL01,TITL02,TITL03,TITL04,TITL5,TITL6,TITL7,TITL8,

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1120 WRITE (6,1120) SURE TO NOTE NUMBER OF ANY INCORRECT ENTRIES,/)
      FORMAT (6,1150) ICSC, INOSE, IDT, IM, IAL, NBODY, ISWPW, IAFBW, ISWEPW,
      *NWRITE, ISWPT, IAFBT, ISWEPT, NTAIL, XLAMW, CLAMW, BW, CROOTW, SW, XMACW,
      *XWRITE, TOVCW, XLAMT, CLAMT, BT, CROOTT, ST
      *XWRITE (6,1170) XMACW, XAL, TOVCT, HT, D, XL, XLNOSE, XCG, AREA, XREF,
      *ENGINE (ENLET, BETA, DBASE, DJET, XLABOD, CDPROT
      WRITE (6,1180) (XVXM(I), I=1,24)
      WRITE (6,1190) (XDT(I), I=1,24)
      WRITE (6,1200) (XAL(I), I=1,24)
1130 FORMAT (1X,15A4//)
1140 FORMAT (1X,1) (ICSC) CONTROL CONSTANT; 1=TAIL, 2=WING, 3=CANARD:
1150 FORMAT (1X,1) (INOSE) NOSE SHAPE; 1=ELLIPSE, 2=OGIVE, 3=CONE; ,T63,I2/,
      *IX,,2) (IDT) NUMBER OF CONTROL DEFLECTIONS: ,T63,I2/,
      *IX,,3) (IM) NUMBER OF MACH NUMBERS: ,T63,I2/,
      *IX,,4) (IAL) NUMBER OF ANGLES OF ATTACK: ,T63,I2/,
      *IX,,5) (NBODY) NUMBER OF CONFIGURATIONS: ,T63,I2/,
      *IX,,6) (ISWPW) 1=NON-DELTA WING, 2=DELTA WING: ,T63,I2/,
      *IX,,7) (IAFBW) 0=NO BODY AFTER WING, 1=BODY AFTER WING: ,T63,I2/,
      *IX,,8) (ISWEPW) WING SWEEP CONSTANT (IF DELTA=0), ,T63,I2/,
      *IX,,9) UNSWEPT LEADING EDGE, 1=SWEEP LEADING EDGE: ,T63,I2/,
      *IX,,10) (NHWING) NUMBER OF WINGS: ,T63,I2/, TAIL: ,T63,I2/,
      *IX,,11) (ISWPT) 1=NON-DELTA TAIL, 2=DELTA TAIL: ,T63,I2/,
      *IX,,12) (IAFBT) 0=NO BODY AFTER TAIL, 1=BODY AFTER TAIL: ,T63,I2/,
1160 FORMAT (1X,13) (ISWPT) TAIL SWEEP CONSTANT (IF DELTA=0), ,T63,I2/,
      *IX,,14) (ISWPT) TAIL SWEEP LEADING EDGE: ,T63,I2/,
      *IX,,15) (NTAIL) NUMBER OF TAILS: ,T63,I2/,
      *IX,,16) (XLAMW) TIP-TO-CHORD RATIO OF WING: ,T56,F12.3/,
      *IX,,17) (CLAMW) WING SPAN, INCLUDING BODY: ,T56,F12.3/,
      *IX,,18) (CROOTW) WING ROOT CHORD (AT BODY JUNCTION): ,T56,F12.3/,
      *IX,,19) (SW) EXPOSED WING AREA (TWO PANELS): ,T56,F12.3/,
      *IX,,20) (XMACW) WING MEAN GEOMETRIC TO WING LE: ,T56,F12.3/,
      *IX,,21) (XWING) DISTANCE FROM NOSE TO CHORD RATIO OF TAIL: ,T56,F12.3/,
      *IX,,22) (TOVCW) WING THICKNESS TO CHORD RATIO OF TAIL: ,T56,F12.3/,
      *IX,,23) (XLAMT) TIP-TO-CHORD RATIO OF TAIL: ,T56,F12.3/,
      *IX,,24) (CLAMT) TAIL LEADING EDGE SWEEP (DEGREES): ,T56,F12.3/,
      *IX,,25) (BT) TAIL SPAN, INCLUDING BODY: ,T56,F12.3/,
      *IX,,26) (CROOTT) TAIL ROOT CHORD: ,T56,F12.3/,
      *IX,,27) (ST) EXPOSED TAIL AREA (TWO PANELS): ,T56,F12.3/,
1170 FORMAT (1X,28) (XMACW) TAIL MEAN GEOMETRIC CHORD: ,T56,F12.3/,
      *IX,,29) (XTAIL) DISTANCE FROM NOSE TO TAIL LE: ,T56,F12.3/,
      *IX,,30) (TOVCT) TAIL THICKNESS TO CHORD RATIO: ,T56,F12.3/,
      *IX,,31) (HT) ALTI TUDE: ,T56,F12.3/,
      *IX,,32) (D) BODY DIAMETER: ,T56,F12.3/,

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*IX,.33) (XL) MISSILE LENGTH:,,T56,F12.3/,
*IX,.34) (XLNOSE) NOSE LENGTH:,,T56,F12.3/,
*IX,.35) (XCG) DISTANCE TO CG LOCATION FROM NOSE:,,T56,F12.3/,
*IX,.36) (XAREA) REFERENCE AREA:,,T56,F12.3/,
*IX,.37) (XREF) REFERENCE LENGTH:,,T56,F12.3/,
*IX,.38) (ENGINE) ENGINE:,,T56,F12.3/,
*IX,.39) (ENLET) INLET:,,T56,F12.3/,
*IX,.40) (BETA) BOAT-TAIL ANGLE:,,T56,F12.3/,
*IX,.41) (DBASE) BASE DIAMETER:,,T56,F12.3/,
*IX,.42) (DJET) NOZZLE EXIT DIAMETER:,,T56,F12.3/,
*IX,.43) (XLABOD) BOAT-TAIL LENGTH:,,T56,F12.3/,
*IX,.44) (CDPRUT) PROUTER DRAG:,,T56,F12.3//)
1180 FORMAT(IX,MACH,,12F6.3/,6X,12F6.3/)
1190 FORMAT(IX,DELTA,,12F6.2/,6X,12F6.2/)
1200 FORMAT(IX,ALPHA,,12F6.2/,6X,12F6.2/)
C
IABC=1
WRITE(6,1210)
FORMAT(IX,IS INPUT DATA CORRECT? O3=YES, IF NO,/)
1210 *IX,ENTER THE TWO-DIGIT NUMBER OF THE VARIABLE TO BE CHANGED.
READ 1060, IVAR
IF(IVAR.EQ.0) GO TO 1220
GO TO 160001,60002,60003,60004,60005,60006,60007,60008,60009,
*60010,60011,60012,60013,60014,60015,60016,60017,60018,60019,
*60020,60021,60022,60023,60024,60025,60026,60027,60028,60029,
*60030,60031,60032,60033,60034,60035,60036,60037,60038,60039,
*60040,60041,60042,60043,60044,IVAR
1220 CONTINUE
WRITE(8,1130)
WRITE(8,1140) TITL1,TITL2,TITL3,TITL4,TITL5,TITL6,TITL7,TITL8,TITL
*9,TITL9,TITL10,TITL11,TITL12,TITL13,TITL14,TITL15,TITL16,TITL17,TITL18,TITL19,TITL20,TITL21,TITL22,TITL23,TITL24,TITL25,TITL26,TITL27,TITL28,TITL29,TITL30,TITL31,TITL32,TITL33,TITL34,TITL35,TITL36,TITL37,TITL38,TITL39,TITL40,TITL41,TITL42,TITL43,TITL44,TITL45,TITL46,TITL47,TITL48,TITL49,TITL50,TITL51,TITL52,TITL53,TITL54,TITL55,TITL56,TITL57,TITL58,TITL59,TITL60,TITL61,TITL62,TITL63,TITL64,TITL65,TITL66,TITL67,TITL68,TITL69,TITL70,TITL71,TITL72,TITL73,TITL74,TITL75,TITL76,TITL77,TITL78,TITL79,TITL80,TITL81,TITL82,TITL83,TITL84,TITL85,TITL86,TITL87,TITL88,TITL89,TITL90,TITL91,TITL92,TITL93,TITL94,TITL95,TITL96,TITL97,TITL98,TITL99,TITL100,TITL101,TITL102,TITL103,TITL104,TITL105
*WRITE(8,1150) ICSC,INNOSE,IDI,IM,IAC,NBODY,ISWPW,IAFBW,ISWEPW,
*NRWING,ISWPT,IAFBT
*WRITE(8,1160) ISWEPT,NIAIL,XLAMW,CLAMW,BW,CROOTW,SW,XMACW,
*XRWING,TOVCW,XLAMT,CLAMT,BT,CROOTT,ST
*WRITE(8,1170) XMACI,XTAIL,TOVCT,HF,D,XL,XLNOSE,XCG,AREA,XREF,
*ENGINE,ENLET,BETA,DBASE,DJET,XLABOD,CDPRUT
*WRITE(8,1180) (XVXM(I), I=1,24)
*WRITE(8,1190) (XDT(I), I=1,24)
*WRITE(8,1200) (XAL(I), I=1,24)
1230 PIE=3.14159
IL=1+IL
LLKK=0
LLLL=0
XCG2 = XCG
IZZY = 0
IF(INNOSE.EQ.3) GO TO 1250
IF(INNOSE.EQ.2) GO TO 1240

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XC=XL/2.
AP=XL*D
GO TO 1260
1240 XLNOD=XLNOSE/D
RADIUS=XLNOD**2+.25
APD2=XLNOD*SQR1(RADIUS**2-XLNOD**2)+RADIUS**2
**ARSI(XLNOD/RADIUS)-2.*XLNOD*(RADIUS-.5)
APN=APD2*D*D
AP=(XL-XLNOD)*D+APN
XCOD1=RADIUS**3-(RADIUS**2)*1.5
XCOD=XLNOD-(.6667*XCOD1-XLNOD**2*(RADIUS-.5))/APD2
XCMOVE=XCOD*D-XLNODSE/2.
XC=XL/2.+XCMOVE
GO TO 1260
1250 APN=.5*D*XLNOSE
AP=APN+(XL-XLNODSE)*D
XCN=.6667*XLNOSE
XCMOVE=XCN-XLNODSE/2.
XC=XL/2.+XCMOVE
1260 CONTINUE
1270 CALL GEOSUB
CALL SCREEN
VXM=XVXM(1)
RE=REFI*VXM
RE=REFI
SQ=2
DO 3590 IJ=1,IM
REFI=REFI/VXM
DELTA=XDI(1)
DO 3580 II=1,IDT
ALPHA=XAL(1)
WRITE (6,1280) VXM
C
1280 FORMAT(//,1X,'MACH',F7.4)
WRITE (6,1290) DELTA
1290 FORMAT(1X,DELTA=,F6.2)
1300 WRITE (6,1300)
FORMAT(1X,AL,3X,CLTOT,2X,CDICT,3X,CLWP,3X,CLBW,3X,CLTP,
*,3X,CLBT,4X,CDI,3X,CNWP,3X,CNTP,3X,CLB,4X,CA,3X,XCPW,3X,XCPT,3X,
WRITE (6,1310)
1310 FORMAT(7X,CLTD,3X,CDTD,5X,CN,5X,CA,3X,XCPW,3X,XCPT,3X,
*,XCPB,4X,XCP,5X,CM)
WRITE (8,1280) VXM
WRITE (8,1290) DELTA
WRITE (8,1320)
1320 FORMAT(1X,AL,2X,CLTOT,1X,CDICT,2X,CLWP,2X,CLBW,2X,CLTP,
*,2X,CLBT,3X,CDI,2X,CNWP,2X,CNTP,2X,CLTD,2X,

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 LAE04350

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**COTD',4X,'CN',4X,'CA',2X,'XCPW',2X,'XCPT',2X,'XCPB',3X,'XCP',4X,
**CM',/)
C 1330 DELTA=DELTA/57.29578+.000000001
DO 3540 J=1,IAL
AL=ALPHA/57.29578+.000000001
SINAAL=SIN(AL)
COSAAAL=COS(AL)
VXMR1=VXM
IF (IZZY=1) IZZY+1
IF (IZZY-4) 1340,1340,1350
1340 VXM=.6
1350 CALL CLASUB
IF (LLL-1) 1360,1640,1710
1360 IF (IZZY-4) 1380,1380,1370
1370 CALL CATSUB
1380 XLAM14=ATAN((.5*(B1-D)))/COLAM+.25*XLAM1*CRROOT-.25*CRROOT)/
*(.5*(B1-D))
RF=REFI*VXM*XMAL
IF (RE-1.E06) 1390,1400,1400
1390 AA=.0835
XNN=-.211
GO TO 1450
1400 IF (RE-1.E07) 1410,1420,1420
1410 AA=.052
XNN=-.177
GO TO 1450
1420 IF (RE-1.E08) 1430,1440,1440
1430 AA=.0333
XNN=-.1488
GO TO 1450
1440 AA=.0221
XNN=-.127
CF=AA*RE**XNN
SURF=FLD*AT(NSURF)
CDO=SURF*CF*(1.+2.*TOVC+100.*TOVC**4.)
IF (IZZY-4) 1460,1460,1470
IF (IZZY-3) 1580,1630,1670
IF (IAL) 1480,1490,1490
1460 ODC=-ODC
1470 LLKK=LLKK+1
1480 IF (LLKK-2) 1500,1520,1540
1490 IF (SW) 1510,1510,1540
1500 LLKK=LLKK+1
1510 IF (SW2) 1530,1530,1540
1520 LLKK=LLKK+1
1530 IF (LLKK-2) 1550,1600,1660
1540 XKWB=XKWB
LAE04360
LAE04370
LAE04380
LAE04390
LAE04400
LAE04410
LAE04420
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LAE04680
LAE04690
LAE04700
LAE04710
LAE04720
LAE04730
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 LAE05080  
 LAE05090  
 LAE05100  
 LAE05110  
 LAE05120  
 LAE05130  
 LAE05140  
 LAE05150  
 LAE05160  
 LAE05170  
 LAE05180  
 LAE05190  
 LAE05200  
 LAE05210  
 LAE05220  
 LAE05230  
 LAE05240  
 LAE05250  
 LAE05260  
 LAE05270  
 LAE05280  
 LAE05290  
 LAE05300  
 LAE05310

XKBMW=XKBW  
 IF(ISWEPW, EQ, 0) GO TO 1560  
 SHIFT=TAN(CLAMW)\*(BW-D)/4.0  
 GO TO 1570  
 1560 SHIFT=0.0  
 XCPBW=XWING+XBCRBW\*CROOT+SHIFT  
 1570 XCPBW=XWING+XBCRBW\*CROOT  
 ODCW=ODC  
 CLW=SIN(AL)\*(XKBW+XKBW)\*CLALW\*SW\*COS(AL)/AREA  
 CLWB=SIN(AL)\*XKBW\*CLALW\*SW\*COS(AL)/AREA  
 CLBW=CLW-CLWB  
 CLVISW=(SIN(AL)\*SW\*COS(AL)/AREA)\*ODCW  
 CLW=CLW+CLVISW  
 CLWP=CLWB+CLVISW  
 CDOW=CDOW\*(SW)/AREA  
 1580 XLAMW4=XLAM14  
 TOVCW=TOVC  
 SWOT=SW  
 IZZY=IZZY+1  
 IF(SW2) 1640, 1640, 1590  
 1590 COLAM=COS(CLAMW2)/SIN(CLAMW2)  
 CDOH2=0  
 BCOLAM=BETA1\*COLAM  
 CROOT=CROOT  
 B1=BW2  
 IAFB=IAFBW2  
 CLAL1=CLALW2  
 XLAM1=XLAMW2  
 TOVC=TOVCW2  
 XMAC=XMACW2  
 ISWP1=ISWPW2  
 BAR=BETA1\*ARW2  
 RATIO=CROOT/(BETA1\*D)  
 IF(IZZY-4) 1380, 1380, 1370  
 1600 XKWBW2=XKBW  
 XKBW2=XKBW  
 IF(ISWEP2, EQ, 0) GO TO 1610  
 SHIFT=TAN(CLAMW2)\*(BW2-D)/4.0  
 GO TO 1620  
 1610 SHIFT=0  
 1620 XCPBW2=XWING2+XBCRBW2\*CROOT+SHIFT  
 XCPBW2=XWING2+XBCRBW2\*CROOT  
 ODCW2=ODC  
 CLW2=SIN(AL)\*(XKBW2+XKBW2)\*CLALW2\*SW2\*COS(AL)/AREA  
 CLWB2=SIN(AL)\*XKBW2\*CLALW2\*SW2\*COS(AL)/AREA  
 CLBW2=CLW2-CLWB2  
 CLVIW2=(SIN(AL)\*SW2\*COS(AL)/AREA)\*ODCW2  
 CLW2=CLW2+CLVIW2



```

1630 CDW2=CDO*(SW2)/AREA
    XLAM24=XLAM14
    SW2TOT=SW2
1640 IZZY = IZZY +1
    LKK=LLKK+2
    IF (ST) 1710,1710,1650
1650 COLAM=COS(CLAMT)/SIN(CLAMT)
    ART=(BT-DI)*2/ST
    BCOLAM=BETA1*COLAM
    CROOT=CROOTT
    BI=BT
    BAR=BETA1*ART
    CLAL1=CLALT
    IAFB=IAFBT
    XMAC=XMACT
    TOVC=TOVCT
    ISWPI=ISWPT
    XLAM1=XLAMT
    RAT10=CROOT/(BETA1*D)
    IF (IZZY-4) 1380,1380,1370
1660 XKWB1=XKWB
    XKBWT=XKBW
    XCPBT=XTAIL+XBCRBW*CROOT
    ODC1=ODC
    CLT=((XKWB1+XKBWT)*SIN(AL))*CLALT*ST*COS(AL)/AREA
    CLTB=SIN(AL)*XKBWT*CLALT*ST*COS(AL)/AREA
    CLBT=CLT-CLTB
    CLTD=XKTB*CLALT*SIN(DELTA)*ST*COS(AL+DELTA)/AREA
    CLTDB=(XKTB+XKB1)*CLALT*SIN(DELTA)*ST*COS(AL+DELTA)/AREA
    CLBDT=CLTD-CLTDB
    CLBT=CLBT+CLBDT
    CLVIST=((SIN(AL+DELTA)*SIN(AL+DELTA))*ST*COS(AL+DELTA)/AREA)*ODCT
    CLTP=CLTB+CLVIST
    CLT=CLT+CLVIST
    CDO1=CDO*(ST)/AREA
1670 CT=COT
    STTOT=ST
    XLAM14=XLAM14
    IF (IZZY-4) 1900,1900,1680
1680 IF (ISWEPT,EQ,0) GO TO 1690
    SHIFT=TAN(CLAMT)*(BT-DI)/4.0
    GO TO 1700
1690 SHIFT=0.0
    XCPT8=XTAIL+((XKBWT*SIN(AL)*XBCRBW+XKTB*SIN(DELTA))*XBCRBW)/
1700 *(XKBWT*SIN(AL)+XKTB*SIN(DELTA))*CROOTT+SHIFT
    IF (IZZY-4) 1900,1900,1720
1710 XLOB = XL/D
1720 ZXM=VXM*ABS(SIN(AL))

```

LAE05320  
 LAE05330  
 LAE05340  
 LAE05350  
 LAE05360  
 LAE05370  
 LAE05380  
 LAE05390  
 LAE05400  
 LAE05410  
 LAE05420  
 LAE05430  
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 LAE05480  
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 LAE05500  
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 LAE05670  
 LAE05680  
 LAE05690  
 LAE05700  
 LAE05710  
 LAE05720  
 LAE05730  
 LAE05740  
 LAE05750  
 LAE05760  
 LAE05770  
 LAE05780  
 LAE05790

```

1730 IF (ZXM-.8) 1730,1740,1740
      CDC=2.4-SQRT(1.5129-1.5129*ZXM*ZXM)
      GO TO 1790
1740 IF (ZXM-1.15) 1750,1760,1760
1750 CDC=1.6+SQRT(.344-{ZXM-.975})**2)
      GO TO 1790
1760 IF (ZXM-3.1) 1770,1780,1780
1770 CDC=1.9-SQRT(.361-.094{ZXM-3.})**2)
      GO TO 1790
1780 CDC=1.3
1790 ETA=(0.0000475*(XLOB**3))-(0.00173*(XLOB**2))+(0.0298*XLOB)+0.5146
      IF (VXM-.5) 1830,1830,1800
1800 IF (VXM-1.4) 1810,1820,1820
1810 ETA=ETA+(1.-ETA)*(VXM-.5)*1.111
      GO TO 1830
1820 ETA=1.
1830 IF (XLOB-10.) 1840,1850,1860
1840 XK2K1=-0.0054*(XLOB**2)+0.104*XLOB+0.437
      GO TO 1870
1850 XK2K1=0.939
      GO TO 1870
1860 XK2K1=0.939+(0.001525*(XLOB-10.0))
1870 ALP=AL
      IF (AL) 1880,1890,1890
1880 CDC=CD
1890 CNB=(XK2K1*SIN(2.*ALP)*COS(ALP/2.))*3.14159*D*D/(4.*AREA)
      *+ETA*CDC*((AP )/AREA)*((SIN(ALP))**2)
      XQ=XCG/D
      CMB1=(XK2K1*XQ*SIN(2.*ALP)*COS(ALP/2.))*3.14159*D*D*D/
      *{(4.*AREA*XREF)
      CMB2=(ETA*CDC*((AP )/AREA)*((XCG-(XC )/DI)*((SIN(ALP))**2)))
      *D/XREF
      CMB=CMB1+CMB2
      RE=REF*VXM*XL
1900 IF (RE-1.E06) 1910,1920,1920
1910 AA=.0835
      XNN=-.211
      GO TO 1970
1920 IF (RE-1.E07) 1930,1940,1940
1930 AA=.052
      XNN=-.177
      GO TO 1970
1940 IF (RE-1.E08) 1950,1960,1960
1950 AA=.033
      XNN=-.1488
      GO TO 1970
1960 AA=.0221

```

LAE05800  
 LAE05810  
 LAE05820  
 LAE05830  
 LAE05840  
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 LAE05870  
 LAE05880  
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 LAE05900  
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 LAE06230  
 LAE06240  
 LAE06250  
 LAE06260  
 LAE06270

```

1970 XNN=-.127
      CFBD0=AA*RE**XNN
      CDOB=(1.02*CFBD0*(1.0+.0025*XLOB+60.0/(XLOB**3.0))*SSUBS/AREA)
      *CDPROT
      IF(ENGINE.EQ.1.0) GO TO 1990
      IF(ENLET.EQ.1.0) GO TO 1980
      CDINL=.038*CDOB
      GO TO 2000
1980 CDINL=0.05*CDOB
      GO TO 2000
1990 CDINL=.0
      CBASE DRAG (NO BOATTAIL)
2000 CBPRI=-(((2.8*VXM-.4)/2.4)/VXM**2.28)*.8123)-1.)*1.4286/VXM**2.
      SB=(DBASE-DJET)*(DBASE+DJET)*3.14159/4.
      CB=CBPRI*SB/AREA
      IF (CB.LT.0.0) CB=0.0
      IF (BETA.NE.0.0) CB=0.0
      CDOB=CDOB+CB CALCULATIONS (BOATTAIL)
      C AFTER BODY DRAG CALCULATIONS (BOATTAIL)
      DELCPD=0.
      DELCPD=0.
      DRATIO=(DBASE**2-DJET**2)/(D**2)
      DRATIO=(DJET**2)/(DBASE*D)
      DBDM=DBASE/D
      DELBAS=-.1532+(.0247*BETA1)-(.002632*(BETA1**2))
      CPBS01=-.11905+(.00017*DBDM)-(.0283*(DBDM**2))
      CPBS02=-.0273+(.00425*DBDM)-(.1143*(DBDM**2))
      CPBS03=-.0612+(.3485*DBDM)-(.4254*(DBDM**2))
      CPBS04=-.0789+(.5252*DBDM)-(.7434*(DBDM**2))
      CPBS05=-.085+(1.324*DBDM)-(.1407*(DBDM**2))
      IF(BETA-3.0)2010,2010,2020
2010 CPBS0=(CPBS01+.15)*BETA/3.0)-.15
      GO TO 2090
2020 IF(BETA-5.6)2030,2030,2040
2030 CPBS0=(CPBS02-CPBS02)*(BETA-3.0)/2.6)+CPBS01
      GO TO 2090
2040 IF(BETA-8.0)2050,2050,2060
2050 CPBS0=(CPBS03-CPBS03)*(BETA-5.6)/2.4)+CPBS02
      GO TO 2090
2060 IF(BETA-16.0)2070,2070,2080
2070 CPBS0=(CPBS04-CPBS03)*(BETA-8.0)/8.0)+CPBS03
      GO TO 2090
2080 CPBS0=(CPBS05-CPBS04)*(BETA-16.0)/4.0)+CPBS04
2090 CDBASE=(-DRATIO)*(CPBS0+DELCPD+(DELCPD*DRATIO))
      IF(ENGINE.EQ.1.0) GO TO 2470
2100 IF(CDOB-.76)2100,2100,2110
      CBOAT5=.1013*DBDM
      GO TO 2130

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LAE06280  
 LAE06290  
 LAE06300  
 LAE06310  
 LAE06320  
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 LAE07210  
 LAE07220  
 LAE07230

2110 IF(DBDM-LT,0.82) GO TO 2120  
 CBOAT5=-.4\*(DBDM-.82)+.077  
 GO TO 2130  
 2120 CBOAT5=.077  
 2130 IF(DBDM-.245)2140,2140,2150  
 2140 CBOAT4=.0653\*DBDM  
 GO TO 2180  
 2150 IF(DBDM-GT,0.76) GO TO 2160  
 CBOAT4=.1048\*(DBDM-.245)+.016  
 GO TO 2180  
 2160 IF(DBDM-GT,0.82) GO TO 2170  
 CBOAT4=.071  
 GO TO 2180  
 2170 CBOAT4=-.369\*(DBDM-.82)+.07  
 2180 IF(DBDM-.36)2190,2190,2200  
 2190 CBOAT3=.0292\*DBDM  
 GO TO 2230  
 2200 IF(DBDM-GT,0.76) GO TO 2210  
 CBOAT3=.10125\*(DBDM-.36)+.0105  
 GO TO 2230  
 2210 IF(DBDM-GT,0.81) GO TO 2220  
 CBOAT3=.057  
 GO TO 2230  
 2220 CBOAT3=-.2579\*(DBDM-.81)+.051  
 2230 IF(DBDM-.32)2240,2240,2250  
 2240 CBOAT2=.0125\*DBDM  
 GO TO 2290  
 2250 IF(DBDM-GT,0.5) GO TO 2260  
 CBOAT2=.0333\*(DBDM-.32)+.004  
 GO TO 2290  
 2260 IF(DBDM-GT,0.72) GO TO 2270  
 CBOAT2=.1068\*(DBDM-.5)+.01  
 GO TO 2290  
 2270 IF(DBDM-GT,0.76) GO TO 2280  
 CBOAT2=.0335  
 GO TO 2290  
 2280 CBOAT2=-.1354\*(DBDM-.76)+.0335  
 2290 IF(DBDM-.6)2300,2300,2310  
 2300 CBOAT1=.0055\*(-.03375\*DBDM)+(-.06875\*(DBDM\*\*2))  
 GO TO 2340  
 2310 IF(DBDM-GT,0.75) GO TO 2320  
 CBOAT1=.1\*(DBDM-.6)+.01  
 GO TO 2340  
 2320 IF(DBDM-GT,0.78) GO TO 2330  
 CBOAT1=.025  
 GO TO 2340  
 2330 CBOAT1=-.091\*(DBDM-.78)+.025  
 2340 IF(BETA-3.0)2350,2350,2360

```

2350 CBOAT1=(CBOAT1*BETA1)/3.0
2360 GO TO 2460
2370 IF(BETA-5.6)2370,2370,2380
2380 CBOAT1=((CBOAT2-CBOAT1)*(BETA-3.0)/2.6)+CBOAT1
2390 GO TO 2460
2400 IF(BETA-8.0)2390,2390,2400
2410 CBOAT1=((CBOAT3-CBOAT2)*(BETA-5.6)/2.4)+CBOAT2
2420 GO TO 2460
2430 IF(BETA-16.0)2410,2410,2420
2440 CBOAT1=((CBOAT4-CBOAT3)*(BETA-8.0)/8.0)+CBOAT3
2450 GO TO 2460
2460 IF(BETA-24.0)2430,2430,2440
2470 CBOAT1=((CBOAT5-CBOAT4)*(BETA-16.0)/8.0)+CBOAT4
2480 GO TO 2460
2490 PRINT 2450
2500 FORMAT(IX,'BOAT TAIL ANGLE GREATER THAN 24 DEGREES')
2510 CBOAT1=CBOAT5
2520 CBOAT=CBOAT1+DELBAS*(DELCPO+(DELCPO)*(DRATOL))
2530 CDAFT=CBOAT+CDBASE
2540 FR=XLNOSE/D
2550 *FR**5.0)+2.074*(FR**4.0)-4.183*(FR**3.0)+4.891*(FR**2.0)-3.017*
2560 *FR+.7795
2570 IF(FR.GT.1.0) COWN1=.7432093E-04*FR**5.0-.15368398E-02*FR**4.0
2580 *+.011741209*FR**3.0-0.039555503*FR**2.0+0.050635882*FR+.005431397
2590 CDPTR=((COWN1/.8)*VXM
2600 COWB1=COWB
2610 COWB=COWB+CDINL+CDAFT+CDPTR
2620 COWBT=COW+COW2+COWT+COWB
2630 COWISC=COWBT*.1
2640 COWBT=COWBT+CDMISC
2650 IF(1ZZY-4)2480,2480,2550
2660 VXM=1.1999999
2670 IF(SW)2490,2490,2500
2680 COW=0
2690 IF(SW2)2510,2510,2520
2700 COW2=0
2710 IF(ST)2530,2530,2540
2720 COWT=0
2730 HONST=COWBT
2740 GO TO 2560
2750 IF(VXM-1.2)2560,2560,3020
2760 IF(SW)2570,2570,2580
2770 DCDOOSW=0.0
2780 SWTOT=0.0
2790 COW=0.0
2800 GO TO 2740
2810 VXM=VXM*SQR(COS(XLAMW4))

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LAE07240
LAE07250
LAE07260
LAE07270
LAE07280
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LAE07580
LAE07590
LAE07600
LAE07610
LAE07620
LAE07630
LAE07640
LAE07650
LAE07660
LAE07670
LAE07680
LAE07690
LAE07700
LAE07710

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```

SQMITC=SQRT((ABS((XXM*XXM)-1.0)))/(TOVCW**0.33333)
ATC=ARW*(TOVCW**0.33333)
IZT=1
2590 IF (ATC-1.5) 2630,2600,2600
2600 IF (VXM-1.1) 2610,2610,2620
2610 *SQMITC*3.3081-1.88779*SQMITC+11.0916*SQMITC*SQMITC-18.6087*
    *SQMITC*3+7.4633*SQMITC**4
    *SQMITC=FUNCT+(ATC-2.0)*0.1
2620 GO TO 2720
    *FUNCT=3.0+(ATC-1.5)*0.3
2630 GO TO 2720
2640 IF (ATC-.5) 2690,2690,2640
2650 IF (VXM-1.1) 2650,2650,2680
2660 *FUNCT=2.47917-1.42798*SQMITC-.324405*SQMITC*SQMITC
2670 IF (SQMITC-0.4) 2660,2670,2670
    *FUNCT=FUNCT+(1.8*(ATC-1.0))/SQMITC
2680 GO TO 2720
    *FUNCT=(0.25*SQMITC)+(ATC*2.3)
2690 GO TO 2720
2700 IF (VXM-1.1) 2700,2700,2710
2710 *FUNCT=0.9-(0.7*SQMITC)
2720 GO TO 2720
2730 *FUNCT=.333*SQMITC+ATC*1.8
    *DCDOSW=FUNCT*(TOVCW**1.66667)*((COS(XLAMW4))**2.5)
2740 IF (DCDOSW.LT.0.0) DCDOSW=0.0
    *DCDOSW=DCDOSW
2750 IF (SW2) 2750,2750,2760
    *DCDOS2 = 0.0
    *SW2TOT = 0.0
    *CDOSW2 = 0.0
    *GO TO 2780
2760 IZT = 2
    *XXM=VXM*SQRT((COS(XLAM24)))
    *SQMITC=SQRT((ABS((XXM*XXM)-1.0)))/(TOVCW2**0.33333)
    *ATC=ARW2*(TOVCW2**0.33333)
    *GO TO 2590
2770 *DCDOS2=FUNCT*(TOVCW2**1.66667)*((COS(XLAM24))**2.5)
    *IF (SQMITC.GT.1.3) DCDOS2=0.0
    *IF (DCDOS2.LT.0.0) DCDOS2=0.0
    *DCDOSW2=DCDOS2
    *IF (ST) 2790,2790,2800
    *DCDOS1 = 0.0
    *STTOT=0.0
    *CDOT = 0.0
    *GO TO 2820

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LAE07720  
 LAE07730  
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 LAE08190

```

2800 IZT = 3
      XSM=VXM*SQRT(COS(XLAMT4))
      SQMITC=SQRT(ABS((XSM*XSM)-1.0))/(TOVCT**0.33333)
      ATC=ART*(TOVCT**0.33333)
      GO TO 2590
2810 DCDOST=FUNCIT*(TOVCT**1.6667)*((COS(XLAMT4))**2.5)
      IF(SQMITC*GT.1.3)DCDOST=0.0
      IF(DCDOST.LT.0.0)DCDOST=0.0
      DCDOIT=DCDOST
2820 IF(VXM-1.0)2840,2830
2830 IF(VXM-2.0)2850,2860,2860
      C TRANSONIC BODY DRAG
2840 COVC=1.0-10.08*VXM)
      GO TO 2870
2850 COVC=0.92-(0.12*(VXM-1.0))
      GO TO 2870
2860 COVC = 1.31213-0.36633*VXM+.06038*VXM**2-.00601*VXM**3+.000275*
      *VXM**4
2870 CDPPTR=1.02*CFBOD*COVC*SSUBS/AREA
      CDPPTR=CDO81-1.02*CFBOD*SSUBS/AREA
      IF(VXM-1.0)2890,2890,2880
2880 CDPPTR=(CDPPTR/0.2)*(1.2-VXM)
2890 IF(FR*GT.2.0)GO TO 2900
      CDWN2=0.00172*(FR**8)-0.00453*(FR**7)+0.050*(FR**6)-0.304*(FR**5)
      *+1.096*(FR**4)-2.406*(FR**3)+3.160*(FR**2)-2.391*(FR)+1.00
      CDWN3=.000125*(FR**8)-.00370*(FR**7)+.0447*(FR**6)-.288*(FR**5)
      *+1.076*(FR**4)-2.385*(FR**3)+3.141*(FR**2)-2.529*FR+1.300
      GO TO 2910
2900 CDWN2=-.33793095E-03*FR**5.0+.76402056E-02*FR**4.0-.67397615E-01*
      *FR**3.0+.29429971*FR**2.0-.65782772*FR+.65397474
      CDWN3=-.36714382E-03*FR**5.0+.88164977E-02*FR**4.0-.83661489E-01*
      *FR**3.0+.39748005*FR**2.0-.96866696*FR+1.0327385
      IF(VXM-.8)3000,2920,2930
2910 IF(VXM-.8)3000,2920,2930
2920 CDPTR=CDWN1
      GO TO 3000
2930 IF(VXM-1.0)2950,2940,2960
2940 CDPTR=CDWN2
      GO TO 3000
2950 CDPTR=((CDWN2-CDWN1)/0.2)*(VXM-0.8)+CDWN1
      GO TO 3000
2960 IF(VXM-1.2)2980,2970,2990
2970 CDPTR=CDWN3
      GO TO 3000
2980 CDPTR=((CDWN3-CDWN2)/0.2)*(VXM-1.0)+CDWN2
      GO TO 3000
2990 CDPTR=0.0
3000 CDOB=CB+CDFPTR+CDPPTR+CDINL+CDAFT+CDPTR
      C THE FOLLOWING INDENTED PROCEDURE WAS INSERTED TO FORCE THE CDOB

```

```

LAE08200
LAE08210
LAE08220
LAE08230
LAE08240
LAE08250
LAE08260
LAE08270
LAE08280
LAE08290
LAE08300
LAE08310
LAE08320
LAE08330
LAE08340
LAE08350
LAE08360
LAE08370
LAE08380
LAE08390
LAE08400
LAE08410
LAE08420
LAE08430
LAE08440
LAE08450
LAE08460
LAE08470
LAE08480
LAE08490
LAE08500
LAE08510
LAE08520
LAE08530
LAE08540
LAE08550
LAE08560
LAE08570
LAE08580
LAE08590
LAE08600
LAE08610
LAE08620
LAE08630
LAE08640
LAE08650
LAE08660
LAE08670

```

```

C CURVE TO SMOOTHLY DECAY. THE ORIGINAL PROGRAM DOES NOT CAUSE
C THE DRAG CURVE TO DECAY PROPERLY.
IF (VXM.LE.1.0) F=0.0
IF (VXM.GT.1.0) F=48.3841618-106.7812601*VXM+24.23729924*VXM**2
*VXM**2.+67.95235861*VXM**3.-1.179384979*VXM**4.-55.05489748*VXM**5
*+22.4414432*VXM**6.
CD08=CD08+F
CDALZ=CD08
CDOT=1.1*(DCDOT*(STTOT/AREA)+CDOT)
IF (VXM.GT.1.1) CDOT=CDOT*2.*EXP(VXM-1.1)
CDOW=1.1*(DCDOSW*(SWTOT/AREA)+CDOW)
CDOW2=1.1*(CDOW2+DCOW2*(SWTOT/AREA))
CDOWBT=CDOW+CDOT+CDOW+CDOW2+CDOWISC
IF (VXM.GT.1.1) CDOWBT=CDOWBT*1.1*EXP(1.1-VXM)
TONST=CDOWBT
HONST=HONST+ZF*(TONST-HONST)
IF (IZZY-4) 3010,3010,3030
3010 VXM=VXMRI
IZZY=IZZY+1
GO TO 1
3020 CDOWBT=((HONST-TONST)/(SQRT(3.))-SQRT(1.2)))*SQRT(VXM)+TONST
*+(HONST-TONST)/(1.-SQRT(3.))/SQRT(1.2))
IF (VXM.GT.1.2) CDOWBT=CDOWBT*.5*EXP(.5*(1.2-VXM))+CDOWBT
*/2.
CDOT=1.1*(DCDOT*(STTOT/AREA)+CDOT)
IF ((SQM/TC.GT.1.3).OR.(VXM.GT.1.0)) CDOT=CDOT*.4*EXP(2.0-
*(1.0-VXM))+CDOT*1.5
CDOW=1.1*(DCOW*(SWTOT/AREA)+CDOW)
CDOW2=1.1*(CDOW2+DCOW2*(SWTOT/AREA))
CDOWBT=CDOWBT-CDOT-CDOW-CDOW2-CB
CDALZ=CDOWBT
CD8=XK2K1*SIN(2.*AL)*SIN(AL/2.)*3.14159*D*(4.*AREA)+ETA*
*CDC*AP*((SIN(AL))*3)/AREA
CLB=XK2K1*(SIN(2.*AL))*COS(AL/2.)*COS(AL)*3.14159*D*D/(4.*AREA)+ETA
*ACDC*AP*((SIN(AL))*2)*COS(AL)/AREA-CDALZ*COS(AL)*SIN(A
*L)
CA5=CDOWBT
IF (AL) 3050,3040,3050
3040 XCPB=0.0
GO TO 3060
3050 XCPB=((XCG/XREF)-(CMB/CNB))*XREF
3060 IF (SW) 3080,3080,3070
3070 IF (ST) 3210,3210,3090
3080 IF (ST) 3340,3340,3220
3090 R=D/2.
IF (ICSC -1) 3110,3110,3100
3100 XB1=BM/2.
XB2=BT/2.

```



```

TT=D/8T
HW1=-0.5*CROOTT*ABS(SIN(DELTA))+(XCPWB-XTAIL-CROOTT)*ABS(SIN(AL))
XLAM1=XLAMW
GO TO 3120
3110 XB1=8T/2.
XB2=8W/2.
TT=D/BW
HW1=-0.5*CROOTT*ABS(SIN(DELTA))+(XCPWB-XTAIL-CROOTT)*ABS(SIN(AL))
XLAM1=XLAMT
3120 FTRT=((XB2-R)/2.*(1.-TT)))*((3.14159/4.)-(3.14159*TT**2)/4.)-TT+
*((1.-TT**2)**2)/(2.*(1.-TT**2))*ARSIN((1.-TT**2)/(1.-TT**2)))
FW=FTRT+R
FI2=(FW*R**2)/(FW**2)+(HW1**2)
HI2=(HW1*R**2)/(FW**2)+(HW1**2)
ZC=FW
ZO=HW1
ZLT=0.0
DO 3130 I=1,4
ZL1=((XB1)-(XLAM1*R))-ZC*(1.-XLAM1))/((2.)*(XB1-R))
ZL2=ALOG((ZD**2)+((ZC-XB1)**2))/((ZC-XB1)**2))
ZL3=((1.-XLAM1)/(XB1-R))*((XB1-R)+(ZD*(ATAN((ZC-XB1)/ZD)-ATAN((ZC-
*R)/ZD)))
ZL=(ZL1*ZL2)-ZL3
IF(I-2) 3130,3140,3140
3130 ZC=-ZC
GO TO 3170
3140 IF(I-3) 3150,3160,3170
3150 ZL=-ZL
ZC=FI2
ZD=HI2
GO TO 3170
3160 ZL=-ZL
ZC=-FI2
ZLT=ZLT+ZL
3170 CONTINUE
IF(ICSC-1) 3190,3190,3200
3190 ART=(BT-D)**2/SI
XB1=8T/2.
CL1=((CLALW*CLALT*XKWB I*SIN(AL)*SW*2.*ZLT*(XBT-R))/(2.*3.14159*ART*
*FTRT*AREA*(1.-XLAMT)))
CL1=CL1*COS(AL)
CLTP=CLTP+CL1
CLIT=CLTP+CL1
CLIT=CL1
CLIW=0.
XCPTV=XCPT8
GO TO 3230
3200 ARW=(BW-D)**2/SW

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LAE09160  
 LAE09170  
 LAE09180  
 LAE09190  
 LAE09200  
 LAE09210  
 LAE09220  
 LAE09230  
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 LAE09480  
 LAE09490  
 LAE09500  
 LAE09510  
 LAE09520  
 LAE09530  
 LAE09540  
 LAE09550  
 LAE09560  
 LAE09570  
 LAE09580  
 LAE09590  
 LAE09600  
 LAE09610  
 LAE09620  
 LAE09630

```

XBW=8W/2.
CLY={CLALW*CLALT*(XKMBI*SIN(AL)+XKIBI*SIN(DELTA))*ST*2.*ZLT*(XBW-
*R1)/12.*3.14159*ARW*FTRT*AREA*(1.+XLAMW))
CLY=CLY*CD$ (AL)
CLW=CLW+CLY
CLWP=CLWP+CLY
CLIM=CLY
CLIT=0.
XCPTV=XCPWB
GO TO 3230
3210 CLT=0.
CLALT=0.
CLTD=0.
CLBT=0.
CLBDT=0.
CLTB=0.
CLTDB=0.
CLVIST=0.
CLIT=0.
CLIW=0.
CLIP=0.
GO TO 3230
3220 CLW=0.
CLALW=0.
CLBW=0.
CLWB=0.
CLVISM=0.
CLIW=0.
CLIT=0.
CLI=0.
IF (SW2) 3240,3240,3250
3230 CLW2=0.
CLALW2=0.
CLWB2=0.
CLWB2=0.
C INDUCED DRAG
3250 ALPTOT=CLWP+CLTP+CLB+CLBW+CLBT
IF (ARW.GT.3.0) GO TO 3260
IF (VXM.GE..85) GO TO 3260
CDI=ABS (CLTOT*TAN (ALPHA))
GO TO 3270
3260 CDI=(CLTOT)**2/(PIE*BW**2*.7/AREA)
3270 IF (BT) 3280,3290,3280
3280 ARI=BT**2/AREA
COTD=CLTD**2/(PIE*ARI*.7)

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LAE09640
LAE09650
LAE09660
LAE09670
LAE09680
LAE09690
LAE09700
LAE09710
LAE09720
LAE09730
LAE09740
LAE09750
LAE09760
LAE09770
LAE09780
LAE09790
LAE09800
LAE09810
LAE09820
LAE09830
LAE09840
LAE09850
LAE09860
LAE09870
LAE09880
LAE09890
LAE09900
LAE09910
LAE09920
LAE09930
LAE09940
LAE09950
LAE09960
LAE09970
LAE09980
LAE09990
LAE10000
LAE10010
LAE10020
LAE10030
LAE10040
LAE10050
LAE10060
LAE10070
LAE10080
LAE10090
LAE10100
LAE10110

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LAE10120  
LAE10130  
LAE10140  
LAE10150  
LAE10160  
LAE10170  
LAE10180  
LAE10190  
LAE10200  
LAE10210  
LAE10220  
LAE10230  
LAE10240  
LAE10250  
LAE10260  
LAE10270  
LAE10280  
LAE10290  
LAE10300  
LAE10310  
LAE10320  
LAE10330  
LAE10340  
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LAE10360  
LAE10370  
LAE10380  
LAE10390  
LAE10400  
LAE10410  
LAE10420  
LAE10430  
LAE10440  
LAE10450  
LAE10460  
LAE10470  
LAE10480  
LAE10490  
LAE10500  
LAE10510  
LAE10520  
LAE10530  
LAE10540  
LAE10550  
LAE10560  
LAE10570  
LAE10580  
LAE10590

```

3290 CLT=CDOT+(CLTP**2/(PIE*AR1*.7))
3300 IF(BW2)3300,3310,3300
3310 AR2=BW2**2/AREA
3320 CDW2=CDOW2+(CLW2**2/(PIE*AR2*.7))
3330 IF(BW1)3320,3330,3320
3340 AR3=BW1**2/AREA
3350 CDW=CDOW+(CLWP**2/(PIE*AR3*.7))
3360 C AXIAL AND NORMAL COMPONENTS
3370 CATD=CDTD*COSSAAL-CLTD*SINAAL
3380 CNTD=CLTD*COSSAAL+CDTD*SINAAL
3390 CNT=CLT*COSSAAL+CDT*SINAAL
3400 CNTP=(CLTP+CLTD)*COSSAAL+(CDT+CDTD)*(SINAAL)
3410 CNW=CLW*COSSAAL+CDW*SINAAL
3420 CNWP=CLWP*COSSAAL+CDW*SINAAL
3430 CNW2=CLW2*COSSAAL+CDW2*SINAAL
3440 CAB=(CDOB+CDB)*COSSAAL-CLB*SINAAL
3450 CAW=CDW*COSSAAL-CLW*SINAAL
3460 CAW2=CDW2*COSSAAL-CLW2*SINAAL
3470 CAT=CDT*COSSAAL-CLT*SINAAL
3480 CA5=CAT+CAW+CAW2+CATD+CAB
3490 GO TO 3370
3500 CN=CNB
3510 XCP2=XCPB
3520 IF(XAL(J).GT.90.)GO TO 3350
3530 CA=CA5*COS(AL)*COS(AL)
3540 GO TO 3360
3550 CA51=-(.5667+.893*VXM-.1727*VXM*VXM)
3560 CA=CA51*COS(AL)*COS(AL)
3570 CONTINUE
3580 CLTOT=CLB
3590 CDTOT=CLB
3600 CLALW=0.
3610 CLALT=0.
3620 CDT=0.
3630 CDO=0.
3640 CDW=0.
3650 CATD=0.
3660 CNTD=0.
3670 CNT=0.
3680 CNTP=0.
3690 CAT=0.
3700 CAW=0.
3710 CNW=0.
3720 CNW2=0.
3730 CLW=0.
3740 CLWP=0.
3750 CLTP=0.

```

```

CLIT=0.
CLL=0.
CLWI=0.
CLALW2=0.
CPW2=0.
CAN2=0.
CNTT=0.
CNWT=0.
CNW12=0.
CNW2=0.
CLW2=0.
XCPW2=0.
XCPW=0.
GO TO 3490
C TOTAL NORMAL, AXIAL, AND DRAG FORCE COEFFICIENTS
3370 CNBC=(CLBW+CLBT+CLBW2)*COSAAL
CNTP=CLTP+COSAAL+CDT*SINAAL
CNWP=CLWP+COSAAL+CDW*SINAAL
CNW2=CLW2+COSAAL+CDW2*SINAAL
CN=CNWP+CNTP+CNB+CNW2+CNBC
CDI=CDI+CDT
CDTOT=CDTOT+CDI+CDT
CA=CDTOT*COSAAL-CLTOT*SINAAL
C TOTAL CENTER OF PRESSURE CALCULATIONS
XCPBC=(XCPBW*CLBW+COSAAL+XCPBT*CLBT+COSAAL+XCPBW2*CLBW2+COSAAL)
*/CNBC
IF (ST) 3390,3390,3380
3380 XCP=XCPTB
3390 IF (SW) 3420,3420,3400
3400 XCPW=XCPTW
IF (SW2) 3420,3420,3410
3410 XCPW2=XCPWB2
3420 IF (SW2) 3430,3430,3440
3430 XCPW2=0.
CNW2=0.
IF (SW) 3450,3450,3440
3440 XCPW=((XCPW)*CNWP+(XCPW2)*CNW2)/(CNWP+CNW2)
CNWP=CNWP+CNW2
IF (SW) 3450,3450,3460
3450 XCPW=0.
3460 IF (ST) 3470,3470,3480
3470 XCP=0.
3480 XCP2=(CNB*XCPB+XCP*CNTP+XCPW*CNWP+XCPBC*CNBC)/(CNB+CNTP+CNWP+CNBC)
C PITCHING MOMENT
3490 CM=CN*(XCG2-XCP2)/XREF
ALI=AL*57.29578

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LAE10600  
 LAE10610  
 LAE10620  
 LAE10630  
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 LAE10980  
 LAE10990  
 LAE11000  
 LAE11010  
 LAE11020  
 LAE11030  
 LAE11040  
 LAE11050  
 LAE11060  
 LAE11070

```

C OUTPUT
WRITE(8,3500) ALL,CLTOT,CDTOT,CLWP,CLBW,CLTP,CLBT,CLB,CDI,CNWP,
*CNTP,CLTD,CDTD,CN,CA,XCPW,XCPT,XCPB,XCP2,CM
3500 FORMAT(1X,F3.0,18(1X,F5.2),1X,F6.2)
3510 WRITE(6,3520)ALL,CLTOT,CDTOT,CLWP,CLBW,CLTP,CLBT,CLB,CDI,CNWP,CNTP,
3520 WRITE(1X,F3.0,10(1X,F6.2))
3530 WRITE(6,3530)CLTD,CDTD,CN,CA,XCPW,XCPT,XCPB,XCP2,CM
3530 FORMAT(4X,9(1X,F6.2))
C*****
C THE FOLLOWING INSTRUCTIONS ARE FOR THE PLOT OUTPUT FACILITY
IF (CLTOT.LT.CLMIN) CLMIN=CLTOT
IF (CLTOT.GT.CLMAX) CLMAX=CLTOT
CLM(IJ,II,J)=CLTOT
CLM(IJ,II,J)=CM
CMM(IJ,II,J)=CM
CAM(IJ,II,J)=CA
CNM(IJ,II,J)=CN
CDIM(IJ,II,J)=CDI
C*****
ALPHA = XAL(J+1)
3540 CONTINUE
WRITE(8,3560)CDINL,CDAFT,CDPROT,CDDB
WRITE(8,3570)CDOW,CDOT,CDMISC,CDOWBT
3550 WRITE(6,3560)CDINL,CDAFT,CDPROT,CDDB
3560 FORMAT(1X,CDINL=F6.4, CDAFT=F6.4, CDPROT=F6.4, CDOB=F6.4)
3570 WRITE(6,3570)CDOW,CDOT,CDMISC,CDOWBT
3570 FORMAT(1X,CDOW=F6.4, CDOT=F6.4, CDMISC=F6.4, CDOWBT=F6.4)
C
DELTA1=XDT(II+1)
3580 CONTINUE
VXM=XVXM(IJ+1)
3590 CONTINUE
IF (NBDY-IL) 3600,3600,1040
3600 CONTINUE
CLAMW=CLAMW*57.29578
CLAMT=CLAMT*57.29578
WRITE(6,3610)
3610 FORMAT(1X,DO YOU WANT ANOTHER RUN, 00=YES, 01=NO)
READ(5,1060)IZXI
IF(IZXI.EQ.0)GO TO 1100
CALL SCREEN
C*****
C THE FOLLOWING INSTRUCTIONS ARE FOR THE PLOT OUTPUT FACILITY
DC 4010 I=1,IM
DO 4010 J=1,IDT

```

LAE11080  
 LAE11090  
 LAE11100  
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 LAE11980  
 LAE11990  
 LAE12000  
 LAE12010  
 LAE12020  
 LAE12030

```

DO 4010 K=1,IAL
  ALK=XAL(I,K)      ALMIN=ALK
  IF (ALK.GT.ALMAX) ALMAX=ALK
  CDK=CDM(I,J,K)    CDMIN=CDK
  IF (CDK.GT.CDMIN) CDMIN=CDK
  CMK=CMN(I,J,K)    CMMIN=CMK
  IF (CMK.GT.CMMIN) CMMIN=CMK
  CAK=CAM(I,J,K)    CAMIN=CAK
  IF (CAK.GT.CAMIN) CAMIN=CAK
  CNK=CNM(I,J,K)    CNMIN=CNK
  IF (CNK.GT.CNMIN) CNMIN=CNK
  CDIK=CDIM(I,J,K)  CDIMIN=CDIK
  IF (CDIK.GT.CDIMIN) CDIMIN=CDIK
  CONTINUE
4010 WRITE(7,4020) IM,DT,ICL,CLMAX,CLMIN
4020 FORMAT(3I2,5X,2F6.2)
DO 4060 I=1,IM
  WRITE(7,4030) XVXM(I)
  DO 4070 J=1,4030
    XDT(J)
    WRITE(7,4040) (CLM(I,J,K), K=1,24)
    FORMAT(12F6.2,12F6.2)
    WRITE(7,4050) ALMAX,ALMIN
    (XAL(K), K=1,24)
    CDMAX,CDMIN
    (CDM(I,J,K), K=1,24)
    CMMAX,CMMIN
    (CMN(I,J,K), K=1,24)
    CAMAX,CAMIN
    (CAM(I,J,K), K=1,24)
    CNMAX,CNMIN
    (CNM(I,J,K), K=1,24)
    CDIMAX,CDIMIN
    (CDIM(I,J,K), K=1,24)
  CONTINUE
4070 CONTINUE
4060 WRITE(7,4080)
4080 FORMAT(1X,'*')
STOP
END
  
```



```

170 IF (HT-35332.0) 170,170,180
170 T=519.-HT/1280.
180 PS=(1.91-0.01315*Z)**5.256
180 GO TO 190
180 T=393.
180 B=1.69-0.0478*Z
190 PS=6.49*EXP(B)
190 C=49.1*SQRT(T)
190 PS=PS*70.9
190 RHO=PS/(1715.*T)
190 XMU=2.270*(T**1.5)/((T+198.6)*(10.**8))
190 REFT=(C*RHO)/XMU
200 WRITE(6,200)
200 FORMAT(1X,'IS THIS PROGRAM COMPARING EXPERIMENTAL DATA')
210 WRITE(6,210)
210 FORMAT(1X,'ENTER 00=NO, 01=YES')
220 READ 220,1EXP
220 FORMAT(12)
220 REFT=1000000.
220 IF(1EXP.EQ.0) GO TO 250
220 WRITE(6,230)
230 FORMAT(1X,'ENTER REYNOLDS NUMBER/XREF OF EXPERIMENTAL DATA')
230 READ 240, REFT
240 READ 240, REFT
240 FORMAT(F14.2)
250 CONTINUE
250 RETURN
250 END

C THIS SUBROUTINE CLASUB CALCULATES THE AERODYNAMIC SURFACE LIFT-CURVE SLOPES.
C DIMENSION VXNM(16),XDT(16),XAL(48)
C COMMON REFT,ISUBS,XLOB,ZF,VXM,IZZY,LLKK,LLLL,NSURF
C COMMON ICSC,INDSE,ISWPMW,IAFBW,ISWPMW2,ISWPT,IAFBT,IDUM1,
C *CLAMT,CLAMW,CLAMW2,D,XLNOS,BT,BW,BW2,CROOTW,CROOT,CROOTW2,
C *ST,SW,SW2,TOVCW,TTOVCW2,TOVCT,XLAMT,XLAMW,XLAMW2,
C *XMACW,XMACW2,XMAC,T,XWING,XWING2,XTAIL,HT,XLAREA,XREF,
C *ISWEPW,ISWEP,ISWEP2,NWING,NTAIL,NWING2,ENGINE,ENLET,BETA,DBASE,
C *DJET,XLABOD
C COMMON ART,ARM,ARM2,BAR,BCOLAM,BETAL,B1,CLALT,CLALW,CLALW2,CLAL1,
C *COLAM,CROOT,IAFB,ISMP,TOVCT,ODC,XBCRBW,XBCRBW2,XKBW,XKT8,XKTBT,
C *XKWB,XKWB1,ISWPL,RATIO,XLAM1,XMAC,DI
C IF (VXM-1.) 10,10,20
10 BETAL=SQRT (1.-VXM**2)
20 BETAL=SQRT (VXM**2-1.)

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LAE12520  
 LAE12530  
 LAE12540  
 LAE12550  
 LAE12560  
 LAE12570  
 LAE12580  
 LAE12590  
 LAE12600  
 LAE12610  
 LAE12620  
 LAE12630  
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 LAE12680  
 LAE12690  
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 LAE12900  
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 LAE12930  
 LAE12940  
 LAE12950  
 LAE12960  
 LAE12970  
 LAE12980  
 LAE12990



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30 IF (IZZY-4) 510,510,40
40 IF (VXM-1.160,50,60
50 BETAL=0.0000001
60 KFIN=0
   KFIN=KF IN+1
70 IF (SW) 420,420,70
   ARW = (BW - D)*12/SW
   BAR=BETAL*ARW
   ISWP=ISWPW
   XLAM=XLAMW
80 IF (BAR.GT.5.0.AND.VXM.GE.1.0) BAR=5.0
   IF (BAR.GT.5.0.AND.VXM.LT.1.0) BAR=5.0
   IF (ISWP-1) 90,90,200
90 IF (XLAM-.25) 170,100,100
100 IF (VXM-1.0) 110,110,120
110 CLAR=-.1833*BAR+1.6
   GO TO 370
120 IF (XLAM-.50) 130,140,150
130 CLAR=-.001032518*BAR**8+.0200677*BAR**7-.1557225*BAR**6
   **+.607131*BAR**5-1.21537*BAR**4+1.13786*BAR**3-.5718*BAR**2
   **+.458487*BAR+1.57588
   GO TO 370
140 CLAR=.00121006*BAR**8-.0254597*BAR**7+.22119793*BAR**6
   *-1.020448*BAR**5+2.651997*BAR**4-3.680957*BAR**3
   **+.1.97903*BAR**2+.27640134*BAR+1.57129
   GO TO 370
150 CLAR=-.00007776*BAR**8-.001814086*BAR**7+.051777483*BAR**6
   *-4355555*BAR**5+1.7240831*BAR**4-3.3472653*BAR**3
   **+.2.6137236*BAR**2-.23389542*BAR+1.57998
   GO TO 370
170 IF (VXM-1.) 180,180,190
180 CLAR=-.1667*BAR+1.575
   GO TO 370
190 IF (BAR-2) 200,200,210
200 CLAR=.00133364*BAR**5-.0318237*BAR**4+.26049*BAR**3-.8643*BAR**2
   **+.669396*BAR+2.2008
   GO TO 370
210 CLAR=-.040277*BAR**4+.222522*BAR**3-.48931*BAR**2+.47287*BAR+1.57
   GO TO 370
220 IF (XLAM-.1) 230,300,300
230 IF (VXM-1.) 240,240,250
240 CLAR=-.2077*BAR+1.575
   GO TO 370
250 IF (BAR-.25) 260,260,270
260 CLAR=.2077*BAR+1.575
   GO TO 370
270 IF (BAR-4.) 280,280,290

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LAE13000
LAE13010
LAE13020
LAE13030
LAE13040
LAE13050
LAE13060
LAE13070
LAE13080
LAE13090
LAE13100
LAE13110
LAE13120
LAE13130
LAE13140
LAE13150
LAE13160
LAE13170
LAE13180
LAE13190
LAE13200
LAE13210
LAE13220
LAE13230
LAE13240
LAE13250
LAE13260
LAE13270
LAE13280
LAE13290
LAE13300
LAE13310
LAE13320
LAE13330
LAE13340
LAE13350
LAE13360
LAE13370
LAE13380
LAE13390
LAE13400
LAE13410
LAE13420
LAE13430
LAE13440
LAE13450
LAE13460
LAE13470

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280 CLAR=-.1668*BAR+1.667
290 GO TO 370
290 CLAR=1.587*(1.26)**(2.-BAR)
300 GO TO 370
300 IF (XLAM-.3) 310,340,340
310 IF (VXM-1.) 320,320,330
320 CLAR=-.2065*BAR+1.6
330 GO TO 370
330 CLAR=.002119027*BAR**5-.03283282*BAR**4+.20366375*BAR**3
   *- .61820362*BAR**2+.62703849*BAR+1.550048
340 GO TO 370
340 IF (VXM-1.) 350,350,360
350 CLAR=-.225*BAR+1.675
360 GO TO 370
360 IF (XLAM-1E-.40) CLAR=.00070428*BAR**8-.0158837*BAR**7
   *+.1489347*BAR**6-.74733673*BAR**5+2.18618223*BAR**4
   *-3.3445976*BAR**3+2.2919403*BAR**2-.21045286*BAR+1.6203524
   *IF (XLAM-1E-.40) CLAR=.00012278513*BAR**8+.0000879756*BAR**7
   *+.025071933*BAR**6-.25587433*BAR**5+1.0834904*BAR**4
   *-2.1562044*BAR**3+1.6307710*BAR**2-.084287165*BAR+1.7039
370 CLAL=CLAR*AR
   IF (KFIN-2) 380,390,400
380 CLALW=CLAL
   GO TO 410
390 CLALW2=CLAL
   GO TO 410
400 CLAL=CLAL
   GO TO 410
410 IF (KFIN-2) 420,440,500
420 KFIN=KFIN+1
   IF (SW2) 440,440,430
430 AR=(BW2-D)**2/SW2
   BAR=BETAL*AR
   ISWP=ISWPW2
   ARW2=AR AMW2
   XLAM=XLAMW2
   GO TO 80
440 KFIN=KFIN+1
   IF (ST) 460,460,450
450 AR=(BT-D)**2/ST
   BAR=BETAL*AR
   ART=AR
   ISWP=ISWPT
   NSURF=NTAIL
   XLAM=XLAMT
   GO TO 80
460 IF (SW) 470,470,500
470 IF (SW2) 480,480,500
480 IF (ST) 490,490,500

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LAE13480
LAE13490
LAE13500
LAE13510
LAE13520
LAE13530
LAE13540
LAE13550
LAE13560
LAE13570
LAE13580
LAE13590
LAE13600
LAE13610
LAE13620
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LAE13650
LAE13660
LAE13670
LAE13680
LAE13690
LAE13700
LAE13710
LAE13720
LAE13730
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LAE13750
LAE13760
LAE13770
LAE13780
LAE13790
LAE13800
LAE13810
LAE13820
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LAE13880
LAE13890
LAE13900
LAE13910
LAE13920
LAE13930
LAE13940
LAE13950

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490 LLLL=2
    RETURN
500 LKK=0
510 IZZY = IZZY + 1
520 IF (SW) 530,520
    COLAM= COS( CLAMW ) / ( SIN( CLAMW + .1 ) )
    ARW= ( BW - D ) * #2 / SW
    BCOLAM= BETA1 * COLAM
    CROOT= CROOTW
    B1=BW
    IAFB= IAFBW
    XMAC= XMACW
    TOVC= TOVCW
    CLAL1= CLALW
    XLAM1= XLAMW
    ISMP1= ISMPW
    NSURF= NSURFW
    BAR= BETA1 * ARW
    RATIO= CROOT / ( BETA1 * D )
    LLLL=0
    RETURN
530 IZZY = IZZY + 1
540 IF (SW2) 540,540,550
550 LLLL=1
    RETURN
    COLAM= COS( CLAMW2 ) / ( SIN( CLAMW2 + .1 ) )
    BCOLAM= BETA1 * COLAM
    CROOT= CROOTW2
    B1=BW2
    IAFB= IAFBW2
    CLAL1= CLALW2
    XLAM1= XLAMW2
    NSURF= NSURFW2
    XMAC= XMACW2
    TOVC= TOVCW2
    ISMP1= ISMPW2
    ARW2= ( BW2 - D ) * #2 / SW2
    BAR= BETA1 * ARW2
    RATIO= CROOT / ( BETA1 * D )
    LLLL=0
    RETURN
    END

```

C C

C C SUBROUTINE CATSUB  
C THIS SUBROUTINE CALCULATES CENTER OF PRESSURE LOCATIONS, CROSS-FLOW  
C DRAG COEFFICIENTS, AND INTERFERENCE FACTORS.

LAE13960  
LAE13970  
LAE13980  
LAE13990  
LAE14000  
LAE14010  
LAE14020  
LAE14030  
LAE14040  
LAE14050  
LAE14060  
LAE14070  
LAE14080  
LAE14090  
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LAE14120  
LAE14130  
LAE14140  
LAE14150  
LAE14160  
LAE14170  
LAE14180  
LAE14190  
LAE14200  
LAE14210  
LAE14220  
LAE14230  
LAE14240  
LAE14250  
LAE14260  
LAE14270  
LAE14280  
LAE14290  
LAE14300  
LAE14310  
LAE14320  
LAE14330  
LAE14340  
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LAE14360  
LAE14370  
LAE14380  
LAE14390  
LAE14400  
LAE14410  
LAE14420  
LAE14430

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DIMENSION XVXM(16), XDT(16), XAL(48)
COMMON REF1, REF2, XSUBS, XLOB, ZF, VXM, IZZY, LKK, LLL, NSURF
COMMON ICSC, INOSE, ISWPW, IAFBW, ISWPW2, IAFBW2, ISWPT, IAFBT, IDUM1,
1CLANT, CLAMW, CLAMW2, D, XLNOSE, BT, BW, BW2, CROOTW, CROOTT, CROOTW2,
2ST, SW, SW2, TOVCW, TOVCW2, TOVCT, XLAMT, XLAMW, XLAMW2,
3XMACW, XMACW2, XMACT, XWING, XWING2, XTAL, HT, XLAREA, XREF,
4ISWEPW, ISWEP, ISWEP2, NWIN, NTAIL, NWIN2, ENGINE, ENLET, BETA, DBASE,
5DJET, XLABOD
COMMON ART, ARW, ARW2, BAR, BCOLAM, BETAL, B1, CLALT, CLALW, CLALW2, CLAL1,
1COLAM, CROOT, IAFB, ISWP, TOVC, ODC, XBCRBW, XBCRBW, XKBW, XKTBT, XKTBT,
2XKWB, XKWB1, ISWP1, RATIO, XLAM1, XMACD1
XKWB=(2./3.14159)*((1.+D**4/B1**4)*{.5*ATAN(.5*(B1/D-D/B1))+3.14159*
19/4.})-((D**2/B1**2)*((B1/D-D/B1)+2.*ATAN(D/B1)))/(1.-D/B1)**2
10 XKTBT=((3.14159)**2*D**2*(B1/D+1.))**2/(4.*B1**2)+3.14159*D**2*(B1**2/B1**2-1.)/(B1**2/B1**2-1.))
22/D**2+1.))
XKTBT2=2.*3.14159*D*(B1/D+1.)/(B1**2/B1**2-1.))**2/(B1**2/D**2+1.))
1B1**2/D**2*(B1/D-1.))**2/(B1**2/D**2-1.))
2)**2
XKTBT3=(4.*D*(B1/D+1.)/(B1**2/B1**2-1.))**2/(B1**2/D**2-1.))/(B1**2/D**2+1.))
1/D**2+1.))-((8.)/(B1/D-1.))**2)*ALOG10((B1**2/D**2+1.))/(2.*B1/D))
XKTBT=(1.)/(3.14159)**2*(XKTBT1-XKTBT2-XKTBT3)
IF (ICSC-1) 20,20,40
20 IF (LLK) 30,30,50
30 XKTBT=D/B1+1.
GO TO 50
IF (LLK-1) 50,50,30
50 BAREF=BAR*(1.+XLAM1)*((1.)/(BETAL*COLAM))+1.))
IF (BAREF-4.) 60,60,70
60 XKWB=(1.+D/B1)**2-XKWB
GO TO 180
70 IF (IAFB) 80,110,80
80 IF (BCOLAM-1.) 100,90,90
90 XKWB1=(BCOLAM/(1.+BCOLAM))*((1.)/(BETAL*COLAM))+1.))
1M1**2)*ARCCOS((1.)/(1.+BCOLAM))*((1.)/(BETAL*COLAM))+1.))
2RATIO))
XKWB2=(SQRT(BCOLAM**2-1.)/(BCOLAM+1.))*(SQRT(1.+2.*BETAL*D/CROOT))-
11.))-((SQRT(BCOLAM**2-1.)/(BCOLAM))*((BETAL*D/CROOT))**2*ALOG(1.+CROOT/
2(BETAL*D))+SQRT((1.+CROOT/(BETAL*D))**2-1.))-((BCOLAM/(1.+BCOLAM))*
3ARCCOS(1.-/BCOLAM)
XKWB=(8.*BCOLAM/(3.14159*SQRT(BCOLAM**2-1.))*(1.+XLAM1)*(BETAL*D/
1CROOT)*(B1/D-1.))*(BETAL*CLAL1))*((XKBW1+XKBW2)
GO TO 180
100 XKWB1=((BCOLAM+1.+BCOLAM)*BETAL*D/CROOT)/(BCOLAM)**1.5+((BCOLAM+1.
1.+BCOLAM)*BETAL*D/CROOT)/(BCOLAM)**5-2.
XKWB2=((1.)+(BCOLAM)*BETAL*D/CROOT)/(BCOLAM)**2*0.5*(ALOG(1.+SQRT(BCOLAM
1OLAM/(BCOLAM+1.+BCOLAM)*BETAL*D/CROOT))-ALOG(1.-SQRT(BCOLAM/(BCOLAM+1.

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21AM+(1.+BCOLAM)*BETAL*D/CROOT))))
XKBW=((16.*(BCOLAM/(1.+BCOLAM)))**2/(3.14159*(1.+XLAM1))*(BETAL*D/
LCROOT)*(B1/D-1.))*(BETAL*CLAL1)))*(XKBW1-XKBW2)
GO TO 180
110 IF(BCOLAM-1.) 150 120,120
120 IF(RATIO-1.) 130,140,140
130 RATIO=1.
140 D=CROOT/BETAL
140 XKB1=(1.+COLAM*BETAL*RATIO)**2*ARCOS((BCOLAM+RATIO)/(1.+COLAM*BETAL
11*RATIO))
XKB2=BCOLAM**2*RATIO**2*ARCOS(1./BCOLAM)-BCOLAM*RATIO**2*SQR T(BCOL
1AM**2-1.)*AR SIN(1./RATIO)
XKB3=SQR T(BCOLAM**2-1.)*ALOG(RATIO+SQR T(RATIO**2-1.))
XKBW=((8./(3.14159*SQR T(BCOLAM**2-1.))*BETAL*CLAL1*(XLAM1+1.))*(B1/D
11-1.)))*(1./RATIO))*(XKB1-XKB2-XKB3)
GO TO 180
150 IF(RATIO-1.) 160,170,170
160 RATIO=1.
170 D=CROOT/BETAL
170 XKB1=(1.+COLAM*BETAL*RATIO)*SQR T((RATIO-1.)*(COLAM*BETAL*RATIO+1.
11)
XKB2=RATIO**2*(BCOLAM)**1.5-BCOLAM*RATIO**2*(BCOLAM+1.)*(ATAN(SQR T
11/BCOLAM))-ATAN(SQR T((RATIO-1.)/(COLAM*BETAL*RATIO+1.)))
XKB3=((BCOLAM+1.)/SQR T(BCOLAM))*0.5*(ALOG(1.+SQR T(BCOLAM*(RATIO-1.
11)/(COLAM*BETAL*RATIO+1.)))-ALOG(1.-SQR T(BCOLAM*(RATIO-1.)/(COLAM*
2BETAL*RATIO+1.))))
XKBW=((16.*SQR T(BCOLAM)*(1./RATIO)/(BETAL*CLAL1*(XLAM1+1.))*(B1/D1
1-1.)*3.14159*(BCOLAM+1.)))*(XKB1-XKB2-XKB3)
180 XKB1=XKBW-XKTB
D=D1
190 IF(VXM-1.0) 190,190,320
190 IF(15MP1-1.) 200,200,230
200 IF(BAR-2.0) 210,220,220
210 XBCRWB=0.35-XLAM1*(0.35+17.885-SQR T(328.8782-(BAR-3.))**2))
GO TO 260
220 XBCRWB=0.35-0.1*XLAM1
GO TO 260
230 IF(BAR-2.0) 240,250,250
240 XCR1=SQR T(2029.5+(BAR-3.))**2)
XBCRWB=(((-44.5+XCR1)-XLAM1*(-44.5+XCR1+17.885-SQR T(328.8782-(BAR
1-3.))**2)))
GO TO 290
250 XBCRWB=0.55-0.3*XLAM1
GO TO 290
260 IF(BAR-4.0) 270,280,280
270 XBCRWB=0.25-XLAM1*(32.125-SQR T(1032.02-(BAR-4.))**2))+(1.-XLAM1)*
1ALOG(1.04+0.1*D/B1)*(-7.5+SQR T(72.25-(BAR-4.0))**2))
GO TO 520

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LAE14920
LAE14930
LAE14940
LAE14950
LAE14960
LAE14970
LAE14980
LAE14990
LAE15000
LAE15010
LAE15020
LAE15030
LAE15040
LAE15050
LAE15060
LAE15070
LAE15080
LAE15090
LAE15100
LAE15110
LAE15120
LAE15130
LAE15140
LAE15150
LAE15160
LAE15170
LAE15180
LAE15190
LAE15200
LAE15210
LAE15220
LAE15230
LAE15240
LAE15250
LAE15260
LAE15270
LAE15280
LAE15290
LAE15300
LAE15310
LAE15320
LAE15330
LAE15340
LAE15350
LAE15360
LAE15370
LAE15380
LAE15390

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280 XBCRBW=0.25+((1.-XLAM1)*ALOG(1.04+0.1*D/B1))
GO TO 520
290 IF (BAR-4.0) 300,310,310
300 XBCRBW=0.25+((1.-2.*XLAM1)*(32.125-SQRT(1032.02-(BAR-4.)*2)))+
1((1.-XLAM1)*ALOG(1.12+0.3*D/B1))*2
GO TO 520
310 XBCRBW=0.25+((1.-XLAM1)*ALOG(1.12+0.3*D/B1))
GO TO 520
320 IF (ISWP1-1) 330,330,360
330 IF (BAR-3.0) 340,350,350
340 XBCRBW=-19.235+25.*((1.-XLAM1))+SQRT((9.71+25.*(1.-XLAM1))*2-
1(BAR-3.)*2)
GO TO 390
350 XBCRBW=0.005*BAR+0.46
GO TO 390
360 IF (BAR-3.1) 370,380,380
370 XBCRBW=0.675-XLAM1*(0.675+9.235-SQRT(94.1-(BAR-3.)*2))
GO TO 490
380 XBCRBW=0.005*BAR+0.46+0.2*((1.-XLAM1))
GO TO 490
390 BARLAM=BAR*((1.-XLAM1)*(1.+(1./BCOLAM))
IF (BARLAM-4.0) 400,400,440
400 IF (BAR-2.0) 410,430,430
410 XBMID1=ALOG(1.32-0.32*XLAM1)
420 XBMID2=4.+XBMID1**2-((0.5+0.5139*(D/B1))*(1.17+XLAM1))*(1./((0.331
1*(D/B1))))**2
XBMID3=2.*((XBMID1)-(0.5+0.5139*(D/B1))*(1.17+XLAM1))*(1./((0.331
1*(D/B1))))
XBMID=XBMID2/XBMID3
XCMID=4.+(XBMID1-XBMID)**2
XBCRBW=SQRT(XCMID-((BAR-2.)*2))+XBMID
GO TO 520
430 XBCRBW=0.5+0.25695*(D/B1)*(1./((0.331*(D/B1)))*BAR*(1.17+XLAM1))
GO TO 520
440 IF (IAFB) 450,450,480
450 IF (RATIO-1.0) 460,460,470
460 XBCRBW=0.67
GO TO 520
470 XBCRBW=2.32+SQRT(8.9401-((1./RATIO)-1.)*2)
GO TO 520
480 XBCRBW=(0.429/RATIO)+0.5
GO TO 520
490 BARLAM=BAR*((1.-XLAM1)*(1.+(1./BCOLAM))
IF (BARLAM-4.0) 500,500,440
500 IF (BAR-2.0) 510,430,430
510 XBMID1=ALOG(1.65-0.65*XLAM1)
GO TO 420
520 J=01

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LAE15400
LAE15410
LAE15420
LAE15430
LAE15440
LAE15450
LAE15460
LAE15470
LAE15480
LAE15490
LAE15500
LAE15510
LAE15520
LAE15530
LAE15540
LAE15550
LAE15560
LAE15570
LAE15580
LAE15590
LAE15600
LAE15610
LAE15620
LAE15630
LAE15640
LAE15650
LAE15660
LAE15670
LAE15680
LAE15690
LAE15700
LAE15710
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LAE15800
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LAE15850
LAE15860
LAE15870

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LAE15880  
 LAE15890  
 LAE15900  
 LAE15910  
 LAE15920  
 LAE15930  
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 LAE15950  
 LAE15960  
 LAE15970  
 LAE15980  
 LAE15990  
 LAE16000  
 LAE16010  
 LAE16020  
 LAE16030  
 LAE16040  
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 LAE16070  
 LAE16080  
 LAE16090  
 LAE16100  
 LAE16110  
 LAE16120  
 LAE16130

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    ARAT=BAR/BETAL
    IF (ARAT-4.0) 540, 540, 530
    ARAT=4.0
    ODC=2.+(1.+XLAM1)**1.6*EXP(-.4*ARAT)
    530 IF (ARAT-1.0) 580, 550, 550
    550 IF (XLAM1-LE-0.25) GO TO 560
    IF (XLAM1-LE-0.75) GO TO 570
    ODC=ODC-.25*(ARAT-1.)
    IF (ARAT-1.2) GO TO 580
    ODC=(2.+(1.+XLAM1)**1.6)*.45-(.85*(ARAT-2.))
    GO TO 580
    ODC=(2.+(1.+XLAM1)**1.6)*.67-(.3*(ARAT-1.0))
    GO TO 580
    ODC=(2.+(1.+XLAM1)**1.6)*.67-(.725*(ARAT-1.))
    560 CONTINUE
    570 RETURN
    580 END

    SUBROUTINE SCREEN
    WRITE (6,500)
    500 FORMAT (/'X', 'CLEAR SCREEN AND ENTER "0"' )
    16 READ (6,16) ISCR
    16 FORMAT (I11)
    RETURN
    END
  
```

C

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```

//AEROPLOT JOB (1414,0483,,24),'LINDSEY',CLASS=A
// EXEC FRTXCLGP
//FORT.SYSIN DD *
C*****PROGRAM AEROPLOT*****
C
C PROGRAM AEROPLOT PLOTS DIMENSIONLESS AERODYNAMIC COEFFICIENTS
C CD TOTAL, CM, CA, CN, CD INDUCED AND ANGLE OF ATTACK AS A
C FUNCTION OF LIFT COEFFICIENT. A SEPARATE PLOT IS GENERATED
C FOR EACH MACH NUMBER (MAX OF 30 MACH NUMBERS) ALLOWING FOR UP
C TO 10 DIFFERENT CONTROL SURFACE DEFLECTIONS FOR EACH PLOT.
C THE PROGRAM USES VER SAPLOT SOFTWARE FOR USE ON THE IBM 3033
C COMPUTER. ACTUAL PLOTTING IS ACCOMPLISHED VIA SUBROUTINE
C "GRAPH" TO PERMIT RELATIVELY PAINLESS TRANSITION TO OTHER
C SOFTWARE, THOUGH LOCATION OF ORIGIN FOR THE VARIOUS PLOTS ARE
C DETERMINED IN MAIN PROGRAM.
C
C VARIABLES USED IN COMMON BLOCKS ARE AS FOLLOWS.
C 1. A SCALE - CONTAINS THE INITIAL PLOTTING VALUE AND PLOT
C INCREMENT FOR ALL 6 PLOT PARAMETERS. PLOT INCREMENTS
C ARE DETERMINED SUCH THAT EACH PLOT IS ON A 5" X 5"
C AXIS
C
C 2. ISYMBL - CONTAINS THE INTEGER DESIGNATION OF THE PLOTTING
C SYMBOL USED IN GRAPHING
C
C OTHER VARIABLES:
C 1. LEGEND - ARRAY OF 10 PLOTTING SYMBOL INTEGERS USED TO
C PRODUCE A LEGEND OF SYMBOLS CORRESPONDING TO THE VARIOUS
C CONTROL SURFACE DEFLECTIONS USED.
C
C 2. DELTA - ARRAY OF CONTROL SURFACE DEFLECTION ANGLES
C
C 3. IFLAG - FLAG WHICH DETERMINES IF COORDINATE AXES ARE
C TO BE PLOTTED (1), OR IF ANOTHER DELTA VALUE IS TO
C BE PLOTTED ON AN ALREADY EXISTING GRAPH (0).
C
C ALL DATA TO BE PLOTTED IS GENERATED FROM AN EXTERNAL SOURCE.
C NO COEFFICIENT CALCULATIONS ARE MADE IN THIS PROGRAM.
C
C LT. GREY HOBBY USN
C*****MARCH 1981*****
C
C DIMENSION CL(24), DELTA(14), LEGEND(10)
C REAL MACH
C COMMON/ASCALE/FVALX,FVALY,DVX,DVY,FCM,DCM,FCD,DCD,
C +FCDT,DCDT,FCA,DCA,FCN,DCN
C COMMON/ISYMBL/NSYMB
C DATA LEGEND /1,2,3,4,5,6,7,8,9,10/
  
```



```
C  
C  
C  
C.  
C.  
C.  
ENTER NUMBER OF MACH,NUMBER OF DELTA/MACH,NUMBER OF CL AND  
MAX,MIN CL  
READ(5,900)NMACH,NDEL,NCL,CLMAX,CLMIN  
  
C  
C.  
C.  
SET UP PLOTTING WINDOW TO ALLOW PLOTTING SPACE FOR UP  
TO 30 MACH NUMBERS  
XMACH=FLOAT(NMACH)  
XPLOT=.2*.X*MACH  
CALL WINDOW(O,XPLOT,O,XPLOT)  
  
C  
C=====  
C INITIALIZE PLOT  
C CALL PLOTS(O,O,O)  
C MOVE ORIGIN TO ALLOW SPACE FOR AXIS LABELS AND TITLES  
C CALL PLOT(1.,1.,-3)  
  
C  
C.  
C READ MACH AND PLOT ALPHA, CM,CDTOT,CA,CLTOT,CN  
DO 100 I=1,NMACH  
C SET UP FLAG FOR AXIS PLOT AND PLOT SYMBOL DESIGNATION  
NSYMB=1  
IFLAG=1  
READ(5,902) MACH  
  
C  
C.  
C PLOT DATA FOR EACH MACH NUMBER  
DO 90 J=1,NDEL  
C READ DELTA  
READ(5,902) DELTA(J)  
C READ CL DATA  
READ(5,901)CL  
  
C  
C.  
C PLOT ANGLE OF ATTACK  
CALL ALPLOT(NCL,CL,CLMIN,CLMAX,IFLAG)  
C REORIGIN AND PLOT TOTAL DRAG COEFFICIENT  
CALL PLOT(5.75,0,-3)  
C CALL CDTPLOT(NCL,CL,CLMIN,CLMAX,IFLAG)  
C CALL PLOT(-5.75,0,-3)  
C REORIGIN AND PLOT Pitching Moment  
CALL PLOT(.75,75,-3)  
C CALL CMPLOT(NCL,CL,CLMIN,CLMAX,IFLAG)  
C CALL PLOT(0,-5.75,-3)  
C REORIGIN AND PLOT CA  
CALL PLOT(5.75,5.75,-3)  
C CALL CAPLOT(NCL,CL,CLMIN,CLMAX,IFLAG)  
C CALL PLOT(-5.75,-5.75,-3)  
C REORIGIN AND PLOT Normal Force
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```

      CALL PLOT(0.,11.5,-3)
      CALL CNPLOT(NCL,C1,CLMIN,CLMAX,IFLAG)
      CALL PLOT(0.,-11.5,-3)
      REORIGIN AND PLOT INDUCED DRAG
      CALL PLOT(5.75,11.5,-3)
      CALL CDPLT(NCL,C1,CLMIN,CLMAX,IFLAG)
      CALL PLOT(-5.75,-11.5,-3)

C. INCREMENT SYMBOL NUMBER AND ZERO AXIS FLAG
  NSYMB=NSYMB+1
  IFLAG=0
  CONTINUE

90 C. LABEL PLOT WITH MACH NUMBER
  CALL NEWPEN(3)
  CALL SYMBOL(4.5,-1.0,.25,'MACH = ',0,0,7)
  CALL NUMBER(6.25,-1.0,.25,'MACH',0,0,2)
  PRINT LEGEND FOR DELTA PLOTTING SYMBOLS
  XSYMB=9.75
  YSYMB=17.0
  XDEL=10.0
  DO 95 J=1,NDEL
    PRINT PLOTTING SYMBOL
    CALL SYMBOL(XSYMB,YSYMB,0.1,LEGEND(J),0.,-1)
  C. PRINT DELTA VALUE
  CALL DELTA VALUE
  CALL NUMBER(XDEL,YSYMB,0.1,DELTA(J),0.,-1)
  C. INCREMENT PLOTTING SYMBOL AND PRINT COORDINATES
  YSYMB=YSYMB+0.15
  95 CONTINUE
  C. LABEL THE LEGEND
  YSYMB=YSYMB+0.15
  CALL SYMBOL(9.5,YSYMB,0.1,'DELTA LEGEND:',0.,13)
  C. LABEL PLOTTING GRAPH
  CALL SYMBOL(3.,19.5,.25,'AERODYNAMIC COEFFICIENTS',0.,24)
  C. MOVE TO NEXT MACH PLOTTING POSITION
  CALL PLOT(12.5,0.,-3)

100 C. CONTINUE
C. TERMINATE PLOT
  CALL PLOT(0.,0.,+999)
C *****FORMATS*****
900 FORMAT(3I2,5X,2F6.2)
901 FORMAT(12F6.2,/,12F6.2)
902 FORMAT(F6.2)
C *****

```

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COMPUTER PROGRAM APPLICATIONS TO TACTICAL MISSILE CONCEPTUAL DE--ETC(U)  
JUN 81 M D SULLIVAN

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C          STOP
C          END
C:
C:      SUBROUTINE GETDAT(YMAX,X,YMIN,Y)
C:      DIMENSION Y(24)
C:
C:      SUBROUTINE INPUTS YCOORD. ARRAY FOR PROCESSING BY PLOT ROUTINE
C:      READ(5,900)YMAX,YMIN
C:      READ(5,901)Y
C:
C:      =====FORMATS=====
C:      900  FORMAT(2F6.2)
C:      901  FORMAT(12F6.2/,12F6.2)
C:      =====
C:
C:      RETURN
C:      END
C
C      FUNCTION YSCALE(YMAX,YMIN)
C:      FUNCTION GENERATES PLOTTING INCREMENT FOR A 5" AXIS
C:      YSCALE=(YMAX-YMIN)/5.0
C:      RETURN
C:      END
C
C      SUBROUTINE GRAPH(NPOINT,XCOORD,YCOORD,FVX,FVY,XINC,YINC)
C:      DIMENSION XCOORD(NPOINT),YCOORD(NPOINT),X(26),Y(26)
C:      COMMON/ISYMBL/NSYMB
C
C:      SUBROUTINE GRAPHS N POINTS WITHOUT ALTERING INPUT ARRAYS
C:
C:      I1=NPOINT+1
C:      I2=NPOINT+2
C:      SET UP THE PLOTTING ARRAYS
C:      DO 10 I=1,NPOINT
C:      X(I)=XCOORD(I)
C:      Y(I)=YCOORD(I)
C:      CONTINUE
C:      INSERT SCALING VALUES: FIRST VALUE AND AXIS INCREMENT
C:      X(I1)=FVX
C:      X(I2)=XINC
C:      Y(I1)=FVY
C:      Y(I2)=YINC
C:      PLOT
C:      CALL LINE(X,Y,NPOINT,1,+2,NSYMB)

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```

C      RETURN
C      END
C
C      SUBROUTINE ALPLOT(NCL,CL,CLMIN,CLMAX,IFLAG)
C      DIMENSION CL(NCL)
C      COMMON/ASCALC/FVALX,FVALY,DVX,DVY,FCM,DCM,FCD,DCD,
C      +FCDT,DCDT,FCA,DCA,FCN,DCN
C      COMMON/ISYMBL/NSYMB
C      REAL ALPHA(24)
C      DATA LMASK1/Z18FF /
C
C      SUBROUTINE PLOTS ANGLE OF ATTACK AS A FUNCTION OF LIFT COEFFICIENT
C
C      READ MAX,MIN ALPHA, AND ALPHA DATA
C      CALL GETDAT(AMAX,AMIN,ALPHA)
C      GENERATE SCALE DATA
C      FVALY=AMIN
C      DVY=YSCALE(AMAX,AMIN)
C      FVALX=CLMIN
C      DVX=YSCALE(CLMAX,CLMIN)
C      CALL NEWPEN(3)
C      IF 1ST ALPHA PLOT, DRAW COORDINATE AXES
C      IF (IFLAG.EQ.0) GO TO 10
C      DRAW X,Y AXES
C      CALL AXIS(0,0,0,CL,-2,5,0,0,FVALX,DVX)
C      CALL AXIS(0,0,0,ALPHA,5,5,0,90,FVALY,DVY)
C      DRAW GRID
C      CALL NEWPEN(1)
C      CALL GRID(0,0,0,5,1,0,5,1,0,LMASK1)
C
C      PLOT ALPHA
C      CALL NEWPEN(2)
C      CALL GRAPH(NCL,CL,ALPHA,FVALX,FVALY,DVX,DVY)
C
C      RETURN
C      END
C
C      SUBROUTINE CMPLOT(NCL,CL,CLMIN,CLMAX,IFLAG)
C      DIMENSION CL(NCL),CM(24)
C      COMMON/ASCALC/FVALX,FVALY,DVX,DVY,FCM,DCM,FCD,DCD,
C      +FCDT,DCDT,FCA,DCA,FCN,DCN
C      COMMON/ISYMBL/NSYMBL
C      DATA LMASK1/Z18FF /
C
C      SUBROUTINE PLOTS PITCHING COEFFICIENT AS A FUNCTION OF LIFT

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```

C. COEFFICIENT
C. INPUT MAX, MIN CM AND CM DATA
C. CALL GETDAT(CMMAX, CMMIN, CM)
C. GENERATE SCALING DATA FOR PLOT: INIT, CM VAL(FCM) AND PLOT
C. INCREMENT(DCM)
  FCM=CMMIN
  DCM=YSCALE(CMMAX, CMMIN)
C. IF FIRST PLOT OF CM, DRAW COORDINATE AXES, OTHERWISE PROCEED
C. WITH PLOTTING.
  IF(FLAG.EQ.0) GO TO 10
  CALL NEWPEN(3)
  CALL AXIS(0.0., 'CM', 2.5, 0.90., FCM, DCM)
C. DRAW THE GRID
  CALL NEWPEN(1)
  CALL GRID(0.0., 0.0., 5, 1.0, 5, 1.0, LMASK1)
C. PLOT CM
  CALL NEWPEN(2)
  CALL GRAPH(NCL, CL, CM, FVALX, FCM, DVX, DCM)
C. DONE
  RETURN
C. END

SUBROUTINE COPLOT(NCL, CL, CLMIN, CLMAX, IFLAG)
  DIMENSION CL(NCL), CD(24)
  COMMON/ASCALE/FVALX, FVALY, DVX, DVY, FCM, DCM, FCD, DCD,
  +FCOT, DCDOT, FCA, DCA, FCN, DCN
  COMMON/ISYMBL/NSYMB
  DATA LMASK/Z18FF/

SUBROUTINE PLOTS DRAG AS A FUNCTION OF LIFT

C. INPUT MAX, MIN CD, AND CD DATA
C. CALL GETDAT(CDMAX, CDMIN, CD)
C. GENERATE SCALE DATA: INITIAL CD (FCD), PLOT INCREMENT (DCD)
  FCD=CDMIN
  DCD=YSCALE(CDMAX, CDMIN)
C. IF 1ST PLOT OF CD, DRAW Y AXIS, OTHERWISE PROCEED
C. WITH PLOT
  IF(FLAG.EQ.0) GO TO 10
  CALL NEWPEN(3)
  CALL AXIS(0.0., 'CDI', 3.5, 0.90, 0., FCD, DCD)
C. DRAW GRID
  CALL NEWPEN(1)
  CALL GRID(0.0., 0.0., 5, 1.0, 5, 1.0, LMASK)
  
```

```

C: 10 PLOT CD NEWPEN(2)
C: CALL GRAPH(NCL,CL,CD,FVALX,FCD,DVX,DCD)
C:
C: DONE
C: RETURN
C: END
C:
C: SUBROUTINE CDTPLT(NCL,CL,CLMIN,CLMAX,IFLAG)
C: DIMENSION CL(NCL),CDT(24)
C: COMMON/ASCAL/FVALX,FVALY,FCM,DCM,FCD,DCD,
C: +FCOT,DCOT,FCA,DCA,FCN,DCN
C: COMMON/ISYMBL/NSYMB
C: DATA LMASK/Z18FF/
C:
C: PLOT TOTAL DRAG AS A FUNCTION OF ANGLE OF ATTACK
C:
C: INPUT CD DATA
C: CALL GETDAT(CDTMAX,CDTMIN,CDT)
C: GENERATE SCALING DATA
C: FCDT=CDTMIN
C: DCDT=YSCALE(CDTMAX,CDTMIN)
C: IF IFLAG.EQ.0) GO TO 10
C: CALL NEWPEN(3)
C: CALL AXIS(0.,0.,,CDTOTAL,7.5,0.90,,FCOT,DCOT)
C: CALL AXIS(0.,0.,,CL,-2,5.0,0.0,FVALX,DVX)
C: DRAW GRID
C: CALL NEWPEN(1)
C: CALL GRID(0.,0.,5,1.0,5,1.0,LMASK)
C:
C: PLOT CD TOTAL
C: 10 CALL NEWPEN(2)
C: CALL GRAPH(NCL,CL,CDT,FVALX,FCDT,DVX,DCDT)
C:
C: DONE
C: RETURN
C: END
C:
C: SUBROUTINE CAPLOT(NCL,CL,CLMIN,CLMAX,IFLAG)
C: DIMENSION CL(NCL),CA(24)
C: COMMON/ASCAL/FVALX,FVALY,FCM,DCM,FCD,DCD,
C: +FCOT,DCOT,FCA,DCA,FCN,DCN
C: COMMON/ISYMBL/NSYMB
C: DATA LMASK/Z18FF/

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```

C. PLOT CA AS A FUNCTION OF ANGLE OF ATTACK
C.
C. INPUT CA DATA
C. CALL GETDAT (CAMAX,CAMIN,CA)
C. GENERATE SCALE DATA
C. FCA=CAMIN
C. DCA=YSCALE (CAMAX,CAMIN)
C. IF 1ST PLOT DRAW Y AXIS
C. IF (IFLAG.EQ.0) GO TO 10
C. CALL NEWPEN(3)
C. CALL AXIS(0.,0.,CA,2.5,90.,FCA,DCA)
C. DRAW GRID
C. CALL NEWPEN(1)
C. CALL GRID(0.,0.,5,1.0,5,1.0,LMASK)
C.
C. PLOT CA
C. 10 CALL NEWPEN(2)
C. CALL GRAPH(NCL,CL,CA,FVALX,FCA,DVX,DCA)
C.
C. DONE
C. RETURN
C. END
C.
C. SUBROUTINE CNPLOT (NCL,CL,CLMIN,CLMAX,IFLAG)
C. DIMENSION CL(NCL),CN(24)
C. COMMON/ASCALE/FVALX,FVALY,DVX,DVY,FCM,DCM,FCD,DCD,
C. +FCDT,DCDT,FCA,DCA,FCN,DCN
C. COMMON/ISYMBL/NSYMB
C. DATA LMASK/Z18FF/
C.
C. PLOT NORMAL FORCE AS A FUNCTION OF ANGLE OF ATTACK
C.
C. INPUT CN DATA
C. CALL GETDAT (CNMAX,CNMIN,CN)
C. GENERATE SCALE DATA
C. FCN=CNMIN
C. DCN=YSCALE (CNMAX,CNMIN)
C. IF 1ST PLOT DRAW Y AXIS
C. IF (IFLAG.EQ.0) GO TO 10
C. CALL NEWPEN(3)
C. CALL AXIS(0.,0.,CN,2.5,90.,FCN,DCN)
C. DRAW GRID
C. CALL NEWPEN(1)
C. CALL GRID(0.,0.,5,1.,5,1.,LMASK)
C.
C. PLOT CN
  
```



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LAEO3980

10 CALL NEWPEN(2)  
CALL GRAPH(NCL,CL,CN,FVALX,FCN,DVX,DCN)

C. DONE  
RETURN  
END

/\*GO.PLOTPARM DD \*  
&PLOT SCALE=0.85 &END  
/\*GO.SYSIN DD \*

#### LIST OF REFERENCES

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